

A. INTRODUCTION

This chapter examines the potential effects of the proposed projects on the study area's transportation systems. Specifically, it compares conditions in the future with the proposed projects (the With Action condition) against conditions in the future without the proposed projects (the No Action condition) in order to determine the potential for significant adverse impacts to transportation systems. The analyses consider the 2021 analysis year to identify potential impacts, and if warranted, identify mitigation measures that would be appropriate to address those impacts. The travel demand projections, trip assignments, and capacity analysis presented in this chapter were conducted pursuant to the methodologies outlined in the 2014 *City Environmental Quality Review (CEQR) Technical Manual*.

PRINCIPAL CONCLUSIONS

TRAFFIC

Based on a detailed assignment of project-generated vehicle trips, 31 intersections were identified as warranting detailed analysis for the weekday AM, midday, and PM peak hours. The detailed analysis concluded that in the future with the proposed projects, there would be the potential for significant adverse impacts at six intersections during the weekday AM peak hour, five intersections during the midday peak hour, and 10 intersections during the PM peak hour.

Table 14-1a provides a summary of the impacted locations by lane group and analysis time period. Potential measures to mitigate the projected traffic impacts are described in Chapter 21, "Mitigation."

Table 14-1a

Summary of Significant Adverse Traffic Impacts

| Intersection | | Weekday AM Peak Hour | Weekday Midday Peak Hour | Weekday PM Peak Hour |
|---|--------------------|--|--|---|
| EB/WB Street | NB/SB Street | | | |
| South Street | Pike Slip | | | SB-L |
| South Street | Clinton Street | | | EB-LT |
| South Street (North) | Montgomery Street | SB-TR | | WB-LTR NB-LT |
| South Street (South) | | SB-LT | | SB-LT |
| Madison Street | Pike Street (East) | EB-LT | | EB-LT |
| Madison Street | Montgomery Street | | | NB-LTR |
| East Broadway | Pike Street (East) | NB-L | NB-L | EB-L NB-L |
| | Pike Street (West) | EB-TR | EB-TR | EB-TR |
| Division Street | Market Street | | NB-L | |
| Canal Street | Allen Street | | | EB-LTR |
| Delancey Street | Allen Street | | WB-L | WB-L |
| Division Street | The Bowery | WB-L | | |
| East Broadway | Chatham Square | | SB-L | NB-R SB-L |
| Worth Street/Oliver Street | Chatham Square | EB-L (Worth Street) EB-LTR (Worth Street) | EB-L (Worth Street) EB-LTR (Worth Street) | EB-L (Worth Street) EB-LTR (Worth Street) WB-R SB-TR |
| | | SB-TR | SB-TR | |
| Worth Street | Centre Street | WB-T | | |
| Total Impacted Intersections/Lane Groups | | 6/10 | 5/8 | 10/18 |
| Notes: L = Left Turn, T = Through, R = Right Turn, DefL = Defacto Left Turn, EB = Eastbound, WB = Westbound, NB = Northbound, SB = Southbound | | | | |

TRANSIT

The preliminary screening assessment summarized below concluded that a detailed analysis of station circulation elements and control areas is warranted for the East Broadway-Rutgers Street Station (F line) for the weekday AM and PM peak hours. A subway line-haul (F line) analysis was also conducted for the weekday AM and PM peak hours.

The line-haul analyses showed that the proposed projects would not result in the potential for a significant adverse subway line-haul impact. The subway station analysis identified significant adverse stairway impacts for the S1 stairway during the weekday AM and PM peak hours, and the P3 stairway for the weekday AM peak hour. Discussions with New York City Transit (NYCT) to identify feasible mitigation measures to alleviate these significant adverse impacts are presented in Chapter 21, "Mitigation."

PEDESTRIANS

Weekday peak period pedestrian conditions were evaluated at key area sidewalk, corner reservoir, and crosswalk locations. Based on the detailed assignment of pedestrian trips, 18 sidewalks, 16 corner reservoirs, and 12 crosswalks were selected for detailed analysis for the weekday AM, midday, and PM peak hours. As summarized in **Table 14-1b**, significant adverse impacts were identified for one sidewalk during the weekday AM and PM peak hours, two crosswalks during the weekday AM peak hour, one crosswalk during the weekday midday peak hour, and two crosswalks during the weekday PM peak hour. Potential measures (i.e., crosswalk

widenings, signal timing adjustments, etc.) were identified to mitigate the pedestrian impacts, as described in Chapter 21, “Mitigation.”

Table 14-1b
Summary of Significant Adverse Pedestrian Impacts

| Pedestrian Element | Weekday AM Peak Hour | Weekday Midday Peak Hour | Weekday PM Peak Hour |
|---|----------------------|--------------------------|----------------------|
| North Sidewalk of Madison Street between Rutgers Street and Pike Street | Impacted | | Impacted |
| Rutgers Street and Madison Street North Crosswalk | Impacted | | |
| Rutgers Street and Madison Street West Crosswalk | Impacted | | Impacted |
| Rutgers Street and Cherry Street South Crosswalk | | Impacted | Impacted |

VEHICULAR AND PEDESTRIAN SAFETY

Crash data for the study area intersections were obtained from the New York State Department of Transportation (NYSDOT) for the time period between November 1, 2013 and October 31, 2016. During this period, a total of 278 injuries, and 96 pedestrian/bicyclist-related accidents occurred at study area intersections. A rolling total of accident data identified three high crash locations in the 2013 to 2016 period, Allen Street and Canal Street, the Bowery and Canal Street at the Manhattan Bridge, and Chatham Square/Park Row at Worth Street/Mott Street. A summary of the identified high crash locations, prevailing trends, project-specific effects, and recommended safety measures is provided in **Table 14-2**.

Table 14-2
Summary of High Crash Locations

| High Crash Intersections | Prevailing Trends | Peak Hour Project-Specific Effects | Recommended Safety Measures |
|--|-------------------|------------------------------------|---|
| Allen Street and Canal Street | None | Incremental trips: 54 vehicles | Install pedestrian countdown timers on all crosswalks |
| The Bowery and Canal Street | None | Incremental trips: 62 vehicles | Install pedestrian countdown timers on the east crosswalk |
| Chatham Square/Park Row and Worth Street/Mott Street | None | Incremental trips: 61 vehicles | No recommendations |
| Source: NYSDOT crash data; November 1, 2013 to October 31, 2016 | | | |

PARKING

The With Action public parking utilization is expected to increase to 113, 132, 116, and 112 percent of the ½-mile off-street parking capacity during the weekday morning, midday, evening, and overnight time periods, respectively. These utilization levels represent parking shortfalls of 293, 755, 373, and 274 spaces during the corresponding weekday peak periods. It is expected that excess parking demands resulting from the proposed projects during the weekday peak periods would need to be accommodated by on-street parking or off-street parking beyond ½-mile walk from the project sites. Alternatively, motorists could choose alternate modes of transportation. As stated in the *CEQR Technical Manual* and discussed in the parking analysis methodology section below, a parking shortfall resulting from a project located in Manhattan does not constitute a significant adverse parking impact, due to the magnitude of available alternative modes of transportation.

B. PRELIMINARY ANALYSIS METHODOLOGY AND SCREENING ASSESSMENT

The *CEQR Technical Manual* recommends a two-tier screening procedure for the preparation of a “preliminary analysis” to determine if quantified analyses of transportation conditions are warranted. As discussed below, the preliminary analysis begins with a trip generation analysis (Level 1) to estimate the volume of person and vehicle trips attributable to a proposed project. If a proposed project is expected to result in fewer than 50 peak hour vehicle trips and fewer than 200 peak hour transit or pedestrian trips, further quantified analyses are not warranted. When these thresholds are exceeded, detailed trip assignments (Level 2) are performed to estimate the incremental trips at specific transportation elements and to identify potential locations for further analyses. If the trip assignments show that a proposed project would result in 50 or more peak hour vehicle trips at an intersection, 200 or more peak hour subway trips at a station, 200 or more peak hour subway trips in one direction on a subway line, 50 or more peak hour bus trips in one direction along a bus route, or 200 or more peak hour pedestrian trips traversing a pedestrian element, then further quantified analyses may be warranted to assess the potential for significant adverse impacts on traffic, transit, pedestrians, parking, and vehicular and pedestrian safety.

As detailed in Chapter 1, “Project Description,” the proposed actions would facilitate the development of three new mixed-use buildings within the Two Bridges Large Scale Residential District (LSRD). The three project sites—Site 4 (4A/4B), Site 5, and Site 6A within the Two Bridges LSRD—are generally bounded by Cherry Street to the north, Pike Street to the west, Clinton Street to the east, and South Street to the south (see **Figure 14-1**). In the future with the proposed projects, the project sites would be developed with a total of approximately 2,775 new dwelling units (DUs), 10,858 gross square feet (gsf) of new local retail, and 17,028 gsf of new community facility use, not including the existing uses on the three sites that would remain in the With Action condition. The proposed community facility space on Site 5 is as yet unprogrammed; however, for the purposes of a conservative analysis, it is assumed that this space could be utilized as an accessory early childhood educational facility. **Table 14-3** provides program assumptions under the Reasonable Worst Case Development Scenario (RWCDs) With Action condition.

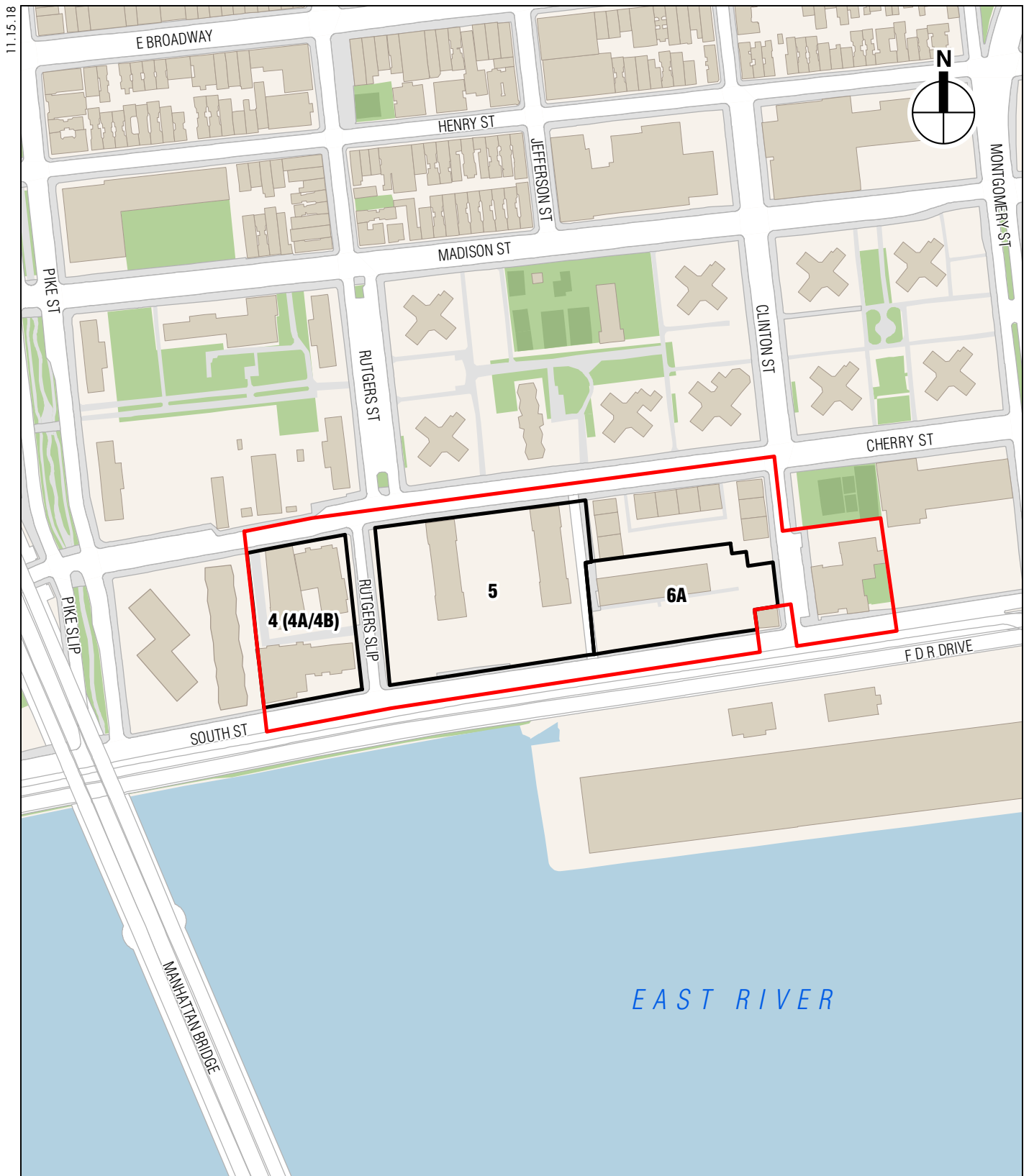
Table 14-3
Future with the Proposed Projects (RWCDs)

| Site | Components | Future with the Proposed Projects (With Action) |
|-----------|--------------------------|---|
| 4 (4A/4B) | Residential (DU) | 660 |
| | Local Retail (gsf) | 3,124 |
| 5 | Residential (DU) | 1,350 |
| | Local Retail (gsf) | 5,319 |
| | Community Facility (gsf) | 17,028 |
| 6A | Residential (DU) | 765 |
| | Local Retail (gsf) | 2,415 |

Note: The programs noted above do not include existing uses on the three sites that would remain in the With Action condition.

LEVEL 1 SCREENING ASSESSMENT

A Level 1 trip generation screening assessment was conducted to estimate the numbers of person and vehicle trips by mode expected to be generated by the proposed projects during the weekday AM, midday, and PM peak hours. These estimates were then compared to the *CEQR Technical*



- Project Sites
- Boundary of Two Bridges LSRD

0 400 FEET

Manual thresholds to determine if a Level 2 screening and/or quantified operational analyses would be warranted.

TRANSPORTATION PLANNING ASSUMPTIONS

Trip generation factors for the proposed projects were developed based on information from the *CEQR Technical Manual*, U.S. Census Data, and other established sources and approved studies, as summarized in **Table 14-4**.

Table 14-4
Travel Demand Assumptions

| Use | Residential | | | Local Retail | | | Community Facility Students | | | Community Facility Parents | | | Community Facility Staff | | |
|--|---|-------|-------|--|-------|-------|---|-------|-------|--------------------------------------|-------|-------|--|-------|-------|
| Total Daily Person Trip | (1) Weekday 8.075 Trips/DU | | | (1) Weekday 205 Trips/1000 SF | | | (1) Weekday 2.0 trips/person | | | (1) Weekday 4.0 trip/person | | | (1) Weekday 2.0 trips/person | | |
| Trip Linkage | 0% | | | 25% | | | 0% | | | 0% | | | 0% | | |
| Net Daily Person trip | Weekday 8.075 Trips/DU | | | Weekday 153.75 Trips/1000 SF | | | Weekday 2.0 Trips/Student | | | Weekday 4.0 Trips/Student | | | Weekday 2.0 Trips/Staff | | |
| Temporal | AM | MD | PM | AM | MD | PM | AM | MD | PM | AM | MD | PM | AM | MD | PM |
| | (1) | | | (1) | | | (1) | | | (1) | | | (1) | | |
| | 10% | 5% | 11% | 3% | 19% | 10% | 49.5% | 0% | 49.5% | 49.5% | 0% | 49.5% | 40% | 0% | 40% |
| Direction In Out Total | (2) | | | (2) | | | (4) | | | (4) | | | (4) | | |
| | 15% | 50% | 70% | 50% | 50% | 50% | 100% | 0% | 0% | 50% | 0% | 50% | 100% | 0% | 0% |
| | 85% | 50% | 30% | 50% | 50% | 50% | 0% | 0% | 100% | 50% | 0% | 50% | 0% | 0% | 100% |
| Modal Split | (3) | | | (2) | | | (4) | | | (5)(8) | | | (6) | | |
| | AM | MD | PM | AM | MD | PM | AM | MD | PM | AM | MD | PM | AM | MD | PM |
| | 14.0% | 14.0% | 14.0% | 2.0% | 2.0% | 2.0% | 10.0% | 10.0% | 10.0% | 0.0% | 0.0% | 0.0% | 18.0% | 18.0% | 18.0% |
| Auto | 5.0% | 5.0% | 5.0% | 3.0% | 3.0% | 3.0% | 2.0% | 2.0% | 2.0% | 0.0% | 0.0% | 0.0% | 1.0% | 1.0% | 1.0% |
| Taxi | 44.0% | 44.0% | 44.0% | 6.0% | 6.0% | 6.0% | 8.0% | 8.0% | 8.0% | 23.0% | 23.0% | 23.0% | 58.0% | 58.0% | 58.0% |
| Subway | 4.0% | 4.0% | 4.0% | 6.0% | 6.0% | 6.0% | 7.0% | 7.0% | 7.0% | 20.0% | 20.0% | 20.0% | 10.0% | 10.0% | 10.0% |
| Bus | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 53.0% | 53.0% | 53.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% | 0.0% |
| School Bus | 33.0% | 33.0% | 33.0% | 83.0% | 83.0% | 83.0% | 20.0% | 20.0% | 20.0% | 57.0% | 57.0% | 57.0% | 13.0% | 13.0% | 13.0% |
| Walk | 100% | 100% | 100% | 100% | 100% | 100% | 100% | 100% | 100% | 100% | 100% | 100% | 100% | 100% | 100% |
| Total | | | | | | | | | | | | | | | |
| Vehicle Occupancy | (2)(3) Weekday 1.30 1.40 N/A | | | (2) Weekday 1.65 1.40 N/A | | | (8) Weekday 1.30 1.30 35.0 | | | | | | (6)(7) Weekday 1.27 1.27 N/A | | |
| Auto | | | | | | | | | | | | | | | |
| Taxi | | | | | | | | | | | | | | | |
| School Bus | | | | | | | | | | | | | | | |
| Daily Delivery Trip Generation Rate | (1) Weekday 0.06 Delivery Trips/DU | | | (1) Weekday 0.35 Delivery Trips/KSF | | | (8) Weekday 0.03 Delivery Trips/students | | | | | | | | |
| Delivery Temporal | AM | MD | PM | AM | MD | PM | AM | MD | PM | | | | | | |
| | (1) | | | (1) | | | (8) | | | | | | | | |
| Delivery Direction | (1) | | | (1) | | | (8) | | | | | | | | |
| | 50% | 50% | 50% | 50% | 50% | 50% | 50% | 50% | 50% | | | | | | |
| | 50% | 50% | 50% | 50% | 50% | 50% | 50% | 50% | 50% | | | | | | |
| Total | 100% | 100% | 100% | 100% | 100% | 100% | 100% | 100% | 100% | | | | | | |
| Sources: | | | | | | | | | | | | | | | |
| (1) 2014 <i>CEQR Technical Manual</i> | | | | | | | | | | | | | | | |
| (2) <i>Seward Park Mixed-Use Development Project FGEIS</i> (2012) | | | | | | | | | | | | | | | |
| (3) U.S. Census Bureau, ACS 2011–2015 Five-Year Estimates—Journey-to-Work (JTW) Data for Census Tract 2.01, 6, 8, 14.01, and 16 | | | | | | | | | | | | | | | |
| (4) <i>Seward Park Mixed-Use Development Tech Memo</i> (2012) | | | | | | | | | | | | | | | |
| (5) Assumes 1 parent for every 1.30 students taking subway, bus, and walk modes to the school and the same temporal distribution as students | | | | | | | | | | | | | | | |
| (6) U.S. Census Bureau Reverse-Journey to Work ACS 2006–2010 five-year estimates | | | | | | | | | | | | | | | |
| (7) The staff taxi occupancy is assumed to be the same as the staff vehicle occupancy | | | | | | | | | | | | | | | |
| (8) East New York Rezoning FEIS (2016) | | | | | | | | | | | | | | | |

Residential

The daily person trip rate and temporal distribution for the residential component were obtained from the *CEQR Technical Manual*. Peak period Journey-to-Work (JTW) data from the 2011–2015 U.S. Census Bureau American Community Survey (ACS) for Manhattan census tracts 2.01, 6, 8, 14.01, and 16 were used for residential modal splits. The directional distribution for all peak periods is from the *Seward Park Mixed-Use Development Project FGEIS*. The vehicle occupancies are from the 2011–2015 U.S. Census ACS for autos and from the *Seward Park Mixed-Use Development Project FGEIS* for taxis. The daily delivery trip rate and temporal and directional distributions are from the *CEQR Technical Manual*.

Local Retail

The daily person trip generation and temporal distribution for the local neighborhood retail component were obtained from the *CEQR Technical Manual*. In line with accepted City practice, a 25 percent linked trip credit was applied to the local retail trip generation estimates. The directional distribution, modal splits, vehicle occupancies for all peak periods were obtained from the *Seward Park Mixed-Use Development Project FGEIS*. The daily delivery trip rate and temporal and directional distributions are from the *CEQR Technical Manual*.

Community Facility—Students

The daily person trip generation rate and temporal distribution for students of the potential early childhood educational facility assumed for the proposed community facility space on Site 5 were obtained from the *CEQR Technical Manual*. The directional distribution and modal splits were obtained from the *Seward Park Mixed-Use Development Tech Memo*. The vehicle occupancies, daily delivery trip rate, and temporal and directional distributions are from the *East New York Rezoning FEIS*.

Community Facility—Parents

The daily person trip generation rate and temporal distribution for parents of the potential early childhood educational facility assumed for the proposed community facility space on Site 5 were obtained from the *CEQR Technical Manual*. In line with typical SCA elementary school assumptions, it is anticipated that one parent would accompany every 1.28 students travelling by transit or walking to the school. The directional distribution is from the *Seward Park Mixed-Use Development Tech Memo*.

Community Facility—Staff

The daily person trip generation rate and temporal distribution for staff of the potential early childhood educational facility assumed for the proposed community facility space on Site 5 were obtained from the *CEQR Technical Manual*. Vehicle occupancies and modal splits are based on Reverse Journey-to-Work (RJTW) data from the 2006–2010 ACS.

TRAVEL DEMAND PROJECTION SUMMARY

As summarized in **Table 14-5**, in the future with the proposed projects, a total of 2,475, 1,442, and 2,815 person trips would be generated during the weekday AM, midday, and PM peak hours, respectively. Correspondingly, 435, 214, and 424 vehicle trips would be generated during the same respective peak hours.

Table 14-5
Trip Generation Summary: With Action Condition

| | Program | Peak Hour | In/Out | Person Trip | | | | | | | Vehicle Trip | | | | |
|--------|------------------------------------|-----------|--------|-------------|------|--------|-----|------------|------|-------|--------------|------|------------|----------|-------|
| | | | | Auto | Taxi | Subway | Bus | School Bus | Walk | Total | Auto | Taxi | School Bus | Delivery | Total |
| Site 4 | Residential 660 DUs | AM | In | 11 | 4 | 35 | 3 | 0 | 26 | 79 | 8 | 17 | 0 | 2 | 27 |
| | | | Out | 63 | 23 | 199 | 18 | 0 | 149 | 452 | 48 | 17 | 0 | 2 | 67 |
| | | | Total | 74 | 27 | 234 | 21 | 0 | 175 | 531 | 56 | 34 | 0 | 4 | 94 |
| | | Midday | In | 19 | 7 | 59 | 5 | 0 | 44 | 134 | 15 | 8 | 0 | 2 | 25 |
| | | | Out | 19 | 7 | 59 | 5 | 0 | 44 | 134 | 15 | 8 | 0 | 2 | 25 |
| | | | Total | 38 | 14 | 118 | 10 | 0 | 88 | 268 | 30 | 16 | 0 | 4 | 50 |
| | Local Retail 3,124 gsf | PM | In | 57 | 21 | 181 | 16 | 0 | 135 | 410 | 44 | 15 | 0 | 0 | 59 |
| | | | Out | 25 | 9 | 77 | 7 | 0 | 58 | 176 | 19 | 15 | 0 | 0 | 34 |
| | | | Total | 82 | 30 | 258 | 23 | 0 | 193 | 586 | 63 | 30 | 0 | 0 | 93 |
| | | AM | In | 0 | 0 | 0 | 0 | 0 | 6 | 6 | 0 | 0 | 0 | 0 | 0 |
| | | | Out | 0 | 0 | 0 | 0 | 0 | 6 | 6 | 0 | 0 | 0 | 0 | 0 |
| | | | Total | 0 | 0 | 0 | 0 | 0 | 12 | 12 | 0 | 0 | 0 | 0 | 0 |
| Site 5 | Residential 1,350 DUs | Midday | In | 1 | 1 | 3 | 3 | 0 | 38 | 46 | 1 | 1 | 0 | 0 | 2 |
| | | | Out | 1 | 1 | 3 | 3 | 0 | 38 | 46 | 1 | 1 | 0 | 0 | 2 |
| | | | Total | 2 | 2 | 6 | 6 | 0 | 76 | 92 | 2 | 2 | 0 | 0 | 4 |
| | | PM | In | 0 | 1 | 1 | 1 | 0 | 20 | 23 | 0 | 1 | 0 | 0 | 1 |
| | | | Out | 0 | 1 | 1 | 1 | 0 | 20 | 23 | 0 | 1 | 0 | 0 | 1 |
| | | | Total | 0 | 2 | 2 | 2 | 0 | 40 | 46 | 0 | 2 | 0 | 0 | 2 |
| | Local Retail 5,319 gsf | AM | In | 23 | 8 | 72 | 7 | 0 | 54 | 164 | 18 | 35 | 0 | 5 | 58 |
| | | | Out | 130 | 46 | 408 | 37 | 0 | 306 | 927 | 100 | 35 | 0 | 5 | 140 |
| | | | Total | 153 | 54 | 480 | 44 | 0 | 360 | 1,091 | 118 | 70 | 0 | 10 | 198 |
| | | Midday | In | 38 | 14 | 120 | 11 | 0 | 90 | 273 | 29 | 15 | 0 | 4 | 48 |
| | | | Out | 38 | 14 | 120 | 11 | 0 | 90 | 273 | 29 | 15 | 0 | 4 | 48 |
| | | | Total | 76 | 28 | 240 | 22 | 0 | 180 | 546 | 58 | 30 | 0 | 8 | 96 |
| | Community Facility 118 Students | PM | In | 118 | 42 | 369 | 34 | 0 | 277 | 840 | 91 | 29 | 0 | 1 | 121 |
| | | | Out | 50 | 18 | 158 | 14 | 0 | 119 | 359 | 38 | 29 | 0 | 1 | 68 |
| | | | Total | 168 | 60 | 527 | 48 | 0 | 396 | 1,199 | 129 | 58 | 0 | 2 | 189 |
| | Community Facility 32 Parents | AM | In | 0 | 0 | 1 | 1 | 0 | 10 | 12 | 0 | 0 | 0 | 0 | 0 |
| | | | Out | 0 | 0 | 1 | 1 | 0 | 10 | 12 | 0 | 0 | 0 | 0 | 0 |
| | | | Total | 0 | 0 | 2 | 2 | 0 | 20 | 24 | 0 | 0 | 0 | 0 | 0 |
| | | Midday | In | 2 | 2 | 5 | 5 | 0 | 64 | 78 | 1 | 1 | 0 | 0 | 2 |
| | | | Out | 2 | 2 | 5 | 5 | 0 | 64 | 78 | 1 | 1 | 0 | 0 | 2 |
| | | | Total | 4 | 4 | 10 | 10 | 0 | 128 | 156 | 2 | 2 | 0 | 0 | 4 |
| | Community Facility 12 Staff | PM | In | 1 | 1 | 2 | 2 | 0 | 34 | 40 | 1 | 1 | 0 | 0 | 2 |
| | | | Out | 1 | 1 | 2 | 2 | 0 | 34 | 40 | 1 | 1 | 0 | 0 | 2 |
| | | | Total | 2 | 2 | 4 | 4 | 0 | 68 | 80 | 2 | 2 | 0 | 0 | 4 |
| | Community Facility 12 Staff | AM | In | 12 | 2 | 9 | 8 | 62 | 23 | 116 | 9 | 2 | 2 | 0 | 13 |
| | | | Out | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 9 | 2 | 2 | 0 | 13 |
| | | | Total | 12 | 2 | 9 | 8 | 62 | 23 | 116 | 18 | 4 | 4 | 0 | 26 |
| | | Midday | In | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | | | Out | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | | | Total | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | Community Facility 12 Staff | PM | In | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 9 | 1 | 2 | 0 | 12 |
| | | | Out | 12 | 2 | 9 | 8 | 62 | 23 | 116 | 9 | 1 | 2 | 0 | 12 |
| | | | Total | 12 | 2 | 9 | 8 | 62 | 23 | 116 | 18 | 2 | 4 | 0 | 24 |
| | Community Facility 12 Staff | AM | In | 0 | 0 | 7 | 6 | 0 | 18 | 31 | 0 | 0 | 0 | 0 | 0 |
| | | | Out | 0 | 0 | 7 | 6 | 0 | 18 | 31 | 0 | 0 | 0 | 0 | 0 |
| | | | Total | 0 | 0 | 14 | 12 | 0 | 36 | 62 | 0 | 0 | 0 | 0 | 0 |
| | | Midday | In | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | | | Out | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | | | Total | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | Community Facility 12 Staff | PM | In | 0 | 0 | 7 | 6 | 0 | 18 | 31 | 0 | 0 | 0 | 0 | 0 |
| | | | Out | 0 | 0 | 7 | 6 | 0 | 18 | 31 | 0 | 0 | 0 | 0 | 0 |
| | | | Total | 0 | 0 | 14 | 12 | 0 | 36 | 62 | 0 | 0 | 0 | 0 | 0 |
| | Community Facility 12 Staff | AM | In | 2 | 0 | 6 | 1 | 0 | 1 | 10 | 2 | 0 | 0 | 0 | 2 |
| | | | Out | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | | | Total | 2 | 0 | 6 | 1 | 0 | 1 | 10 | 2 | 0 | 0 | 0 | 2 |
| | | Midday | In | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | | | Out | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | | | Total | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | Community Facility 12 Staff | PM | In | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | | | Out | 2 | 0 | 6 | 1 | 0 | 1 | 10 | 2 | 0 | 0 | 0 | 2 |
| | | | Total | 2 | 0 | 6 | 1 | 0 | 1 | 10 | 2 | 0 | 0 | 0 | 2 |

Table 14-5 (cont'd)

Trip Generation Summary: With Action Condition

| | Program | Peak Hour | In/Out | Person Trip | | | | | | | Vehicle Trip | | | | |
|-------------|---------------------------|-----------|--------|-------------|------|--------|-----|------------|-------|-------|--------------|------|------------|----------|-------|
| | | | | Auto | Taxi | Subway | Bus | School Bus | Walk | Total | Auto | Taxi | School Bus | Delivery | Total |
| Site 6A | Residential 765 DUs | AM | In | 13 | 5 | 41 | 4 | 0 | 31 | 94 | 10 | 21 | 0 | 3 | 34 |
| | | | Out | 74 | 26 | 231 | 21 | 0 | 173 | 525 | 57 | 21 | 0 | 3 | 81 |
| | | | Total | 87 | 31 | 272 | 25 | 0 | 204 | 619 | 67 | 42 | 0 | 6 | 115 |
| | | Midday | In | 22 | 8 | 68 | 6 | 0 | 51 | 155 | 17 | 9 | 0 | 2 | 28 |
| | | | Out | 22 | 8 | 68 | 6 | 0 | 51 | 155 | 17 | 9 | 0 | 2 | 28 |
| | | | Total | 44 | 16 | 136 | 12 | 0 | 102 | 310 | 34 | 18 | 0 | 4 | 56 |
| | Local Retail 2,415 gsf | PM | In | 67 | 24 | 209 | 19 | 0 | 157 | 476 | 52 | 17 | 0 | 0 | 69 |
| | | | Out | 29 | 10 | 90 | 8 | 0 | 67 | 204 | 22 | 17 | 0 | 0 | 39 |
| | | | Total | 96 | 34 | 299 | 27 | 0 | 224 | 680 | 74 | 34 | 0 | 0 | 108 |
| | | AM | In | 0 | 0 | 0 | 0 | 0 | 5 | 5 | 0 | 0 | 0 | 0 | 0 |
| | | | Out | 0 | 0 | 0 | 0 | 0 | 5 | 5 | 0 | 0 | 0 | 0 | 0 |
| | | | Total | 0 | 0 | 0 | 0 | 0 | 10 | 10 | 0 | 0 | 0 | 0 | 0 |
| Grand Total | | AM | In | 1 | 1 | 2 | 2 | 0 | 29 | 35 | 1 | 1 | 0 | 0 | 2 |
| | | | Out | 1 | 1 | 2 | 2 | 0 | 29 | 35 | 1 | 1 | 0 | 0 | 2 |
| | | | Total | 2 | 2 | 4 | 4 | 0 | 60 | 72 | 2 | 2 | 0 | 0 | 4 |
| | | Midday | In | 0 | 1 | 1 | 1 | 0 | 15 | 18 | 0 | 1 | 0 | 0 | 1 |
| | | | Out | 0 | 1 | 1 | 1 | 0 | 15 | 18 | 0 | 1 | 0 | 0 | 1 |
| | | | Total | 0 | 2 | 2 | 2 | 0 | 32 | 36 | 0 | 2 | 0 | 0 | 2 |
| | | PM | In | 61 | 19 | 171 | 30 | 62 | 174 | 517 | 47 | 75 | 2 | 10 | 134 |
| | | | Out | 267 | 95 | 846 | 83 | 0 | 667 | 1,958 | 214 | 75 | 2 | 10 | 301 |
| | | | Total | 328 | 114 | 1,017 | 113 | 62 | 841 | 2,475 | 261 | 150 | 4 | 20 | 435 |
| | | Midday | In | 83 | 33 | 257 | 32 | 0 | 316 | 721 | 64 | 35 | 0 | 8 | 107 |
| | | | Out | 83 | 33 | 257 | 32 | 0 | 316 | 721 | 64 | 35 | 0 | 8 | 107 |
| | | | Total | 166 | 66 | 514 | 64 | 0 | 632 | 1,442 | 128 | 70 | 0 | 16 | 214 |
| | | PM | In | 243 | 90 | 770 | 79 | 0 | 656 | 1,838 | 197 | 65 | 2 | 1 | 265 |
| | | | Out | 119 | 42 | 351 | 48 | 62 | 355 | 977 | 91 | 65 | 2 | 1 | 159 |
| | | | Total | 362 | 132 | 1,121 | 127 | 62 | 1,011 | 2,815 | 288 | 130 | 4 | 2 | 424 |

TRAFFIC

As shown in **Table 14-5**, the incremental trips generated by the proposed projects would be 435, 214, and 424 vehicle trips during the weekday AM, midday, and PM peak hours, respectively. Since the incremental vehicle trips would be greater than 50 vehicles during the weekday AM, midday, and PM peak hours, a Level 2 screening assessment (presented in the section below) was conducted to determine if a quantified traffic analysis is warranted.

TRANSIT

As shown in **Table 14-5**, the incremental subway trips generated by the proposed projects would be 1,017, 514, and 1,121 person trips during the weekday AM, midday, and PM peak hours, respectively. Since the incremental subway trips would be greater than 200 during the weekday AM and PM peak hours and the majority of these trips would be expected to use the East Broadway Station (F line), a detailed analysis of subway facilities at this station and line-haul conditions on the F line is warranted.

As detailed in **Table 14-5**, the incremental bus trips generated by the proposed projects would be 113, 64, and 127 person trips during the weekday AM, midday, and PM peak hours, respectively. Considering that these trips would be further dispersed among the multiple local bus routes serving the study area, including the M9, M15, M15 Select Bus Service (SBS), and M22, no single bus route would incur incremental trips exceeding the *CEQR Technical Manual* analysis threshold of 50 or more peak hour bus riders in a single direction. Therefore, a detailed bus line-haul analysis would not be warranted, and the proposed projects are not expected to result in any significant adverse bus line-haul impacts.

PEDESTRIANS

All incremental person trips generated by the proposed projects would traverse the pedestrian elements (i.e., sidewalks, corners, and crosswalks) surrounding the project sites. As shown in **Table 14-5**, the net incremental pedestrian trips would be greater than 200 during the weekday AM, midday, and PM peak hours. A Level 2 screening assessment (presented in the section below) was conducted to determine if there is a need for additional quantified pedestrian analyses.

LEVEL 2 SCREENING ASSESSMENT

As part of the Level 2 screening assessment, project-generated trips were assigned to specific intersections and pedestrian elements near the project sites. As previously stated, further quantified analyses to assess the potential impacts of the proposed projects on the transportation system would be warranted if the trip assignments were to identify key intersections incurring 50 or more peak hour vehicle-trips or pedestrian elements incurring 200 or more peak hour pedestrian-trips. Similarly, for transit elements, the projected trips were considered in determining the likely transit facilities requiring a detailed analysis of potential impacts.

SITE ACCESS AND EGRESS

For Site 4 (4A/4B), the proposed building entrance would be located on the south side of Cherry Street between Pike Street and Rutgers Slip, and on the west side of Rutgers Slip between Cherry Street and South Street. For Site 5, the proposed building entrances would be located on the south side of Cherry Street between Rutgers Slip and Clinton Street, and the north side of South Street between Rutgers Slip and Clinton Street. For Site 6A, the proposed building entrances would be located on the west side of Clinton Street between Cherry Street and South Street, and on the north side of South Street between Rutgers Slip and Clinton Street.

TRAFFIC

As shown in **Table 14-5**, incremental vehicle trips resulting from the proposed projects would exceed the CEQR Level-1 screening threshold during the weekday AM, midday, and PM peak hours. These vehicle trips were assigned to study area intersections based on the most likely travel routes to and from the project sites, prevailing travel patterns, commuter origin-destination (O-D) summaries from the census data, and configuration of the roadway network. Since available parking spaces at off-site parking facilities within a ¼-mile are expected to be insufficient to accommodate the proposed projects' anticipated parking demand, project-generated trips were also assigned to parking resources between ¼-mile and ½-mile distance from the project sites. Non-pick-up and drop-off auto trips were assigned to the parking facilities summarized in Section H, "Parking Assessment," (excluding No. 1 and No. 2, as these facilities are planned for redevelopment). Taxi trips were assigned to the various project sites' frontages along South Street, Rutgers Street, and Clinton Street. All delivery trips were assigned to the project sites via the New York City Department of Transportation (DOT) designated truck routes. Traffic assignments for autos, taxis, and deliveries for the various development uses are discussed below.

Residential

Auto trips generated by the proposed residential uses were assigned to the surrounding roadway network based on the 2006–2010 U.S. Census ACS JTW origin-destination estimates. Many of the residential trips would be traveling to work destinations within the local region of Manhattan

(31 percent), with the remaining trips traveling to Brooklyn (17 percent), New Jersey (17 percent), Queens (11 percent), Upstate New York, and others (10 percent), Staten Island (8 percent), the Bronx (4 percent), and Long Island (2 percent). Residential trips would originate from off-site parking facilities to which project-generated trips were assigned and use the most direct routes for travel to their destinations. Overall, vehicle trips generated by the proposed residential uses were distributed to the study area roadway network in the following manner: approximately 34 percent assigned to points north of the project sites, 30 percent to points west, 24 percent to points southeast, and 12 percent to points east. The majority of trips traveling to Brooklyn and Staten Island south were assigned to the FDR Drive, with the remaining trips utilizing West Street, the Manhattan Bridge, the Queensboro Bridge, the Queens-Midtown Tunnel, the Williamsburg Bridge, and the Brooklyn Bridge, as well as Allen Street and Canal Street. Vehicles heading to New Jersey, Pennsylvania, and Manhattan west of the project sites were assigned primarily to South Street and Worth Street. Eastbound trips to Queens and Long Island were assigned to the Queensboro Bridge, Queen-Midtown Tunnel, and the Williamsburg Bridge. Vehicles traveling to Manhattan north of the project site, the Bronx, and Upstate were assigned to the FDR Drive and West Street.

Community Facility

The proposed community facility use is expected to serve patrons primarily from the immediate area. Therefore, auto trips were generally assigned from local origins within the neighborhood and adjacent residential areas. Overall, the vehicle trips generated by the proposed community facility use were distributed to the study area roadway network in the following manner: approximately 35 percent assigned to points north of the project site, 35 percent to points east, and 30 percent to points southeast.

Local Retail

The proposed local retail uses are expected to also serve patrons primarily from the immediate area, following the same general distribution described above for the community facility. Travel to the various off-site parking options would occur via the major roadways surrounding the project sites, including the Bowery, Allen Street, and Grand Street.

Taxis

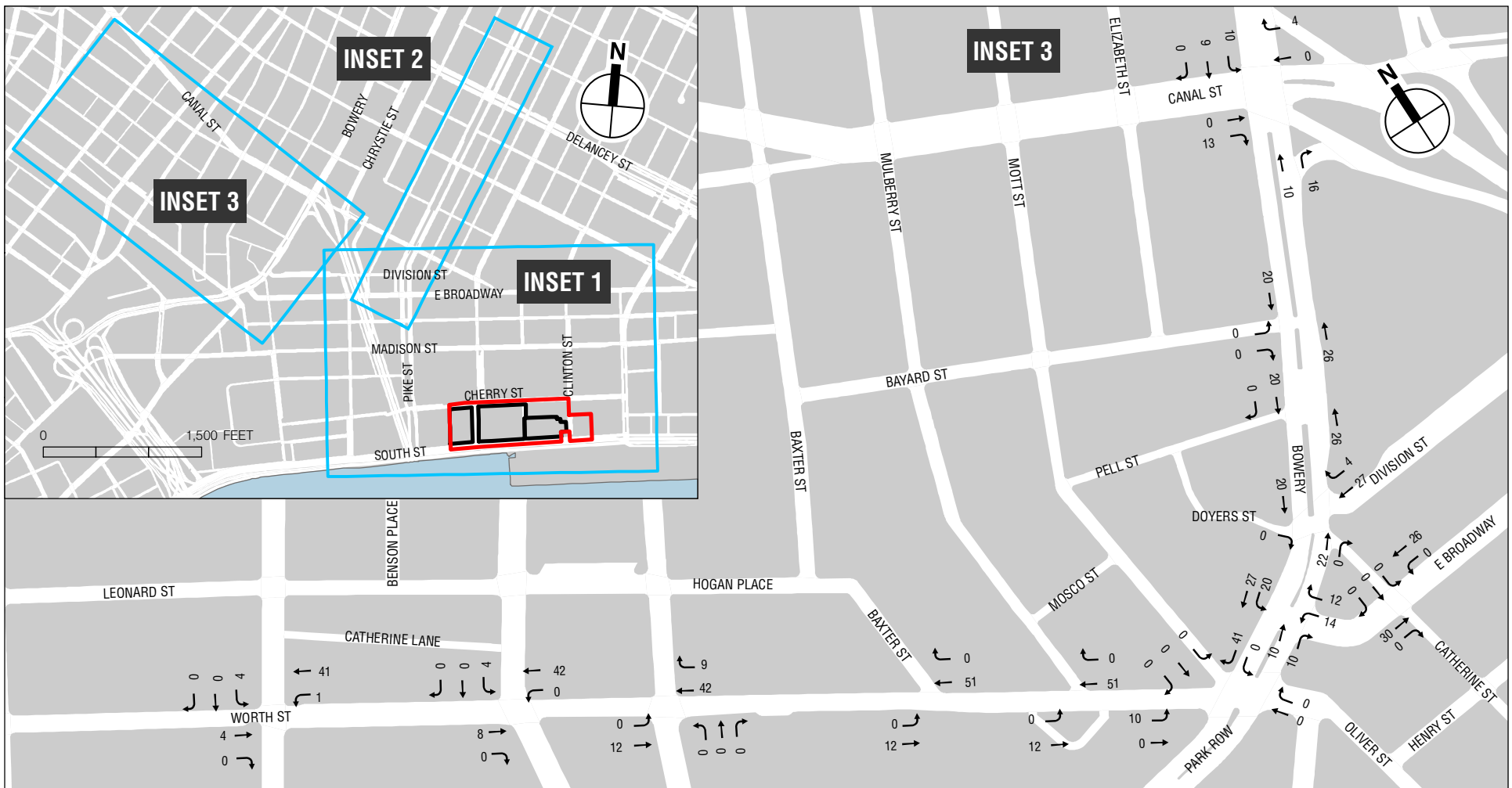
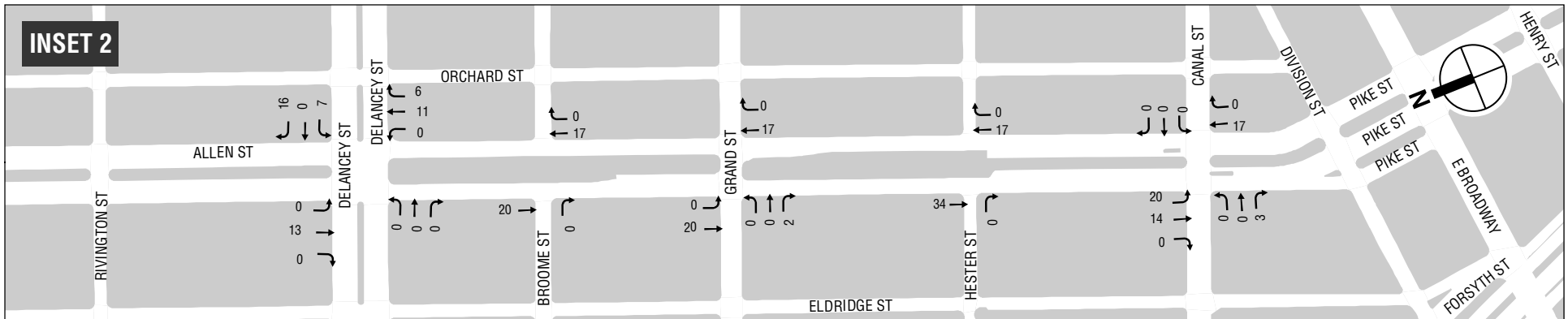
Taxi pick-ups and drop-offs for the proposed residential components were split among the project sites' frontages along South Street, Rutgers Street, and Clinton Street. Taxi trips for the proposed local retail components were assigned to the Cherry Street and Rutgers Street curbsides facing the sites. All taxi trips for the proposed community facility were assigned to the South Street curbside in front of Site 5.

Deliveries

Truck delivery trips for all land uses were assigned to DOT-designated truck routes as long as possible until reaching the area surrounding the project sites. These trips were then distributed primarily along South Street and Cherry Street.

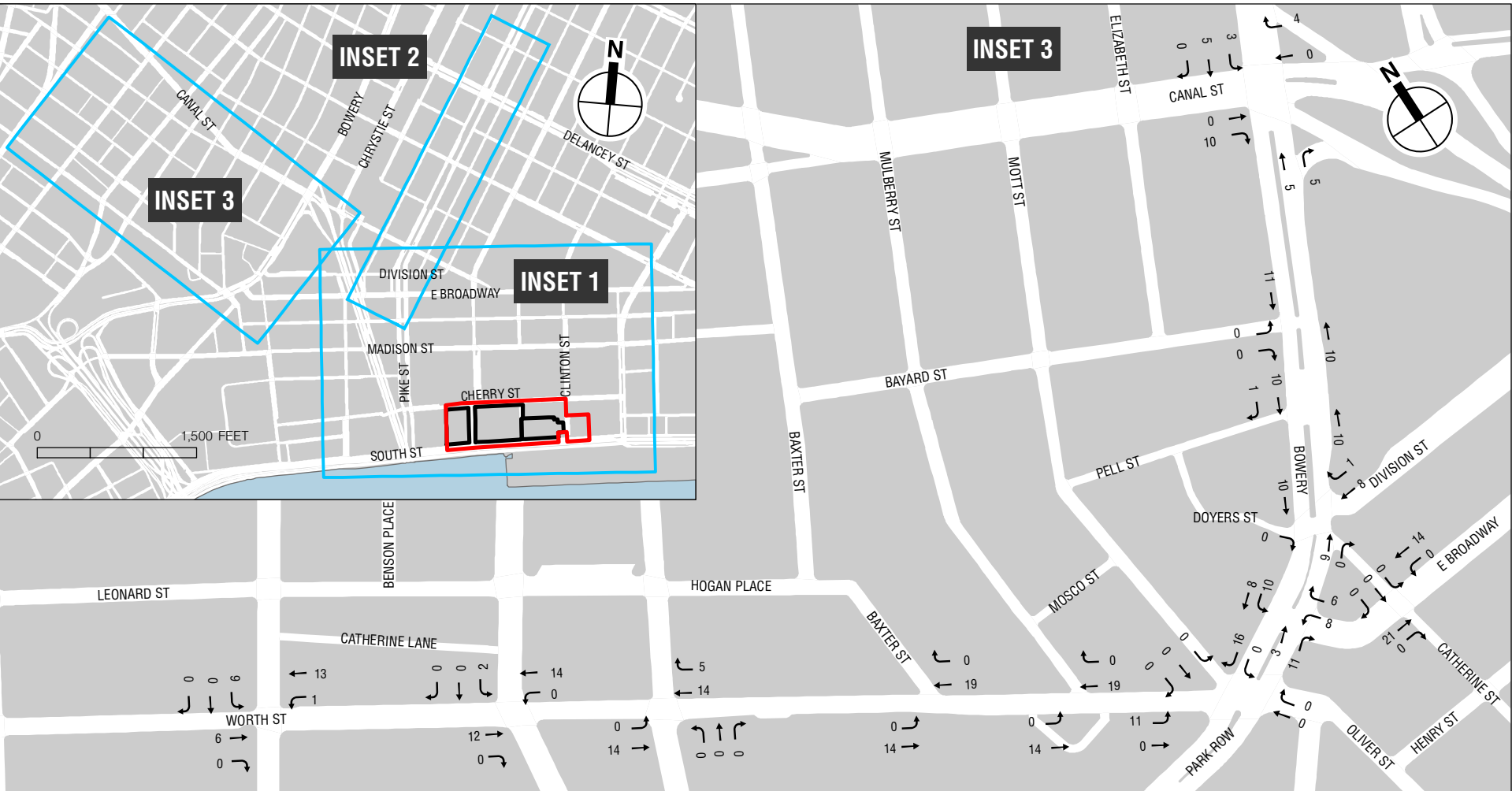
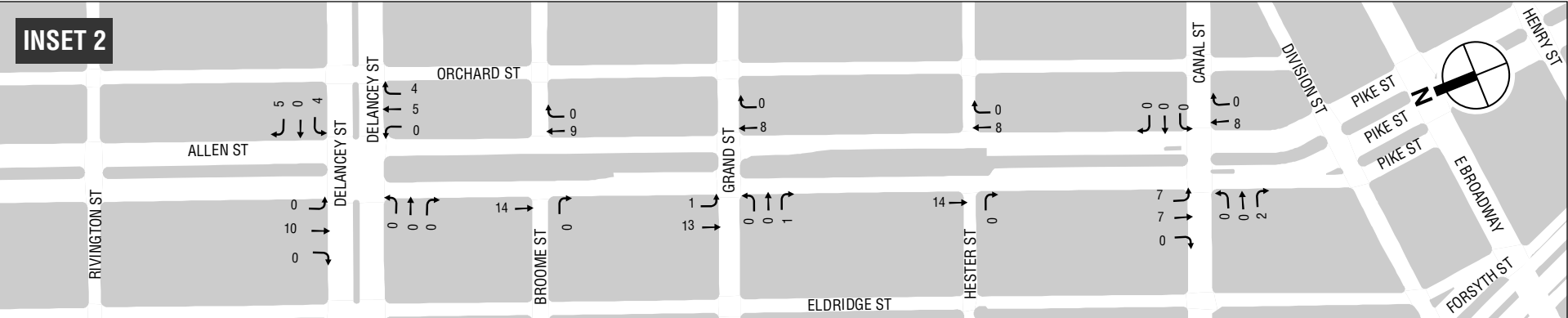
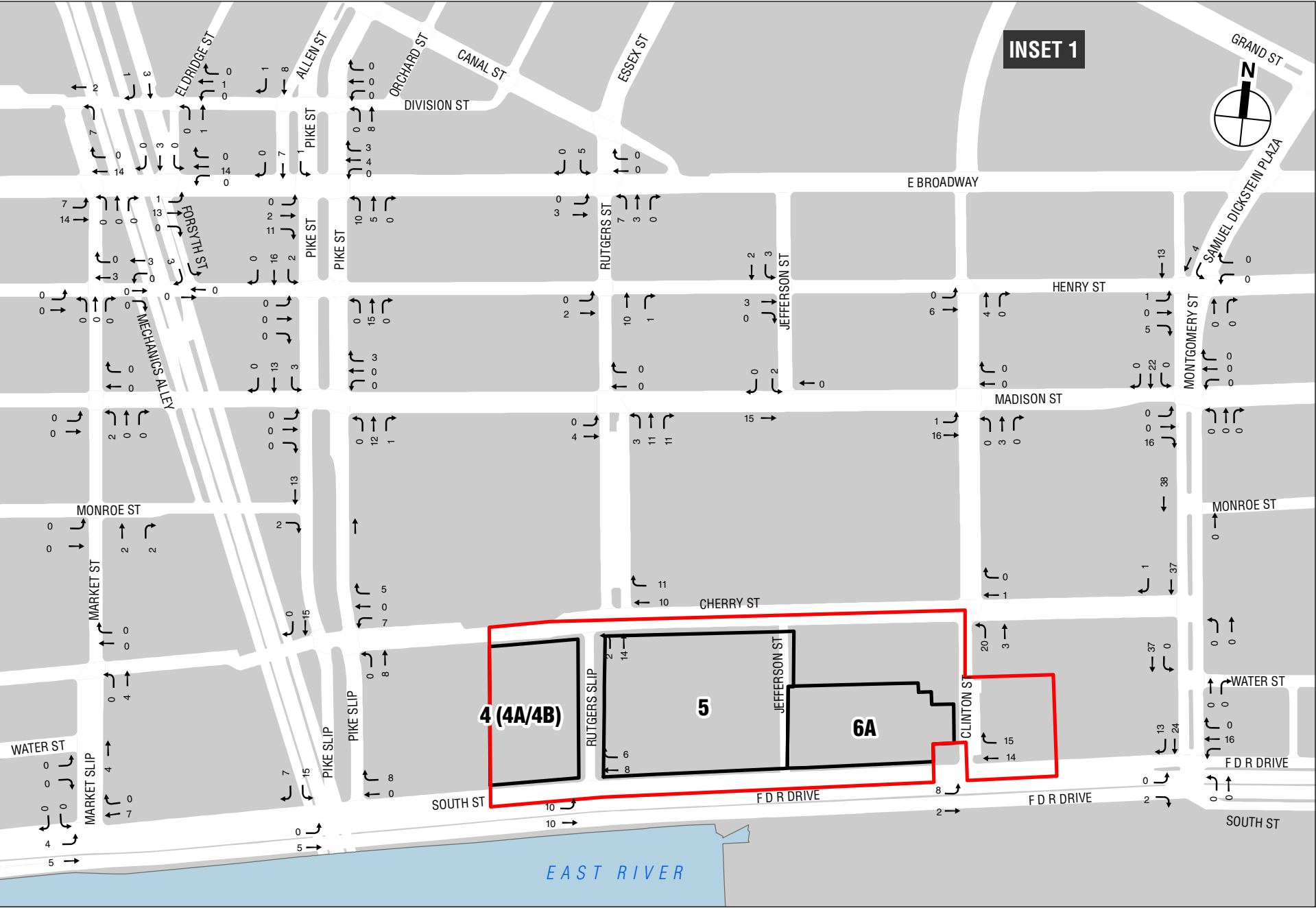
Summary

As shown in **Figures 14-2 through 14-4** and summarized in **Table 14-6**, 31 intersections comprising the traffic study area have been selected for analysis, in consultation with DOT, based on the volume of trips projected and turning movements anticipated to occur at those locations. The selected traffic analysis locations are shown in **Figure 14-5**.



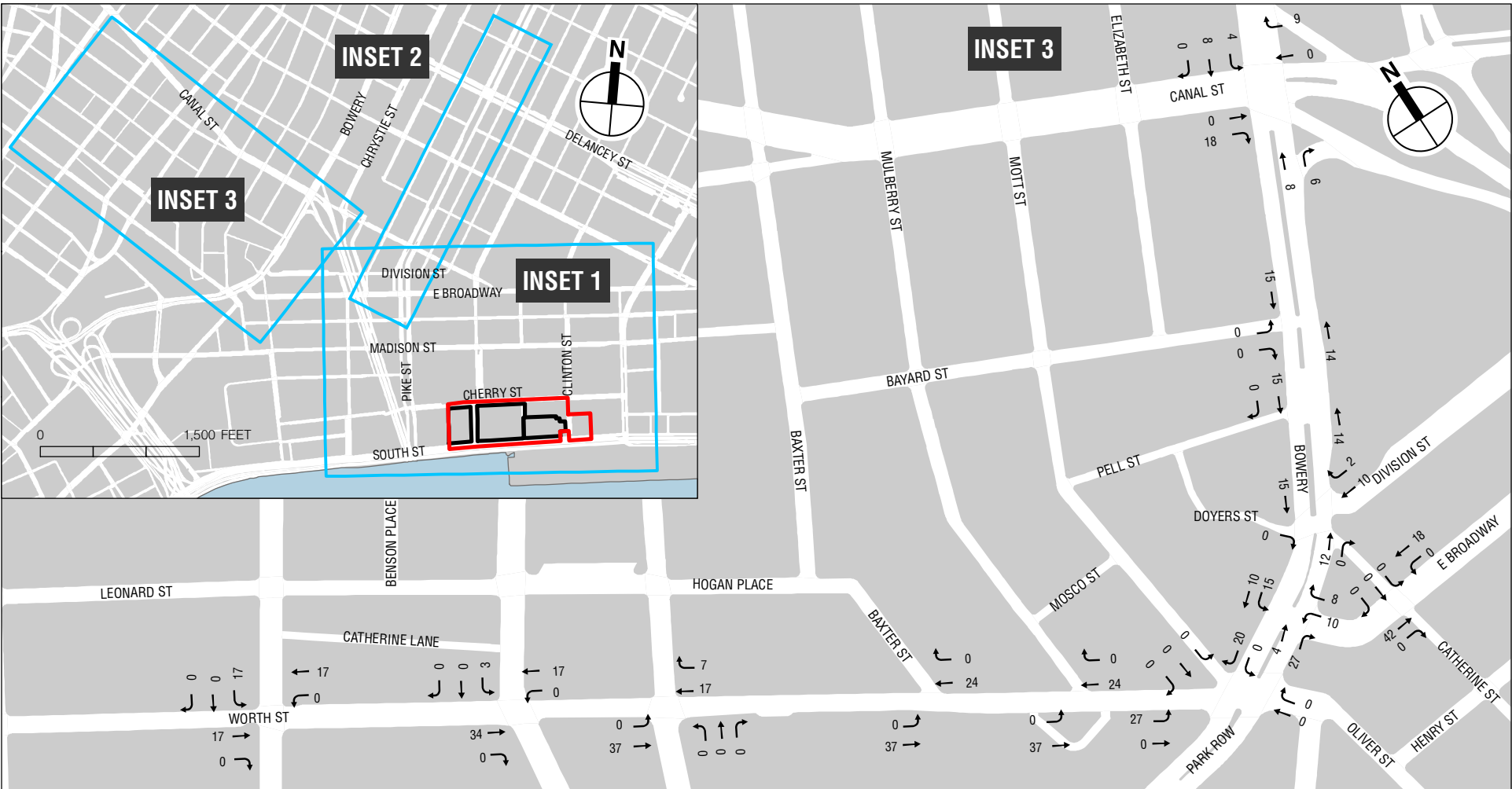
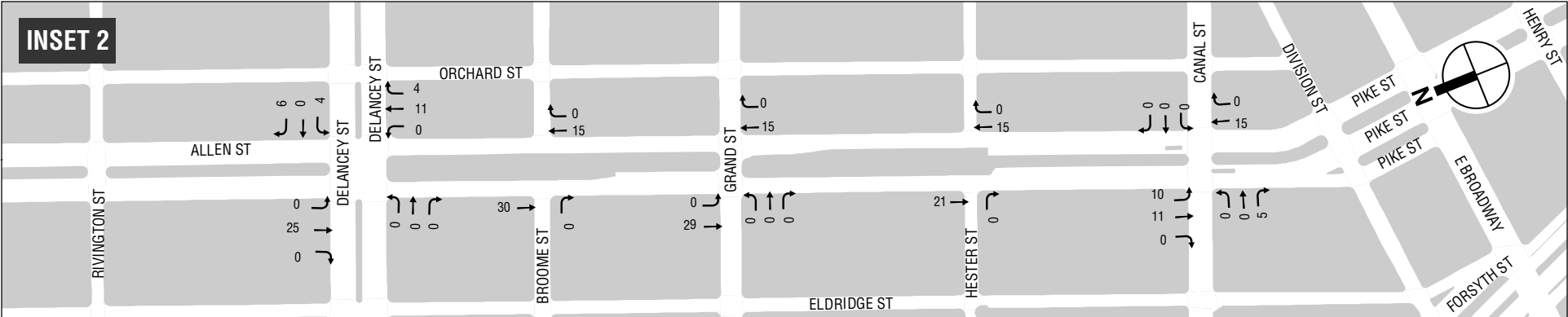
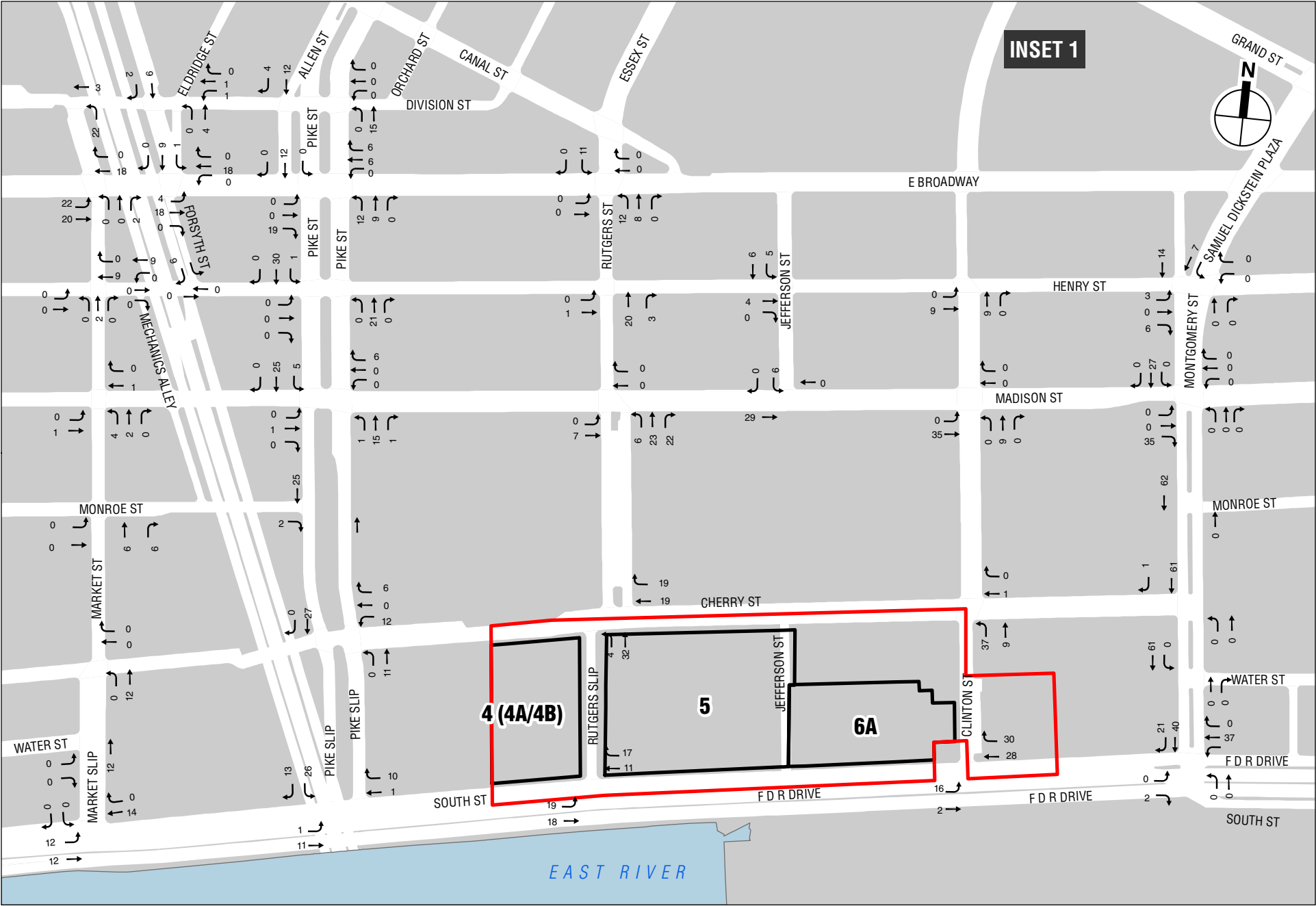
 Project Sites
 Boundary of Two Bridges LSRD

0 400 FEET



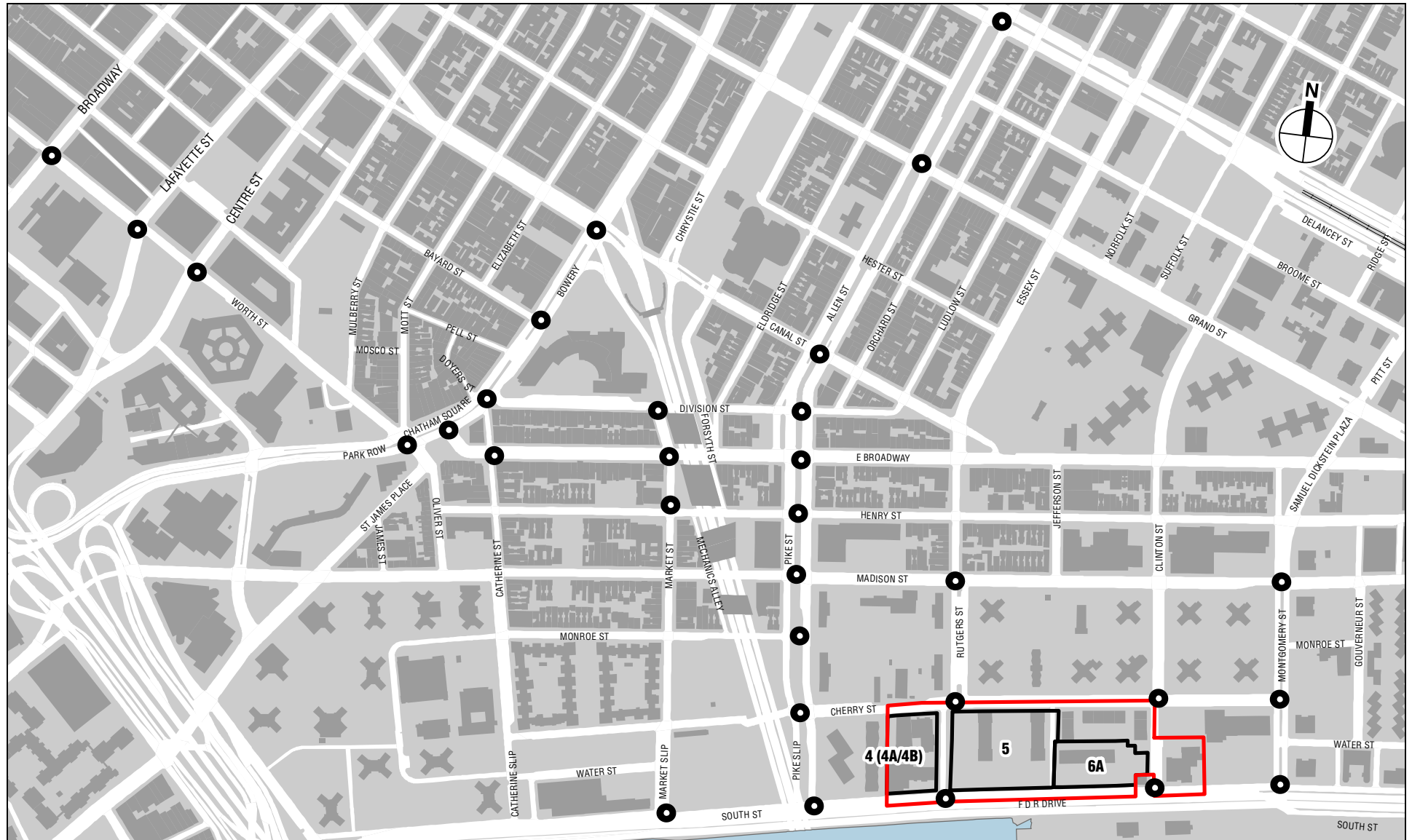
 Project Sites
 Boundary of Two Bridges LSRD

0 400 FEET



Project Sites
 Boundary of Two Bridges LSRD

0 400 FEET



- Project Sites
- Boundary of Two Bridges LSRD
- Traffic Analysis Location

TWO BRIDGES LSRD

0 1,000 FEET

Traffic Analysis Locations
Figure 14-5

Table 14-6

Traffic Level 2 Screening Analysis Results – Selected Analysis Locations

| Traffic Intersections | AM | MD | PM | Analysis Location |
|--|-----|----|-----|-------------------|
| Grand Street and the Bowery | 34 | 18 | 33 | |
| Grand Street and Allen Street | 39 | 23 | 44 | ✓ |
| Hester Street and the Bowery | 33 | 17 | 29 | |
| Hester Street and Pike Street | 51 | 22 | 36 | |
| Canal Street/Manhattan Bridge Entrance (BK) and the Bowery | 62 | 32 | 53 | ✓ |
| Canal Street and Manhattan Bridge Lower Level | 4 | 4 | 9 | |
| Canal Street and Manhattan Bridge Upper Level/ Chrystie Street | 5 | 5 | 14 | |
| Canal Street and Forsyth Street | 5 | 5 | 14 | |
| Canal Street and Eldridge Street | 3 | 2 | 5 | |
| Canal Street and Allen Street | 54 | 24 | 41 | ✓ |
| The Bowery and Bayard Street | 46 | 21 | 29 | ✓ |
| Pell Street and the Bowery | 46 | 21 | 29 | |
| Division Street and the Bowery | 73 | 28 | 39 | ✓ |
| Division Street and Market Street | 10 | 9 | 25 | ✓ |
| Division Street and Forsyth Street/Eldridge Street | 11 | 6 | 17 | |
| Division Street and Allen Street | 34 | 17 | 31 | ✓ |
| Worth Street/Oliver Street and Chatham Square | 61 | 30 | 51 | ✓ |
| Chatham Square and East Broadway | 93 | 46 | 74 | ✓ |
| East Broadway and Catherine Street | 56 | 35 | 60 | ✓ |
| East Broadway and Market Street | 56 | 35 | 62 | ✓ |
| East Broadway and Forsyth Street | 56 | 31 | 50 | |
| East Broadway and Allen Street | 86 | 43 | 64 | ✓ |
| East Broadway and EssExcept Street | 40 | 18 | 31 | |
| Henry Street and Market Street | 2 | 3 | 11 | ✓ |
| Henry Street and Mechanics Alley | 2 | 3 | 9 | |
| Henry Street and Forsyth Street | 2 | 3 | 9 | |
| Henry Street and Pike Street | 69 | 33 | 52 | ✓ |
| Henry Street and Rutgers Street | 31 | 13 | 24 | |
| Henry Street and Jefferson Street | 20 | 8 | 15 | |
| Henry Street and Clinton Street | 17 | 10 | 18 | |
| Henry Street and Montgomery Street | 48 | 19 | 23 | |
| Madison Street and Market Street | 3 | 2 | 8 | |
| Madison Street and Mechanics Alley | 2 | 0 | 2 | |
| Madison Street and Pike Street | 70 | 32 | 54 | ✓ |
| Madison Street and Rutgers Street | 72 | 29 | 58 | ✓ |
| Madison Street and Jefferson Street | 45 | 17 | 35 | |
| Madison Street and Clinton Street | 48 | 20 | 44 | |
| Madison Street and Montgomery Street | 103 | 38 | 62 | ✓ |
| Monroe Street and Market Street | 2 | 4 | 12 | |
| Monroe Street and Mechanics Alley | 1 | 2 | 6 | |
| Monroe Street and Pike Street | 59 | 28 | 44 | ✓ |
| Monroe Street/ Catherine Street and Montgomery Street | 103 | 38 | 62 | |
| Cherry Street and Market Street | 2 | 4 | 12 | |
| Cherry Street and Pike Street | 78 | 35 | 56 | ✓ |
| Cherry Street and Rutgers Street | 79 | 37 | 74 | ✓ |
| Cherry Street and Clinton Street | 43 | 24 | 47 | ✓ |
| Cherry Street and Montgomery Street | 103 | 38 | 62 | ✓ |
| Water Street and Market Street | 2 | 4 | 12 | |
| Water Street and Montgomery Street | 103 | 37 | 61 | |
| South Street and Market Street | 36 | 16 | 38 | ✓ |
| South Street and Pike Street | 83 | 35 | 62 | ✓ |
| South Street and Rutgers Street | 81 | 34 | 65 | ✓ |
| South Street and Clinton Street | 87 | 39 | 76 | ✓ |
| South Street/ FDR North Ramp and Montgomery Street | 138 | 55 | 100 | ✓ |
| Worth Street and Church Street | 45 | 19 | 34 | |
| Worth Street and Broadway | 50 | 26 | 51 | ✓ |
| Worth Street and Lafayette Street | 54 | 28 | 54 | ✓ |
| Worth Street and Centre Street | 63 | 33 | 61 | ✓ |
| Worth Street and Baxter Street | 63 | 33 | 61 | |
| Worth Street and Mulberry Street | 63 | 33 | 61 | |
| Delancey Street and Allen Street | 53 | 28 | 50 | ✓ |
| Broome Street and Allen Street | 37 | 23 | 45 | |
| Note: ✓ denotes intersections recommended for detailed traffic analysis | | | | |

TRANSIT

As stated above, the Level 1 trip generation estimates showed that detailed station and line-haul analyses would be warranted for the East Broadway Station and for the F line, respectively. The residential use accounts for the majority of trips generated by the proposed projects, of which, 95 percent of subway riders were assigned to the East Broadway station (F train). The remaining 5 percent were assigned to the Grand Street Station (B and D trains), which provides service to sections of Brooklyn and the Bronx that are not captured by the F train. The same assignment patterns were applied to the community facility staff trips. For subway trips made to/from the retail uses and by community facility parents and students, 100 percent were assigned to the East Broadway Station.

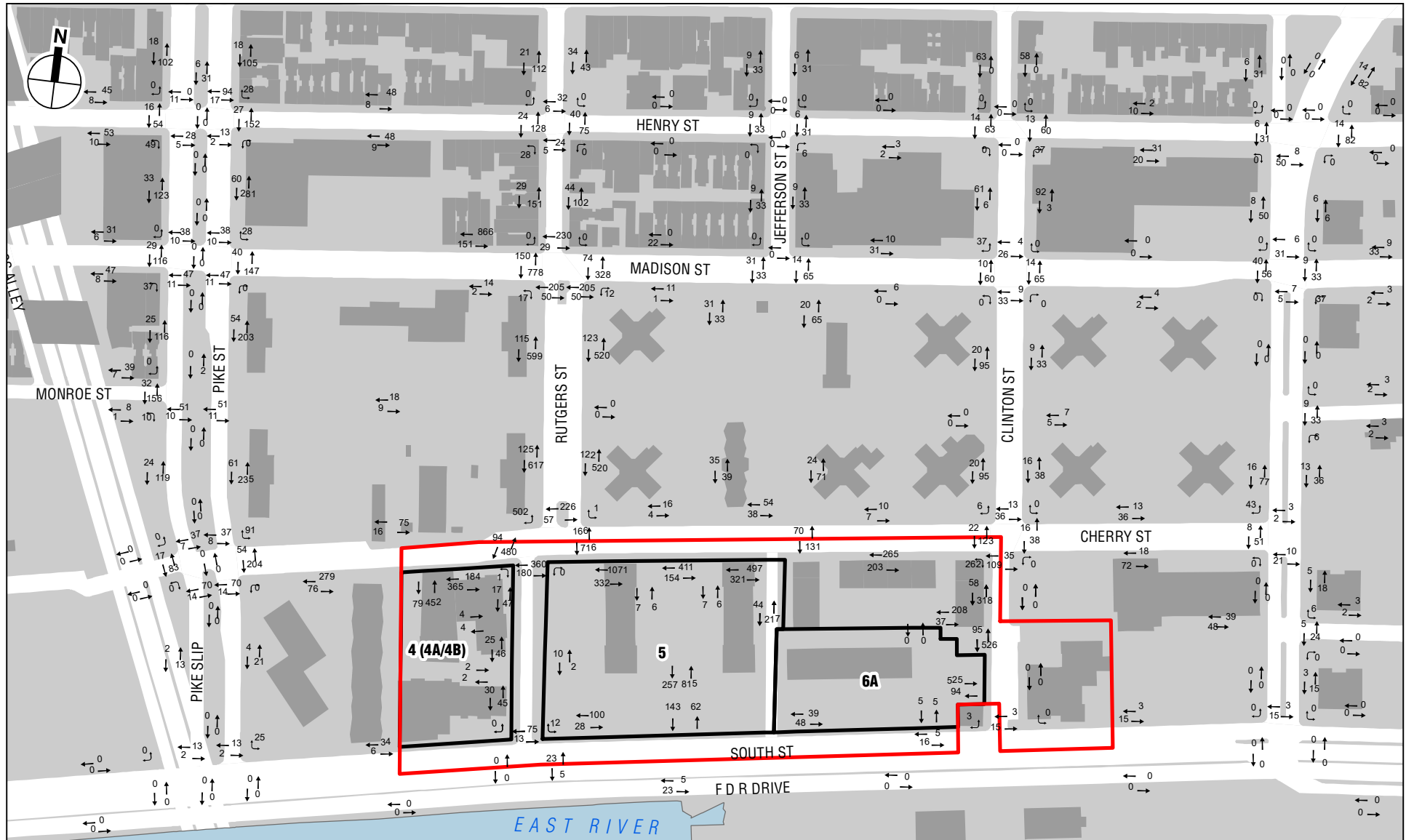
The same subway assignment patterns were applied to the AM and PM peak periods. However, slight variations in inbound and outbound patterns were assumed with respect to the use of specific station entrances. For the inbound F train subway trips, 80 percent were assumed to use the entrance at the northwest corner of Rutgers Street and Madison Street, with the remainder exiting at the Rutgers Street and East Broadway entrances for local shopping before continuing to the project sites. For outbound F train subway trips, 100 percent were assumed to use the nearest entrance to the project sites, which is located at the northwest corner of Rutgers Street and Madison Street.

PEDESTRIANS

All person trips generated by the proposed projects would traverse the pedestrian elements (i.e., sidewalks, corners, and crosswalks) surrounding the project sites. As shown in **Table 14-5**, the net incremental pedestrian trips would be greater than 200 during the weekday AM, midday, and PM peak hours. A Level 2 screening assessment was conducted to identify specific pedestrian elements that are expected to incur 200 or more peak hour pedestrian-trips and which would be subject to a detailed analysis of potential pedestrian impacts.

- **Auto Trips**—Motorists would park at the nearby off-site parking facilities and travel along the area intersections to enter the project sites via adjacent sidewalks.
- **Taxi Trips**—Taxi users would get dropped off and picked up near the entrances of the project sites.
- **Bus Trips**—Bus riders would use numerous area bus routes (M9, M15 local, M15 SBS, and M22) and would get on and off at the bus stops located in the vicinity of the project sites.
- **Subway Trips**—The majority of the project-generated subway riders were assigned to the East Broadway (F line) station. A small portion was assigned to Grand Street (B and D) station.
- **Walk-Only Trips**—Pedestrian walk-only trip assignments were developed by reviewing the proposed projects' various land uses and population distribution within walking distance from the project sites and distributing the walk-only person trips to surrounding pedestrian facilities, including sidewalks, corner reservoirs, and crosswalks.

Based on the detailed assignment of pedestrian trips, shown in **Figures 14-6 through 14-8**, 18 sidewalks, 16 corner reservoirs, and 12 crosswalks were selected, in consultation with DOT, for a detailed analysis of weekday peak hour conditions. These locations and associated trip increments are summarized in **Table 14-7** and depicted in **Figure 14-9**.

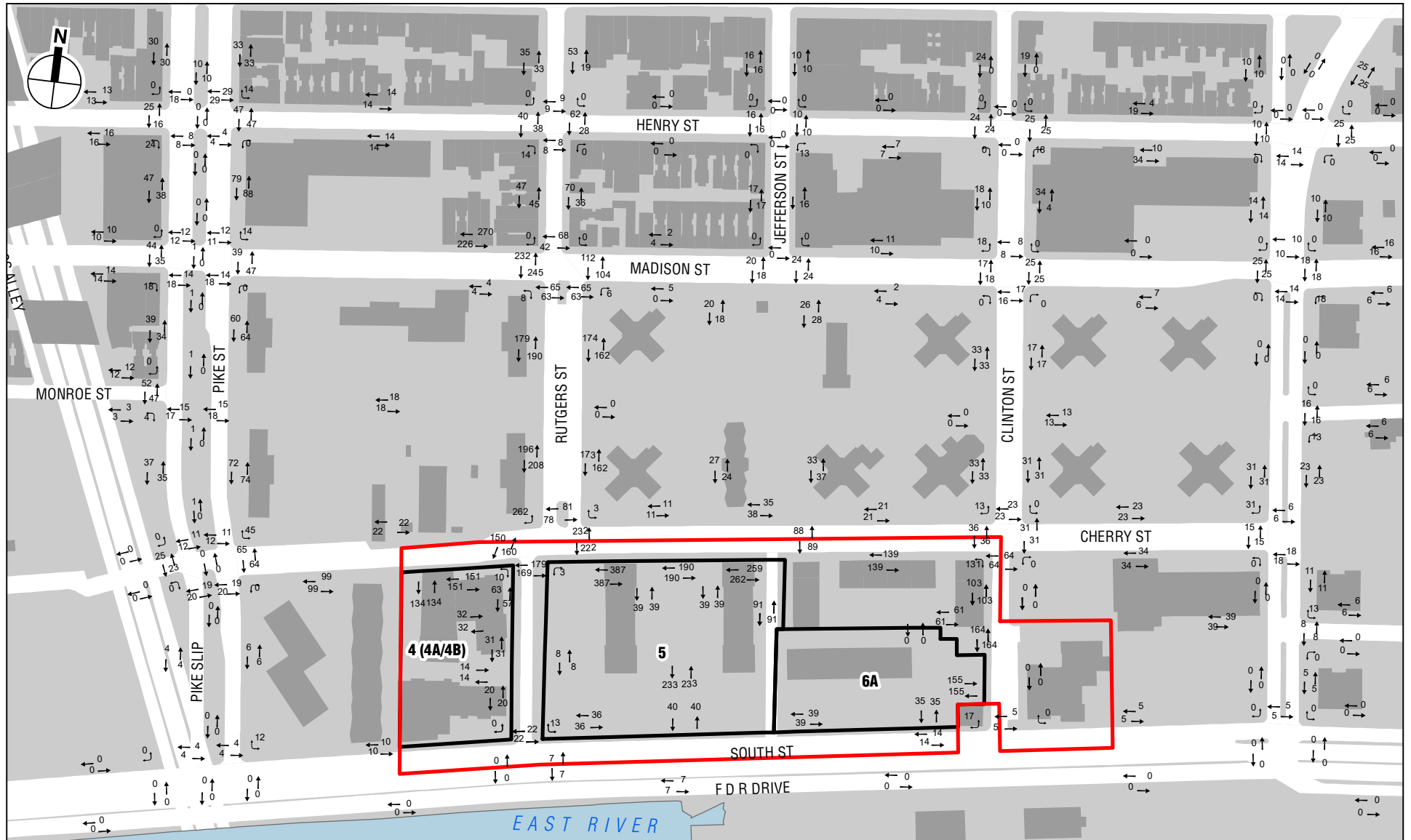


 Project Sites


 Boundary of Two Bridges LSRD

TWO BRIDGES LSRD

Proposed Projects Incremental Pedestrian Trips
Weekday AM Peak Hour
Figure 14-6

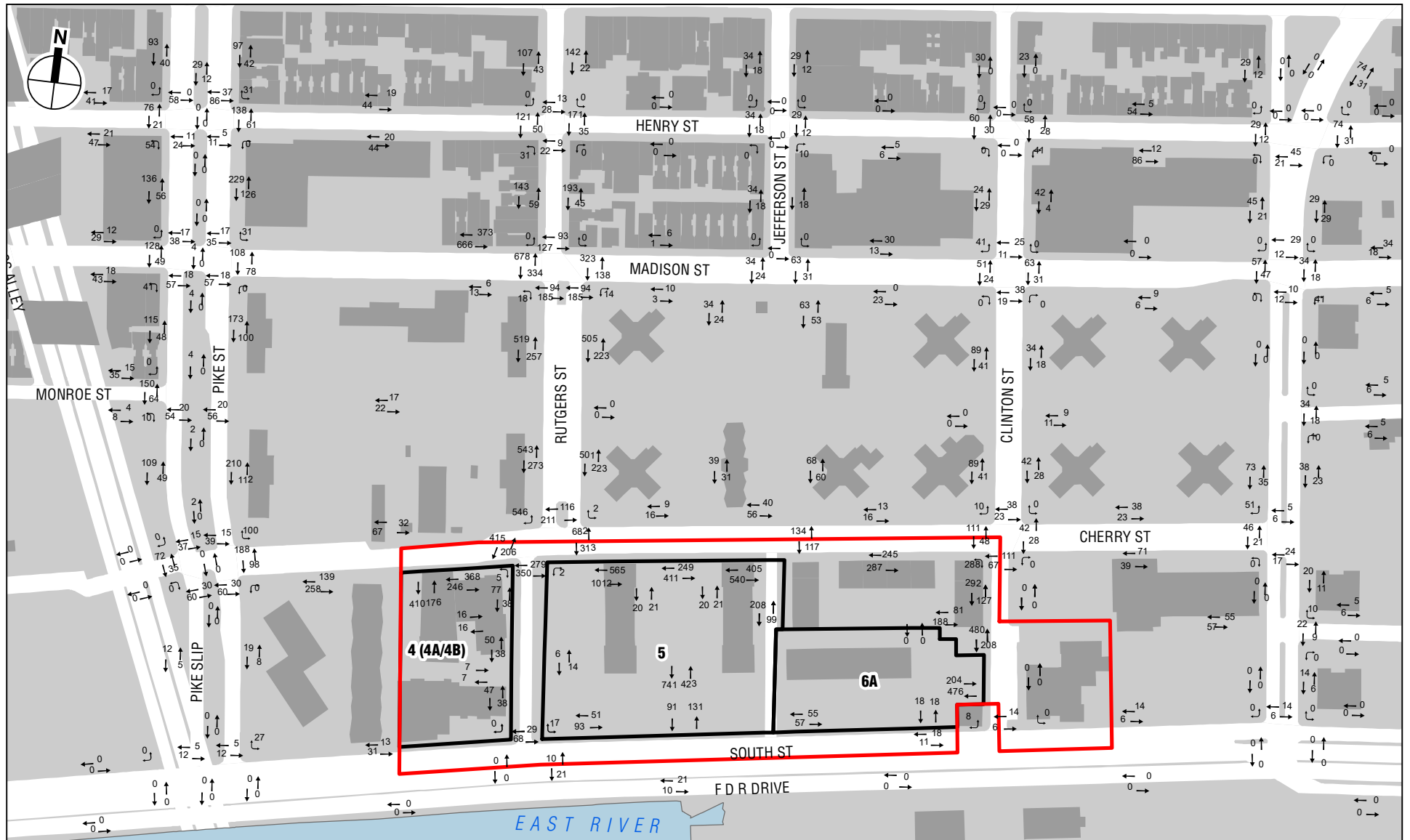


 Project Sites

 Boundary of Two Bridges LSRD

TWO BRIDGES LSRD

Proposed Projects Incremental Pedestrian Trips
Weekday Midday Peak Hour
Figure 14-7

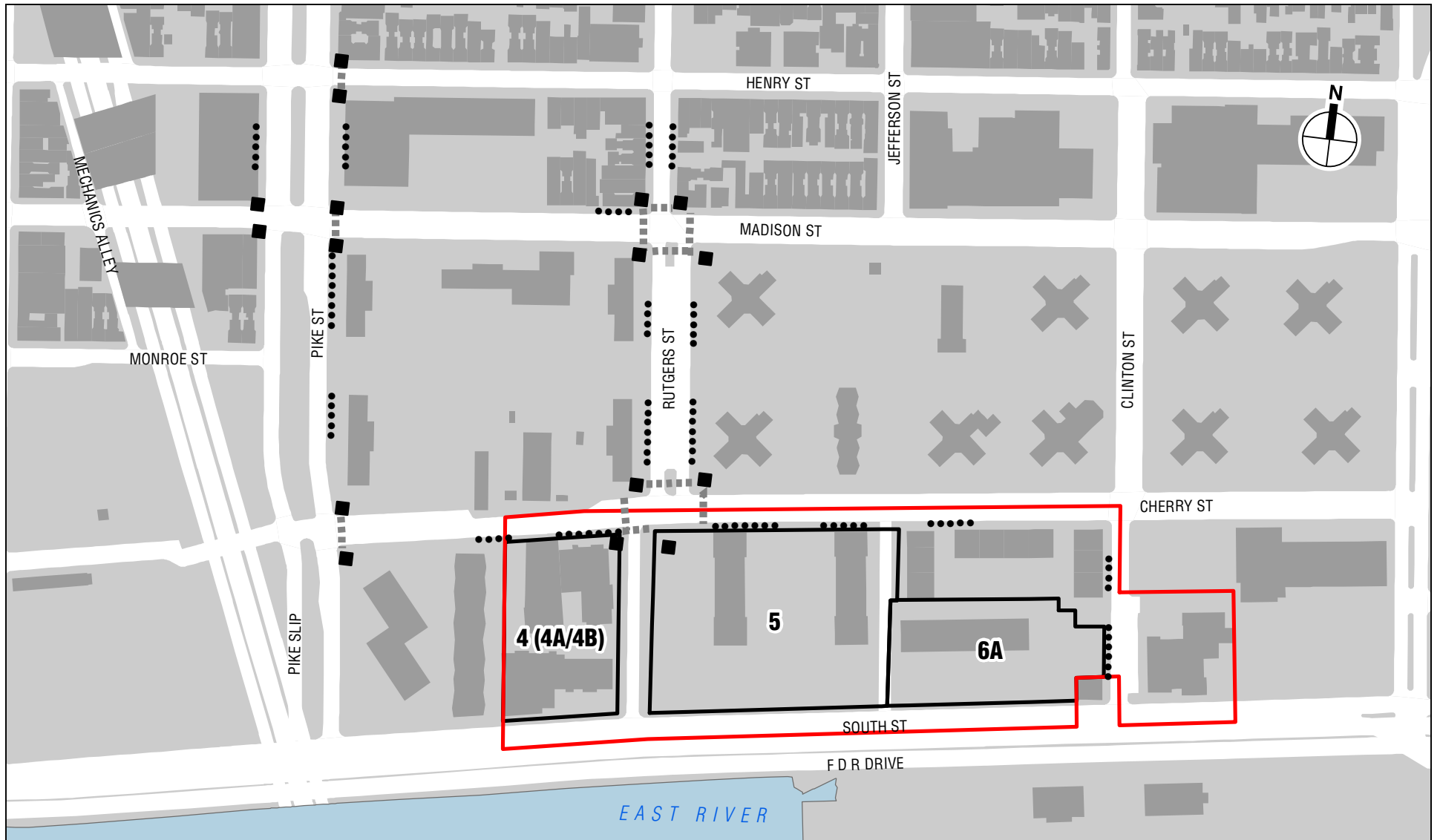


Project Sites

Boundary of Two Bridges LSRD

TWO BRIDGES LSRD

Proposed Projects Incremental Pedestrian Trips
Weekday PM Peak Hour
Figure 14-8



- Project Sites
- Sidewalk
- Boundary of Two Bridges LSRD
- Corner
- Crosswalk

TWO BRIDGES LSRD

Pedestrian Analysis Locations

Figure 14-9

Table 14-7

Pedestrian Level 2 Screening Analysis Results – Selected Analysis Locations

| Pedestrian Elements | AM | MD | PM |
|---|-------------|------------|-------------|
| Pike Street and Henry Street | | | |
| East Crosswalk | 179 | 94 | 199 |
| NE Corner | 318 | 166 | 353 |
| SE Corner | 194 | 102 | 215 |
| West Sidewalk between Madison Street and Henry Street | 156 | 85 | 192 |
| East Sidewalk between Madison Street and Henry Street | 341 | 167 | 355 |
| Rutgers Street and Henry Street | | | |
| East Sidewalk between Madison Street and Henry Street | 146 | 106 | 238 |
| West Sidewalk between Madison Street and Henry Street | 180 | 92 | 202 |
| Pike Street and Madison Street (West) | | | |
| SW Corner | 240 | 129 | 293 |
| NW Corner | 193 | 103 | 232 |
| Pike Street and Madison Street (East) | | | |
| East Sidewalk between Madison Street and Monroe Street | 257 | 124 | 273 |
| NE Corner | 263 | 123 | 269 |
| SE Corner | 245 | 118 | 261 |
| Rutgers Street and Madison Street | | | |
| North Crosswalk | 259 | 110 | 220 |
| East Crosswalk | 402 | 216 | 461 |
| South Crosswalk | 255 | 128 | 279 |
| West Crosswalk | 928 | 477 | 1012 |
| NE Corner | 661 | 326 | 681 |
| SE Corner | 669 | 350 | 754 |
| SW Corner | 1200 | 613 | 1309 |
| NW Corner | 1187 | 587 | 1232 |
| North Sidewalk between Rutgers Street and Pike Street | 1017 | 496 | 1039 |
| East Sidewalk between Madison Street and Monroe Street | 643 | 336 | 728 |
| West Sidewalk between Madison Street and Monroe Street | 714 | 369 | 776 |
| Pike Street and Monroe Street | | | |
| East Sidewalk between Monroe Street and Cherry Street | 296 | 146 | 322 |
| Pike Street and Cherry Street | | | |
| East Crosswalk | 258 | 129 | 286 |
| NE Corner | 394 | 197 | 440 |
| SE Corner | 342 | 168 | 376 |
| South Sidewalk between Pike Street and Site 4 (4A/4B) Residential Entrance | 355 | 198 | 397 |
| Rutgers Street/Frank T. Modica Way and Cherry Street | | | |
| North Crosswalk | 283 | 159 | 327 |
| East Crosswalk | 882 | 454 | 995 |
| South Crosswalk | 540 | 348 | 629 |
| West Crosswalk | 574 | 310 | 621 |
| NE Corner | 1166 | 616 | 1324 |
| SE Corner | 540 | 351 | 631 |
| SW Corner | 1115 | 668 | 1255 |
| NW Corner | 785 | 421 | 873 |
| East Sidewalk between Monroe Street and Cherry Street | 642 | 335 | 724 |
| South Sidewalk between Frank T. Modica Way and Site 5 Entrance | 1403 | 774 | 1577 |
| South Sidewalk (east) between Frank T. Modica Way and Site 4 (4A/4B) Residential Entrance | 549 | 302 | 614 |
| West Sidewalk between Cherry St and Monroe Street | 742 | 404 | 816 |
| Cherry Street and Jefferson Street | | | |
| South Sidewalk Between Site 5 Entrance and Clinton Street | 818 | 521 | 945 |
| Cherry Street and Clinton Street | | | |
| West Sidewalk (north) between Cherry Street and Plaza Entrance | 376 | 206 | 419 |
| South Sidewalk between Plaza entrance and Clinton St | 468 | 278 | 532 |
| South Street and Clinton Street | | | |
| West Sidewalk between Cherry Street and South Street | 621 | 328 | 688 |
| Note: Bold numbers indicate pedestrian incremental volumes are above analysis threshold of 200 | | | |

C. TRANSPORTATION ANALYSIS METHODOLOGIES

TRAFFIC OPERATIONS

The operations of all of the signalized and unsignalized intersections in the study area were assessed using methodologies presented in the *2000 Highway Capacity Manual (HCM)* using the *Highway Capacity Software (HCS+ 5.5)*. The HCM procedure evaluates the levels of service (LOS) for signalized and unsignalized intersections using average stop control delay, in seconds per vehicle, as described below.

SIGNALIZED INTERSECTIONS

The average control delay per vehicle is the basis for LOS determination for individual lane groups (grouping of movements in one or more travel lanes), the approaches, and the overall intersection. The levels of service are defined in **Table 14-8**.

Table 14-8
Level of Service Criteria for Signalized Intersections

| LOS | Average Control Delay |
|---|--------------------------|
| A | ≤ 10.0 seconds |
| B | >10.0 and ≤ 20.0 seconds |
| C | >20.0 and ≤ 35.0 seconds |
| D | >35.0 and ≤ 55.0 seconds |
| E | >55.0 and ≤ 80.0 seconds |
| F | >80.0 seconds |
| Source: Transportation Research Board. <i>Highway Capacity Manual</i> , 2000 | |

Although the HCM methodology calculates a volume-to-capacity (v/c) ratio, there is no strict relationship between v/c ratios and LOS as defined in the HCM. A high v/c ratio indicates substantial traffic passing through an intersection, but a high v/c ratio combined with low average delay actually represents the most efficient condition in terms of traffic engineering standards, where an approach or the whole intersection processes traffic close to its theoretical maximum capacity with minimal delay. However, very high v/c ratios—especially those approaching or greater than 1.0—are often correlated with a deteriorated LOS. Other important variables affecting delay include cycle length, progression, and green time. LOS A and B indicate good operating conditions with minimal delay. At LOS C, the number of vehicles stopping is higher, but congestion is still fairly light. LOS D describes a condition where congestion levels are more noticeable and individual cycle failures (a condition where motorists may have to wait for more than one green phase to clear the intersection) can occur. Conditions at LOS E and F reflect poor service levels, and cycle breakdowns are frequent. The HCM methodology also provides for a summary of the total intersection operating conditions. The analysis chooses the two critical movements (the worst case from each roadway) and calculates a summary critical v/c ratio. The overall intersection delay, which determines the intersection's LOS, is based on a weighted average of control delays of the individual lane groups. Within New York City, the midpoint of LOS D (45 seconds of delay) is generally considered as the threshold between acceptable and unacceptable operations.

Significant Impact Criteria

According to the criteria presented in the *CEQR Technical Manual*, impacts are considered significant and require examination of mitigation if they result in an increase in the With Action condition of 5 or more seconds of delay in a lane group over No Action levels beyond mid-LOS D. For No Action LOS E, a 4-second increase in delay is considered significant. For No Action LOS F, a 3-second increase in delay is considered significant. In addition, impacts are considered significant if levels of service deteriorate from acceptable A, B, or C in the No Action condition to marginally unacceptable LOS D (a delay in excess of 45 seconds, the midpoint of LOS D), or unacceptable LOS E or F in the With Action condition.

UNSIGNALIZED INTERSECTIONS

For unsignalized intersections, the average control delay is defined as the total elapsed time from which a vehicle stops at the end of the queue until the vehicle departs from the stop line. This includes the time required for the vehicle to travel from the last-in-queue to the first-in-queue position. The average control delay for any particular minor movement is a function of the service rate or capacity of the approach and the degree of saturation. The LOS criteria for unsignalized intersections are summarized in **Table 14-9**.

Table 14-9
Level of Service Criteria for Unsignalized Intersections

| LOS | Average Control Delay |
|-----|---------------------------|
| A | ≤ 10.0 seconds |
| B | > 10.0 and ≤ 15.0 seconds |
| C | > 15.0 and ≤ 25.0 seconds |
| D | > 25.0 and ≤ 35.0 seconds |
| E | > 35.0 and ≤ 50.0 seconds |
| F | > 50.0 seconds |

Source: Transportation Research Board. *Highway Capacity Manual*, 2000

The LOS thresholds for unsignalized intersections are different from those for signalized intersections. The primary reason is that drivers expect different levels of performance from different types of transportation facilities. The expectation is that a signalized intersection is designed to carry higher traffic volumes than an unsignalized intersection; hence, the corresponding control delays are higher at a signalized intersection than at an unsignalized intersection for the same LOS. In addition, certain driver behavioral considerations combine to make delays at signalized intersections less onerous than at unsignalized intersections. For example, drivers at signalized intersections are able to relax during the red interval, whereas drivers on minor approaches to unsignalized intersections must remain attentive to the task of identifying acceptable gaps and vehicle conflicts. Also, there is often much more variability in the amount of delay experienced by individual drivers at unsignalized intersections. For these reasons, the corresponding delay thresholds for unsignalized intersections are lower than those of signalized intersections. As with signalized intersections, within New York City, the midpoint of LOS D (30 seconds of delay) is generally perceived as the threshold between acceptable and unacceptable operations.

Significant Impact Criteria

The same sliding scale of significant delays described for signalized intersections applies for unsignalized intersections. For the minor street to trigger significant impacts, at least 90 passenger car equivalents (PCE) must be identified in the With Action condition in any peak hour.

TRANSIT OPERATIONS

SUBWAY STATION ELEMENTS

The methodology for assessing station circulation (stairs, escalators, and passageways) and fare control (regular turnstiles, high entry/exit turnstiles, and high exit turnstiles) elements compares the user volume with the analyzed element's design capacity, resulting in a v/c ratio. For stairs, the design capacity considers the effective width of a tread, which accounts for railings or other obstructions, the friction or counter-flow between upward and downward pedestrians (up to 10 percent capacity reduction is applied to account for counter-flow friction), surging of entering and exiting pedestrians (up to 25 percent capacity reduction is applied to account for surged flows off of platforms and onto platforms), and the average area required for circulation. For passageways, similar considerations are made. For escalators and turnstiles, capacities are measured by the number and width of an element and the NYCT optimum capacity per element, also account for the potential for surging of entering and exiting pedestrians. In the analysis for each of these elements, volumes and capacities are presented for 15-minute intervals. The estimated v/c ratio is compared with NYCT criteria to determine a LOS for the operation of an element, as summarized in **Table 14-10**.

| Table 14-10 Level of Service Criteria for Subway Station Elements | |
|---|--------------|
| LOS | V/C Ratio |
| A | 0.00 to 0.45 |
| B | 0.45 to 0.70 |
| C | 0.70 to 1.00 |
| D | 1.00 to 1.33 |
| E | 1.33 to 1.67 |
| F | Above 1.67 |
| Sources: New York City Mayor's Office of Environmental Coordination, CEQR Technical Manual | |

At LOS A ("free flow") and B ("fluid flow"), there is sufficient area to allow pedestrians to freely select their walking speed and bypass slower pedestrians. When cross and reverse flow movement exists, only minor conflicts may occur. At LOS C ("fluid, somewhat restricted"), movement is fluid although somewhat restricted. While there is sufficient room for standing without personal contact, circulation through queuing areas may require adjustments to walking speed. At LOS D ("crowded, walking speed restricted"), walking speed is restricted and reduced. Reverse and cross flow movement is severely restricted because of congestion and the difficult passage of slower moving pedestrians. At LOS E ("congested, some shuffling and queuing") and F ("severely congested, queued"), walking speed is restricted. There is also insufficient area to bypass others, and opposing movement is difficult. Often, forward progress is achievable only through shuffling, with queues forming.

Significant Impact Criteria

The determination of significant impacts for station elements varies based on their type and use. For stairs and passageways, significant impacts are defined in term of width increment threshold (WIT) based on the minimum amount of additional capacity that would be required either to mitigate the LOS under the No Action levels, or to bring it to a v/c ratio of 1.00 (LOS C/D), whichever is greater. Significant impacts are typically considered to occur once the WITs in **Table 14-11** are reached or exceeded.

Table 14-11
Significant Impact Guidance for Stairs and Passageways

| With Action V/C Ratio | WIT for Significant Impact (inches) | |
|--|-------------------------------------|------------|
| | Stairway | Passageway |
| 1.00 to 1.09 | 8.0 | 13.0 |
| 1.10 to 1.19 | 7.0 | 11.5 |
| 1.20 to 1.29 | 6.0 | 10.0 |
| 1.30 to 1.39 | 5.0 | 8.5 |
| 1.40 to 1.49 | 4.0 | 6.0 |
| 1.50 to 1.59 | 3.0 | 4.5 |
| 1.60 and up | 2.0 | 3.0 |
| Note: WIT = Width Increment Threshold | | |
| Sources: New York City Mayor's Office of Environmental Coordination, <i>CEQR Technical Manual</i> | | |

For escalators and control area elements, impacts are significant if the proposed project causes a v/c ratio to increase from below 1.00 to 1.00 or greater. Where a facility is already at or above its capacity (a v/c of 1.00 or greater) in the No Action condition, a 0.01 increase in v/c ratio is also significant.

SUBWAY LINE-HAUL CAPACITIES

As per the *CEQR Technical Manual*, line-haul capacities are evaluated when a proposed project is anticipated to generate a perceptible number of passengers on particular subway and bus routes. For subways, if a subway line is expected to incur 200 or more passengers in one direction of travel during the commuter peak hours, a detailed review of ridership level at its maximum load point and/or other project-specific load points would be required to determine if the route's guideline (or practical) capacity would be exceeded. NYCT operates six different types of subway cars with different seating and guideline capacities. The peak period guideline capacity of a subway car, which ranges from 110 to 175 passengers, is compared with ridership levels to determine the acceptability of conditions.

Significant Impact Criteria

For subways, projected increases from the No Action condition within guideline capacity to a With Action condition that exceeds guideline capacity may be considered a significant adverse impact, if a subway car for a particular route is expected to incur five or more riders from a proposed project. Since there are constraints on what service improvements are available to NYCT, significant line-haul capacity impacts on subway routes are generally disclosed but would usually remain unmitigated.

PEDESTRIAN OPERATIONS

The adequacy of the study area's sidewalk, crosswalk, and corner reservoir capacities in relation to the demand imposed on them is evaluated based on the methodologies presented in the 2010 *HCM*, pursuant to procedures detailed in the *CEQR Technical Manual*.

The primary performance measure for sidewalks and walkways is pedestrian space, expressed as square feet per pedestrian (SFP), which is an indicator of the quality of pedestrian movement and comfort. The calculation of the sidewalk SFP is based on the pedestrian volumes by direction, the effective sidewalk or walkway width, and average walking speed. The SFP forms the basis for a sidewalk LOS analysis. The determination of sidewalk LOS is also dependent on whether the pedestrian flow being analyzed is best described as "non-platoon" or "platoon." Non-platoon flow occurs when pedestrian volume within the peak 15-minute period is relatively uniform, whereas, platoon flow occurs when pedestrian volumes vary significantly with the peak 15-minute period. Such variation typically occurs near bus stops, subway stations, and/or where adjacent crosswalks account for much of the walkway's pedestrian volume.

Street corners and crosswalks are not easily measured in terms of free pedestrian flow, as they are influenced by the effects of traffic signals. Street corners must be able to provide sufficient space for a mix of standing pedestrians (queued to cross a street) and circulating pedestrians (crossing the street or moving around the corner). The HCM methodologies apply a measure of time and space availability based on the area of the corner, the timing of the intersection signal, and the estimated space used by circulating pedestrians.

The total "time-space" available for these activities, expressed in square feet-second, is calculated by multiplying the net area of the corner (in square feet) by the signal's cycle length. The analysis then determines the total circulation time for all pedestrian movements at the corner per signal cycle (expressed as pedestrians per second). The ratio of net time-space divided by the total pedestrian circulation volume per signal cycle provides the LOS measurement of available SFP.

Crosswalk LOS is also a function of time and space. Similar to the street corner analysis, crosswalk conditions are first expressed as a measurement of the available area (the crosswalk width multiplied by the width of the street) and the permitted crossing time. This measure is expressed in square feet-second. The average time required for a pedestrian to cross the street is calculated based on the width of the street and an assumed walking speed. The ratio of time-space available in the crosswalk to the total crosswalk pedestrian occupancy time is the LOS measurement of available square feet per pedestrian. The LOS analysis also accounts for vehicular turning movements that traverse the crosswalk.

The LOS standards for sidewalks, corner reservoirs, and crosswalks are summarized in **Table 14-12**. The *CEQR Technical Manual* specifies acceptable LOS C or better (minimum of 31.5 SFP platoon flows for sidewalks; minimum of 19.5 SFP for corners and crosswalks) in Central Business District (CBD) settings, which include the project study area.

SIGNIFICANT IMPACT CRITERIA

The determination of significant pedestrian impacts considers the level of predicted decrease in pedestrian space between the No Action and With Action conditions. For different pedestrian elements, flow conditions, and area types, the CEQR procedure for impact determination corresponds with various sliding-scale formulas, as further detailed below.

Table 14-12

Level of Service Criteria for Pedestrian Elements

| LOS | Sidewalks | | Corner Reservoirs and Crosswalks |
|-----|-------------------|--------------------|----------------------------------|
| | Non-Platoon Flow | Platoon Flow | |
| A | > 60 SFP | > 530 SFP | > 60 SFP |
| B | > 40 and ≤ 60 SFP | > 90 and ≤ 530 SFP | > 40 and ≤ 60 SFP |
| C | > 24 and ≤ 40 SFP | > 40 and ≤ 90 SFP | > 24 and ≤ 40 SFP |
| D | > 15 and ≤ 24 SFP | > 23 and ≤ 40 SFP | > 15 and ≤ 24 SFP |
| E | > 8 and ≤ 15 SFP | > 11 and ≤ 23 SFP | > 8 and ≤ 15 SFP |
| F | ≤ 8 SFP | ≤ 11 SFP | ≤ 8 SFP |

Note: SFP = square feet per pedestrian
Sources: New York City Mayor's Office of Environmental Coordination, *CEQR Technical Manual*

Sidewalks

There are two sliding-scale formulas for determining significant sidewalk impacts. For non-platoon flow, the determination of significant sidewalk impacts is based on the sliding scale using the following formula: $Y \geq X/9.0 - 0.31$, where Y is the decrease in pedestrian space in SFP and X is the No Action pedestrian space in SFP. For platoon flow, the sliding-scale formula is $Y \geq X/(9.5 - 0.321)$. Since a decrease in pedestrian space within acceptable levels would not constitute a significant impact, these formulas would apply only if the With Action pedestrian space falls short of LOS C in non-CBD areas or mid-LOS D in CBD areas. **Table 14-13** summarizes the sliding scale guidance provided by the *CEQR Technical Manual* for determining potential significant sidewalk impacts.

Table 14-13
Significant Impact Guidance for Sidewalks

| Non-Platoon Flow | | | | Platoon Flow | | | |
|--|--|-------------------------------------|--|---|--|-------------------------------------|--|
| Sliding Scale Formula: $Y \geq X/9.0 - 0.31$ | | | | Sliding Scale Formula: $Y \geq X/(9.5 - 0.321)$ | | | |
| Non-CBD Areas | | CBD Areas | | Non-CBD Areas | | CBD Areas | |
| No Action Ped. Space (X, SFP) | With Action Ped. Space Reduc. (Y, SFP) | No Action Ped. Space (X, SFP) | With Action Ped. Space Reduc. (Y, SFP) | No Action Ped. Space (X, SFP) | With Action Ped. Space Reduc. (Y, SFP) | No Action Ped. Space (X, SFP) | With Action Ped. Space Reduc. (Y, SFP) |
| — | — | — | — | 43.5 to 44.3 | ≥ 4.3 | — | — |
| — | — | — | — | 42.5 to 43.4 | ≥ 4.2 | — | — |
| — | — | — | — | 41.6 to 42.4 | ≥ 4.1 | — | — |
| — | — | — | — | 40.6 to 41.5 | ≥ 4.0 | — | — |
| — | — | — | — | 39.7 to 40.5 | ≥ 3.9 | — | — |
| — | — | — | — | 38.7 to 39.6 | ≥ 3.8 | 38.7 to 39.2 | ≥ 3.8 |
| — | — | — | — | 37.8 to 38.6 | ≥ 3.7 | 37.8 to 38.6 | ≥ 3.7 |
| — | — | — | — | 36.8 to 37.7 | ≥ 3.6 | 36.8 to 37.7 | ≥ 3.6 |
| — | — | — | — | 35.9 to 36.7 | ≥ 3.5 | 35.9 to 36.7 | ≥ 3.5 |
| — | — | — | — | 34.9 to 35.8 | ≥ 3.4 | 34.9 to 35.8 | ≥ 3.4 |
| — | — | — | — | 34.0 to 34.8 | ≥ 3.3 | 34.0 to 34.8 | ≥ 3.3 |
| — | — | — | — | 33.0 to 33.9 | ≥ 3.2 | 33.0 to 33.9 | ≥ 3.2 |
| — | — | — | — | 32.1 to 32.9 | ≥ 3.1 | 32.1 to 32.9 | ≥ 3.1 |
| — | — | — | — | 31.1 to 32.0 | ≥ 3.0 | 31.1 to 32.0 | ≥ 3.0 |
| — | — | — | — | 30.2 to 31.0 | ≥ 2.9 | 30.2 to 31.0 | ≥ 2.9 |
| — | — | — | — | 29.2 to 30.1 | ≥ 2.8 | 29.2 to 30.1 | ≥ 2.8 |
| 25.8 to 26.6 | ≥ 2.6 | — | — | 28.3 to 29.1 | ≥ 2.7 | 28.3 to 29.1 | ≥ 2.7 |
| 24.9 to 25.7 | ≥ 2.5 | — | — | 27.3 to 28.2 | ≥ 2.6 | 27.3 to 28.2 | ≥ 2.6 |
| 24.0 to 24.8 | ≥ 2.4 | — | — | 26.4 to 27.2 | ≥ 2.5 | 26.4 to 27.2 | ≥ 2.5 |
| 23.1 to 23.9 | ≥ 2.3 | — | — | 25.4 to 26.3 | ≥ 2.4 | 25.4 to 26.3 | ≥ 2.4 |
| 22.2 to 23.0 | ≥ 2.2 | — | — | 24.5 to 25.3 | ≥ 2.3 | 24.5 to 25.3 | ≥ 2.3 |
| 21.3 to 22.1 | ≥ 2.1 | 21.3 to 21.5 | ≥ 2.1 | 23.5 to 24.4 | ≥ 2.2 | 23.5 to 24.4 | ≥ 2.2 |
| 20.4 to 21.2 | ≥ 2.0 | 20.4 to 21.2 | ≥ 2.0 | 22.6 to 23.4 | ≥ 2.1 | 22.6 to 23.4 | ≥ 2.1 |
| 19.5 to 20.3 | ≥ 1.9 | 19.5 to 20.3 | ≥ 1.9 | 21.6 to 22.5 | ≥ 2.0 | 21.6 to 22.5 | ≥ 2.0 |
| 18.6 to 19.4 | ≥ 1.8 | 18.6 to 19.4 | ≥ 1.8 | 20.7 to 21.5 | ≥ 1.9 | 20.7 to 21.5 | ≥ 1.9 |
| 17.7 to 18.5 | ≥ 1.7 | 17.7 to 18.5 | ≥ 1.7 | 19.7 to 20.6 | ≥ 1.8 | 19.7 to 20.6 | ≥ 1.8 |
| 16.8 to 17.6 | ≥ 1.6 | 16.8 to 17.6 | ≥ 1.6 | 18.8 to 19.6 | ≥ 1.7 | 18.8 to 19.6 | ≥ 1.7 |
| 15.9 to 16.7 | ≥ 1.5 | 15.9 to 16.7 | ≥ 1.5 | 17.8 to 18.7 | ≥ 1.6 | 17.8 to 18.7 | ≥ 1.6 |
| 15.0 to 15.8 | ≥ 1.4 | 15.0 to 15.8 | ≥ 1.4 | 16.9 to 17.7 | ≥ 1.5 | 16.9 to 17.7 | ≥ 1.5 |
| 14.1 to 14.9 | ≥ 1.3 | 14.1 to 14.9 | ≥ 1.3 | 15.9 to 16.8 | ≥ 1.4 | 15.9 to 16.8 | ≥ 1.4 |
| 13.2 to 14.0 | ≥ 1.2 | 13.2 to 14.0 | ≥ 1.2 | 15.0 to 15.8 | ≥ 1.3 | 15.0 to 15.8 | ≥ 1.3 |
| 12.3 to 13.1 | ≥ 1.1 | 12.3 to 13.1 | ≥ 1.1 | 14.0 to 14.9 | ≥ 1.2 | 14.0 to 14.9 | ≥ 1.2 |
| 11.4 to 12.2 | ≥ 1.0 | 11.4 to 12.2 | ≥ 1.0 | 13.1 to 13.9 | ≥ 1.1 | 13.1 to 13.9 | ≥ 1.1 |
| 10.5 to 11.3 | ≥ 0.9 | 10.5 to 11.3 | ≥ 0.9 | 12.1 to 13.0 | ≥ 1.0 | 12.1 to 13.0 | ≥ 1.0 |
| 9.6 to 10.4 | ≥ 0.8 | 9.6 to 10.4 | ≥ 0.8 | 11.2 to 12.0 | ≥ 0.9 | 11.2 to 12.0 | ≥ 0.9 |
| 8.7 to 9.5 | ≥ 0.7 | 8.7 to 9.5 | ≥ 0.7 | 10.2 to 11.1 | ≥ 0.8 | 10.2 to 11.1 | ≥ 0.8 |
| 7.8 to 8.6 | ≥ 0.6 | 7.8 to 8.6 | ≥ 0.6 | 9.3 to 10.1 | ≥ 0.7 | 9.3 to 10.1 | ≥ 0.7 |
| 6.9 to 7.7 | ≥ 0.5 | 6.9 to 7.7 | ≥ 0.5 | 8.3 to 9.2 | ≥ 0.6 | 8.3 to 9.2 | ≥ 0.6 |
| 6.0 to 6.8 | ≥ 0.4 | 6.0 to 6.8 | ≥ 0.4 | 7.4 to 8.2 | ≥ 0.5 | 7.4 to 8.2 | ≥ 0.5 |
| 5.1 to 5.9 | ≥ 0.3 | 5.1 to 5.9 | ≥ 0.3 | 6.4 to 7.3 | ≥ 0.4 | 6.4 to 7.3 | ≥ 0.4 |
| < 5.1 | ≥ 0.2 | < 5.1 | ≥ 0.2 | < 6.4 | ≥ 0.3 | < 6.4 | ≥ 0.3 |

Notes: SFP = square feet per pedestrian; Y = decrease in pedestrian space in SFP; X = No Action pedestrian space in SFP
Sources: New York City Mayor's Office of Environmental Coordination, *CEQR Technical Manual*

Corner Reservoirs and Crosswalks

The determination of significant corner and crosswalk impacts is also based on a sliding scale using the following formula: $Y \geq X/9.0 - 0.31$, where Y is the decrease in pedestrian space in SFP and X is the No Action pedestrian space in SFP. Since a decrease in pedestrian space within acceptable levels would not constitute a significant impact, this formula would apply only if the With Action pedestrian space falls short of LOS C in non-CBD areas or mid-LOS D in CBD areas. **Table 14-14** summarizes the sliding scale guidance provided by the *CEQR Technical Manual* for determining potential significant corner reservoir impacts.

Table 14-14
Significant Impact Guidance for Corners and Crosswalks

| Sliding Scale Formula: $Y \geq X/9.0 - 0.31$ | | | |
|--|---|-------------------------------------|---|
| Non-CBD Areas | | CBD Areas | |
| No Action Pedestrian Space (X, SFP) | With Action Pedestrian Space Reduction (Y, SFP) | No Action Pedestrian Space (X, SFP) | With Action Pedestrian Space Reduction (Y, SFP) |
| 25.8 to 26.6 | ≥ 2.6 | — | — |
| 24.9 to 25.7 | ≥ 2.5 | — | — |
| 24.0 to 24.8 | ≥ 2.4 | — | — |
| 23.1 to 23.9 | ≥ 2.3 | — | — |
| 22.2 to 23.0 | ≥ 2.2 | — | — |
| 21.3 to 22.1 | ≥ 2.1 | 21.3 to 21.5 | ≥ 2.1 |
| 20.4 to 21.2 | ≥ 2.0 | 20.4 to 21.2 | ≥ 2.0 |
| 19.5 to 20.3 | ≥ 1.9 | 19.5 to 20.3 | ≥ 1.9 |
| 18.6 to 19.4 | ≥ 1.8 | 18.6 to 19.4 | ≥ 1.8 |
| 17.7 to 18.5 | ≥ 1.7 | 17.7 to 18.5 | ≥ 1.7 |
| 16.8 to 17.6 | ≥ 1.6 | 16.8 to 17.6 | ≥ 1.6 |
| 15.9 to 16.7 | ≥ 1.5 | 15.9 to 16.7 | ≥ 1.5 |
| 15.0 to 15.8 | ≥ 1.4 | 15.0 to 15.8 | ≥ 1.4 |
| 14.1 to 14.9 | ≥ 1.3 | 14.1 to 14.9 | ≥ 1.3 |
| 13.2 to 14.0 | ≥ 1.2 | 13.2 to 14.0 | ≥ 1.2 |
| 12.3 to 13.1 | ≥ 1.1 | 12.3 to 13.1 | ≥ 1.1 |
| 11.4 to 12.2 | ≥ 1.0 | 11.4 to 12.2 | ≥ 1.0 |
| 10.5 to 11.3 | ≥ 0.9 | 10.5 to 11.3 | ≥ 0.9 |
| 9.6 to 10.4 | ≥ 0.8 | 9.6 to 10.4 | ≥ 0.8 |
| 8.7 to 9.5 | ≥ 0.7 | 8.7 to 9.5 | ≥ 0.7 |
| 7.8 to 8.6 | ≥ 0.6 | 7.8 to 8.6 | ≥ 0.6 |
| 6.9 to 7.7 | ≥ 0.5 | 6.9 to 7.7 | ≥ 0.5 |
| 6.0 to 6.8 | ≥ 0.4 | 6.0 to 6.8 | ≥ 0.4 |
| 5.1 to 5.9 | ≥ 0.3 | 5.1 to 5.9 | ≥ 0.3 |
| < 5.1 | ≥ 0.2 | < 5.1 | ≥ 0.2 |

Notes: SFP = square feet per pedestrian; Y = decrease in pedestrian space in SFP; X = No Action pedestrian space in SFP
Sources: New York City Mayor's Office of Environmental Coordination, *CEQR Technical Manual*

VEHICULAR AND PEDESTRIAN SAFETY EVALUATION

An evaluation of vehicular and pedestrian safety is necessary for locations within the traffic and pedestrian study areas that have been identified as high accident locations, where 48 or more total reportable and non-reportable crashes or five or more pedestrian/bicyclist injury crashes occurred in any consecutive 12 months of the most recent 3-year period for which data are available. For these locations, accident trends are identified to determine whether projected vehicular and pedestrian traffic would further impact safety at these locations. The determination of potential significant safety impacts depends on the type of area where the project site is located, traffic volumes, accident types and severity, and other contributing factors. Where appropriate, measures to improve traffic and pedestrian safety are identified and coordinated with DOT for their approval.

PARKING CONDITIONS ASSESSMENT

The parking analysis identifies the extent to which off-street parking is available and utilized under existing and future conditions. It takes into consideration anticipated changes in area parking supply and provides a comparison of parking needs versus availability to determine if a parking shortfall is likely to result from parking displacement attributable to or additional demand generated by a proposed project. Typically, this analysis encompasses a study area within a ¼-mile of the project site. If the analysis concludes a shortfall in parking within the ¼-mile study area, the study area could sometimes be extended to a ½-mile to identify additional parking supply.

Under the *CEQR Technical Manual's* guidance, for proposed projects located in Manhattan or other CBD areas, the inability of the proposed project or the surrounding area to accommodate the projects' future parking demand is considered a parking shortfall, but is generally not considered significant due to the magnitude of available alternative modes of transportation. For other areas in New York City, a parking shortfall that exceeds more than half the available on-street and off-street parking spaces within a ¼-mile of the project site may be considered significant. Additional factors, such as the availability and extent of transit in the area, proximity of the project to such transit, and patterns of automobile usage by area residents, could be considered to determine the significance of the identified parking shortfall. In some cases, if there is adequate parking supply within ½-mile of the project site, the projected parking shortfall may also not necessarily be considered significant.

D. DETAILED TRAFFIC ANALYSIS

As described above in Section B, "Preliminary Analysis Methodology and Screening Assessment," 29 signalized intersections and two unsignalized intersections have been selected for analysis in the weekday AM, midday, and PM peak hours.

EXISTING CONDITIONS

ROADWAY NETWORK AND TRAFFIC STUDY AREA

The key roadways in the study area include South Street, Cherry Street, Madison Street, Henry Street, East Broadway, Division Street, Allen/Pike Street, Rutgers Street, Clinton Street, Montgomery Street, the Bowery, and Worth Street. The physical and operational characteristics of the study area roadways are described below.

- South Street is a local two-way northbound-southbound roadway located immediately adjacent to the East River and operates from Whitehall Street to Jackson Street near Corlears Hook Park. South Street is approximately 34 feet wide curb-to-curb and is a DOT-designated truck route south of Pike Street. South Street provides vehicular, pedestrian, and bicycle access/egress to the East River Park at Montgomery Street.
- Cherry Street is a local one-way westbound roadway located immediately adjacent to the project sites and operates with one moving lane from Montgomery Street to Catherine Street. Cherry Street is approximately 50 feet wide curb-to-curb with on-street parking available on both sides of the street.
- Madison Street is a local two-way eastbound-westbound roadway that operates with one moving lane and bike lane in each direction, and curb-to-curb width of approximately 50 feet. Curbside parking is available on both sides of the street.
- East Broadway is a local two-way eastbound-westbound roadway that operates with one moving lane and bike lane in each direction, and curb-to-curb width of approximately 50 feet. Curbside parking is available on both sides of the street.
- Division Street is a local one-way westbound roadway from Canal Street to The Bowery. It is approximately 25–35 feet wide curb-to-curb, and operates with one to two moving lanes with curbside parking available on both sides of the street. In addition, it is classified as a local truck route from Delancey Street to South Street, and a through truck route from West Houston Street to Delancey Street.

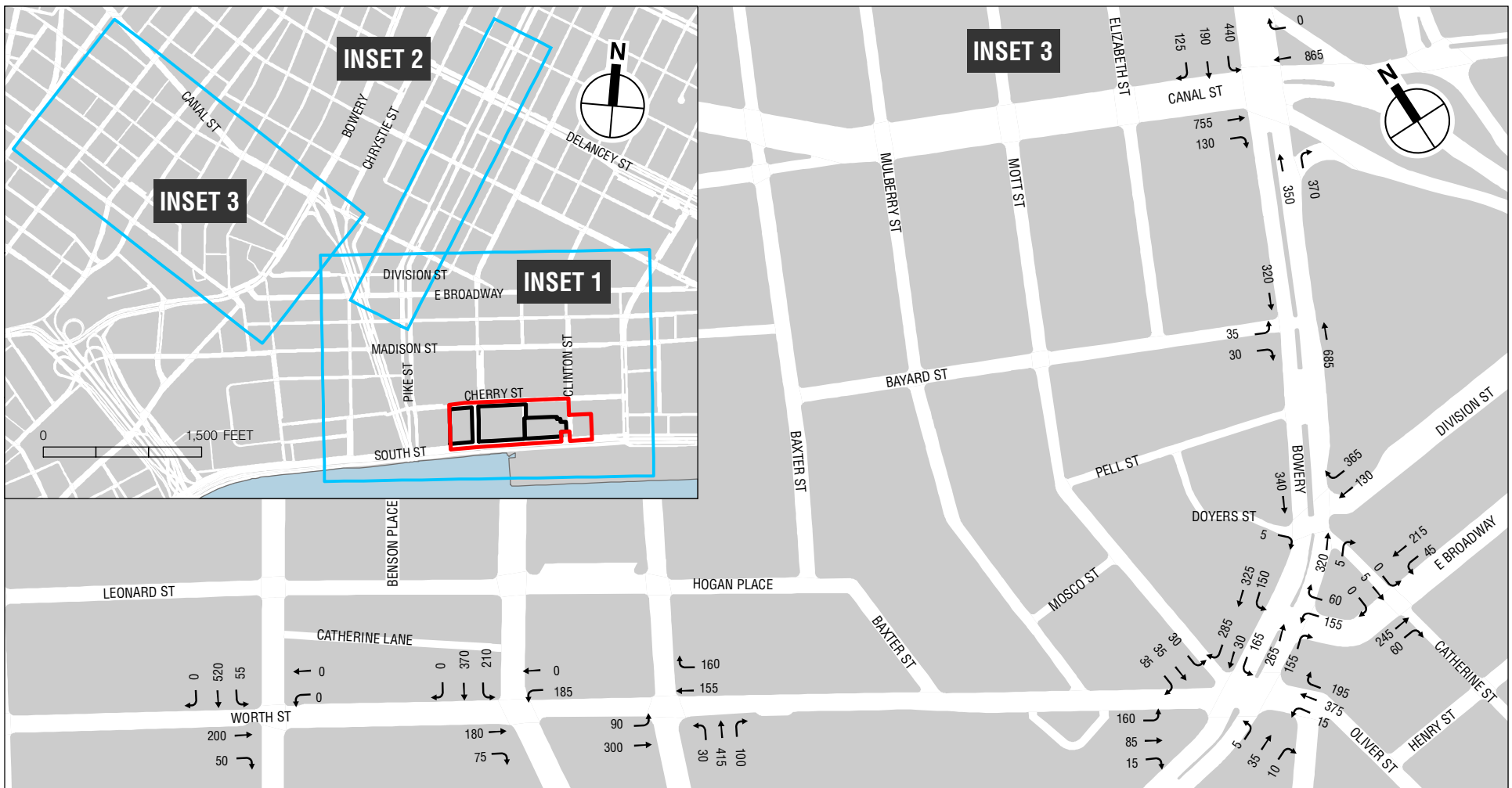
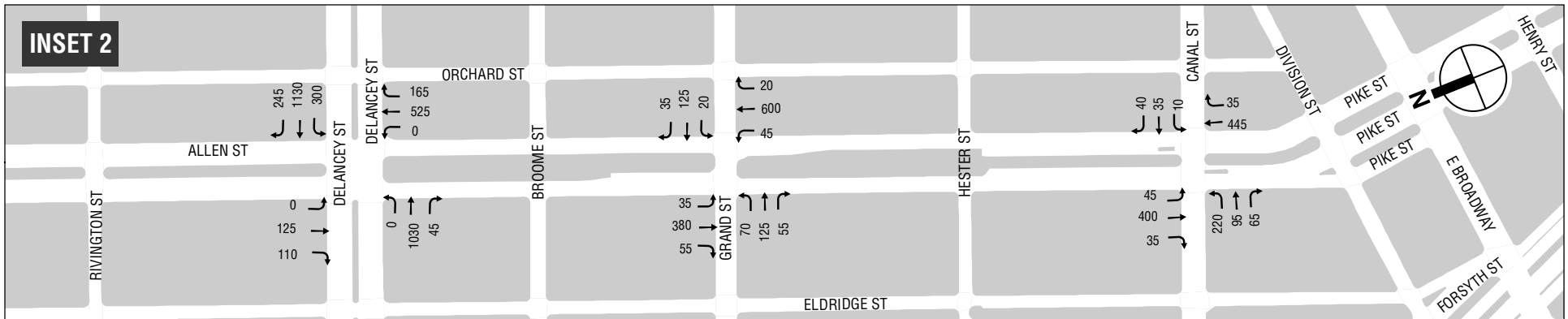
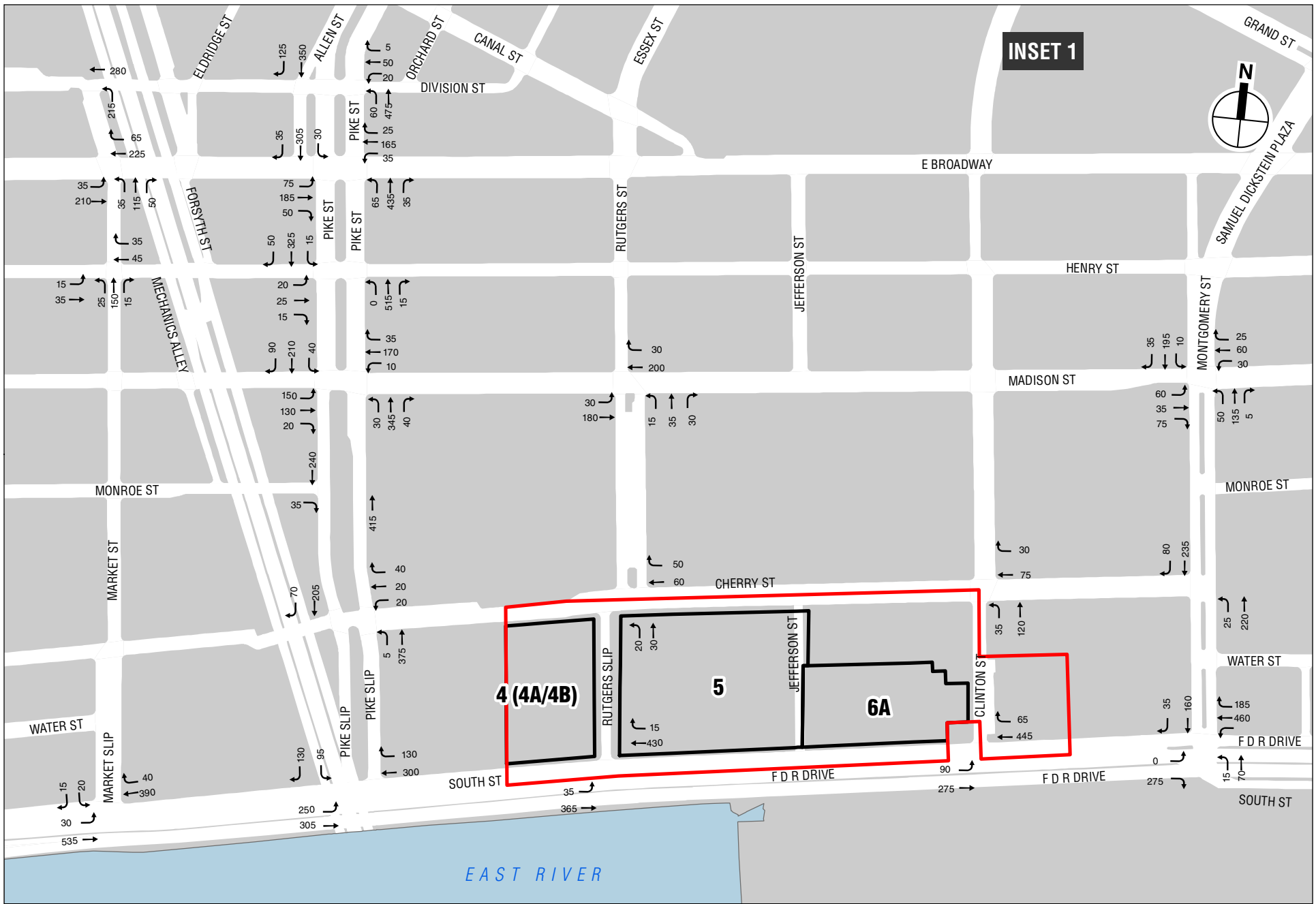
- Allen/Pike Street is major two-way northbound-southbound roadway with pedestrian refuge islands within the roadway's median to separate the two-directional traffic and provides storage for pedestrians. Allen/Pike Street generally consists of two moving lanes in each direction with curbside parking available on both sides of the street, and a curb-to-curb width of approximately 115 feet. In addition, it is classified as a local truck route from Delancey Street to South Street, and a through truck route from West Houston Street to Delancey Street.
- Rutgers Street is a local roadway which operates two-way northbound and southbound between Madison Street and Cherry Street, and one-way northbound on the remaining portions. It generally operates with one moving lane with curbside parking available on both sides of the street.
- Clinton Street is a local one-way northbound roadway. It operates with one moving lane and a curb-to-curb width of varying from approximately 30–50 feet. Curbside parking is available on both sides of the street.
- Montgomery Street is a local two-way northbound-southbound roadway with one moving lane and bike lane in each direction. It is approximately 60 feet wide curb-to-curb and provides curbside parking on both sides of the street.
- Worth Street is a local two-way eastbound-westbound roadway, which runs from Chatham Square to Hudson Street. It is approximately 45 feet wide curb-to-curb and operates with one to two moving lanes in each direction with limited curbside parking available.

TRAFFIC CONDITIONS

Traffic data were collected in May 2016 and March 2017 for the weekday AM, midday, and PM peak periods via a combination of intersection turning movement counts and 24-hour Automatic Traffic Recorder (ATR) counts. Existing peak period traffic volumes were developed based on these counts. The standard peak hours in Manhattan south of 110th Street generally occur from 8:00 AM to 9:00 AM, 12:00 PM to 1:00 PM, and 5:00 PM to 6:00 PM on weekdays. For analysis, the highest peak hour traffic volumes (from 9:00 AM to 10:00 AM, 12:45 PM to 1:45 PM, and 5:30 PM to 6:30 PM) during the respective peak periods based on the collected data were used.

Inventories of roadway geometry, traffic controls, bus stops, and parking regulations/activities were recorded to provide appropriate inputs for the operational analyses. Official signal timings were also obtained from DOT for use in the analysis of the study area signalized intersections. **Figures 14-10 through 14-12** show the existing traffic volumes for the weekday AM, midday, and PM peak hours, respectively. During the data collection, the traffic operations/roadway configuration at two intersections in the study area was modified due to an ongoing roadway reconstruction project that is expected to be completed by 2019. These intersections are Worth Street at Broadway and Worth Street at Lafayette Street. Worth Street operated with one lane eastbound only from West Broadway to Lafayette Street. Westbound vehicles travelling along Worth Street terminated with a left-turn onto Lafayette Street. The two-way operation of Worth Street was restored in the analysis of the No Action and With Action conditions.

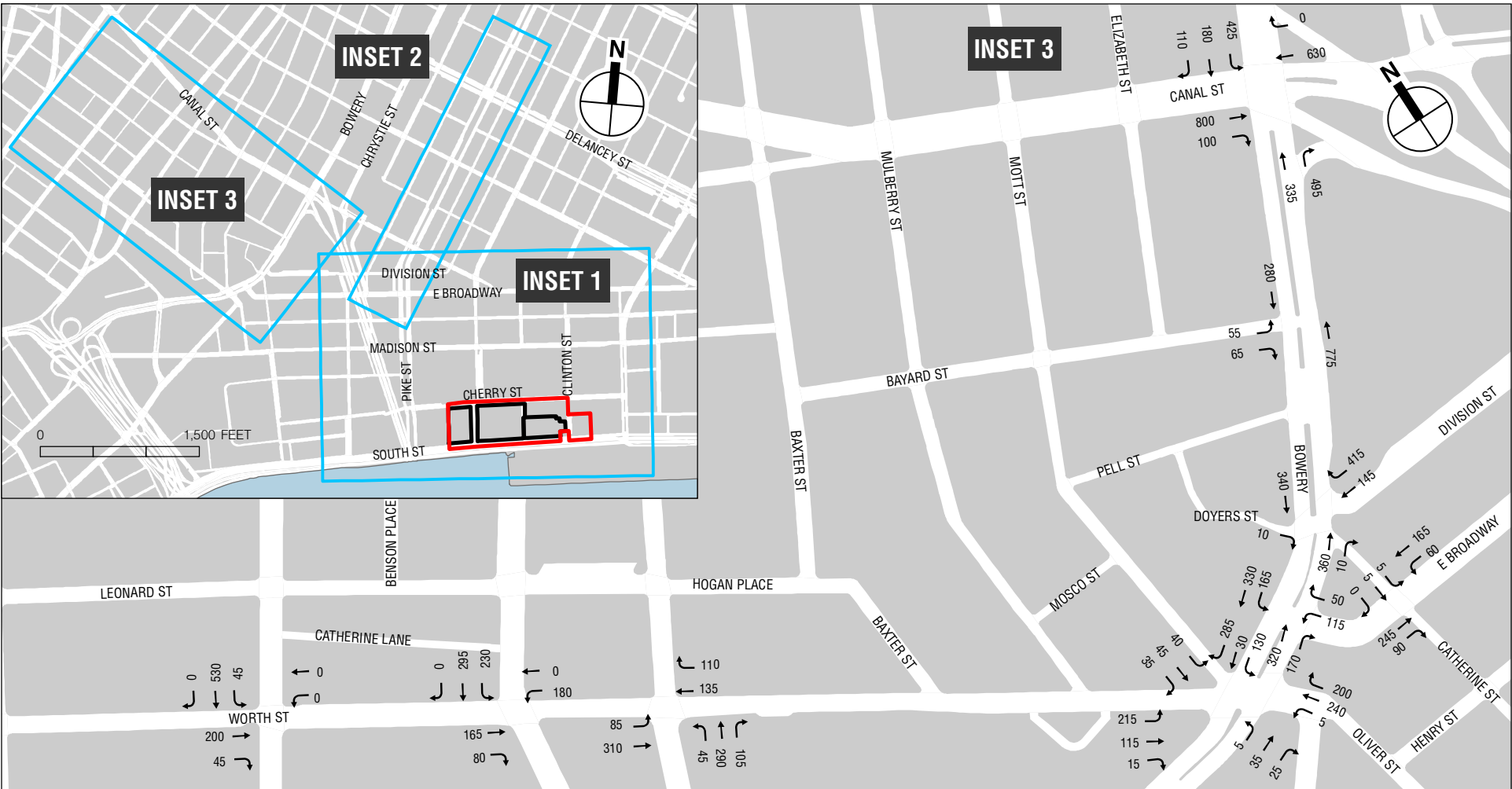
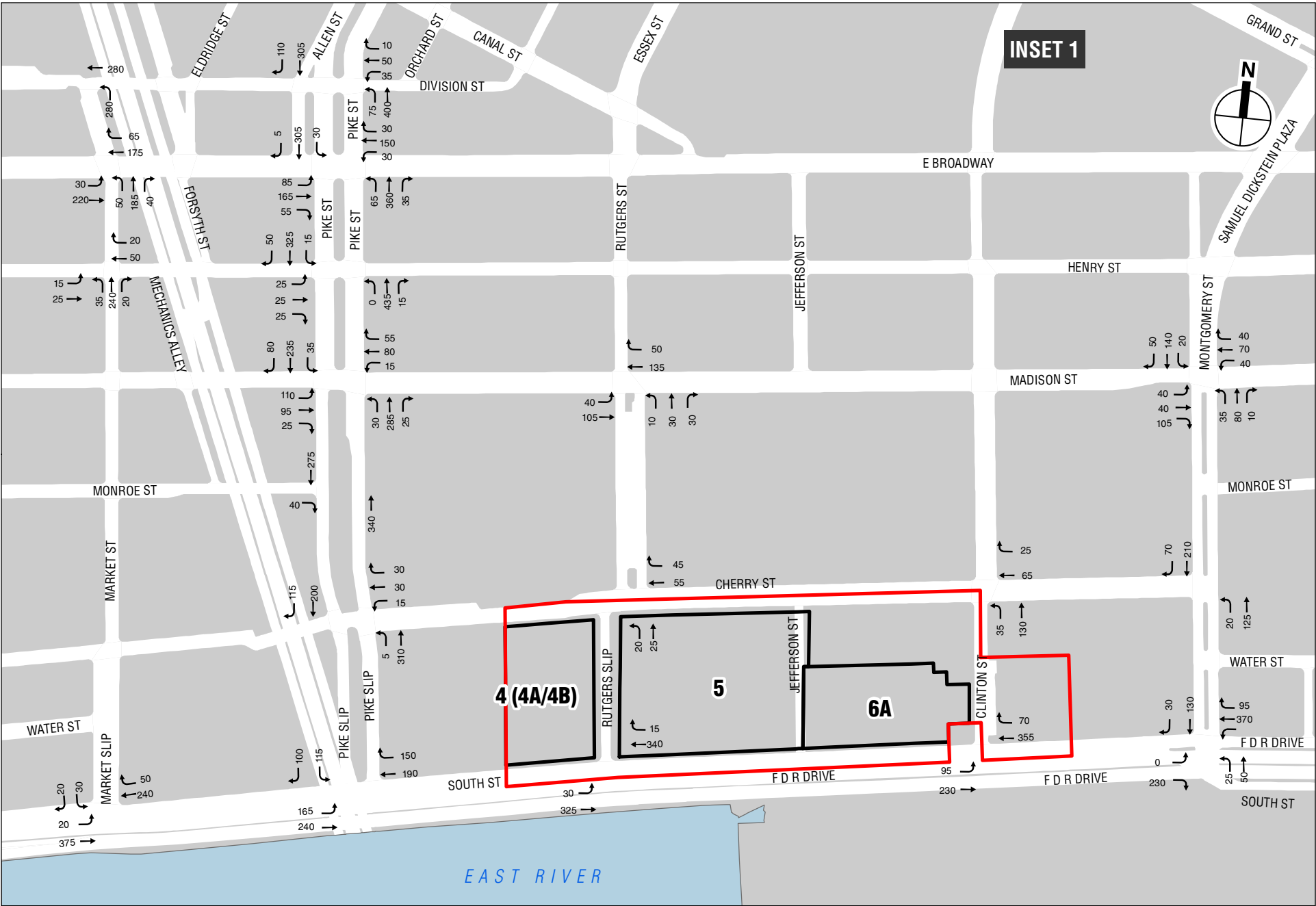
As described in Chapter 1, "Project Description," Site 4 (4A/4B) has three existing curb cuts, one each on Cherry Street, Rutgers Slip, and South Street. Site 5 has four existing curb cuts on Cherry Street and five existing curb cuts on South Street. Site 6A has two existing curb cuts on South Street.



 Project Sites

 Boundary of Two Bridges LSRD

Existing Traffic Volumes
Weekday AM Peak Hour
Figure 14-10

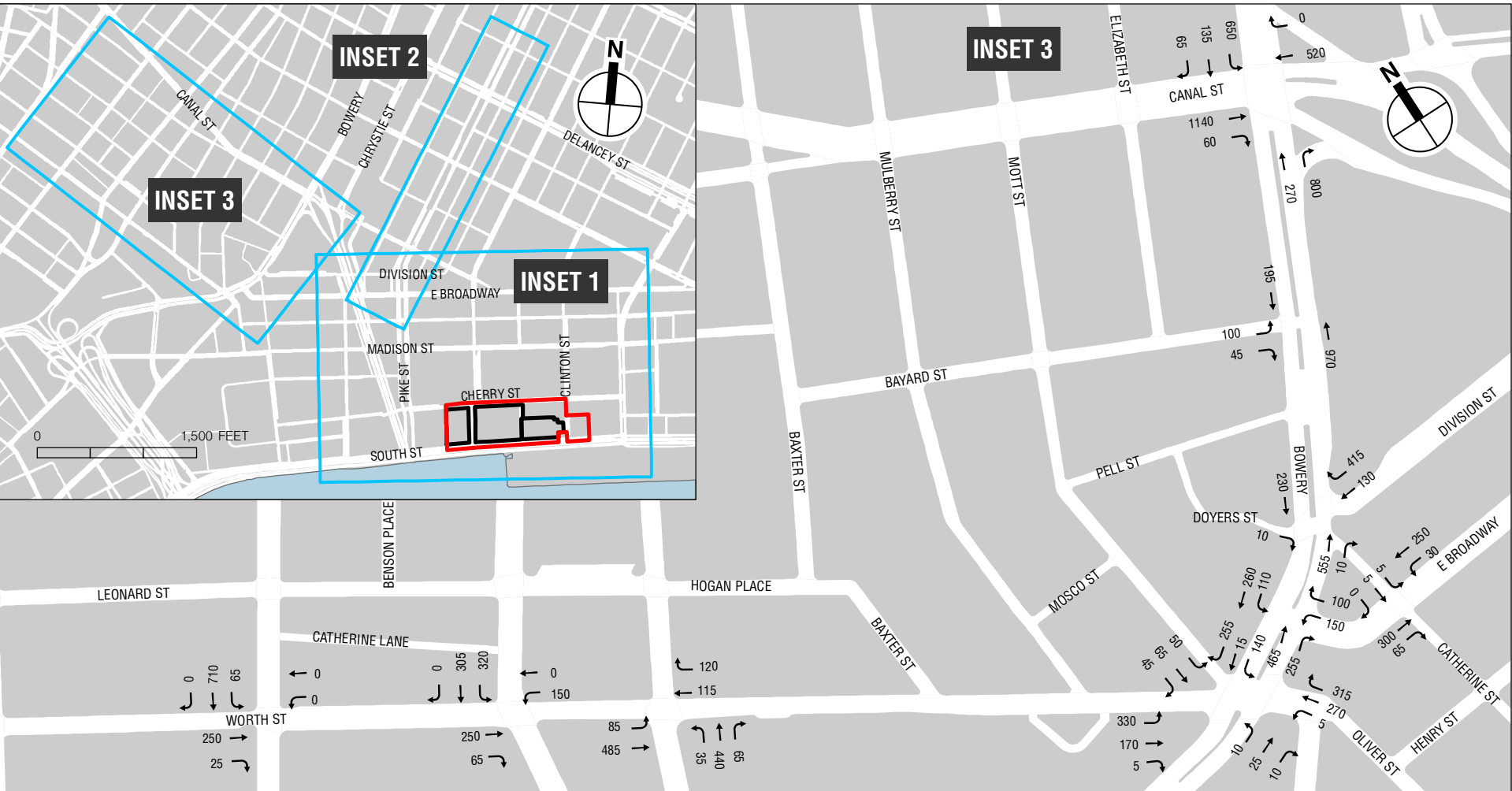
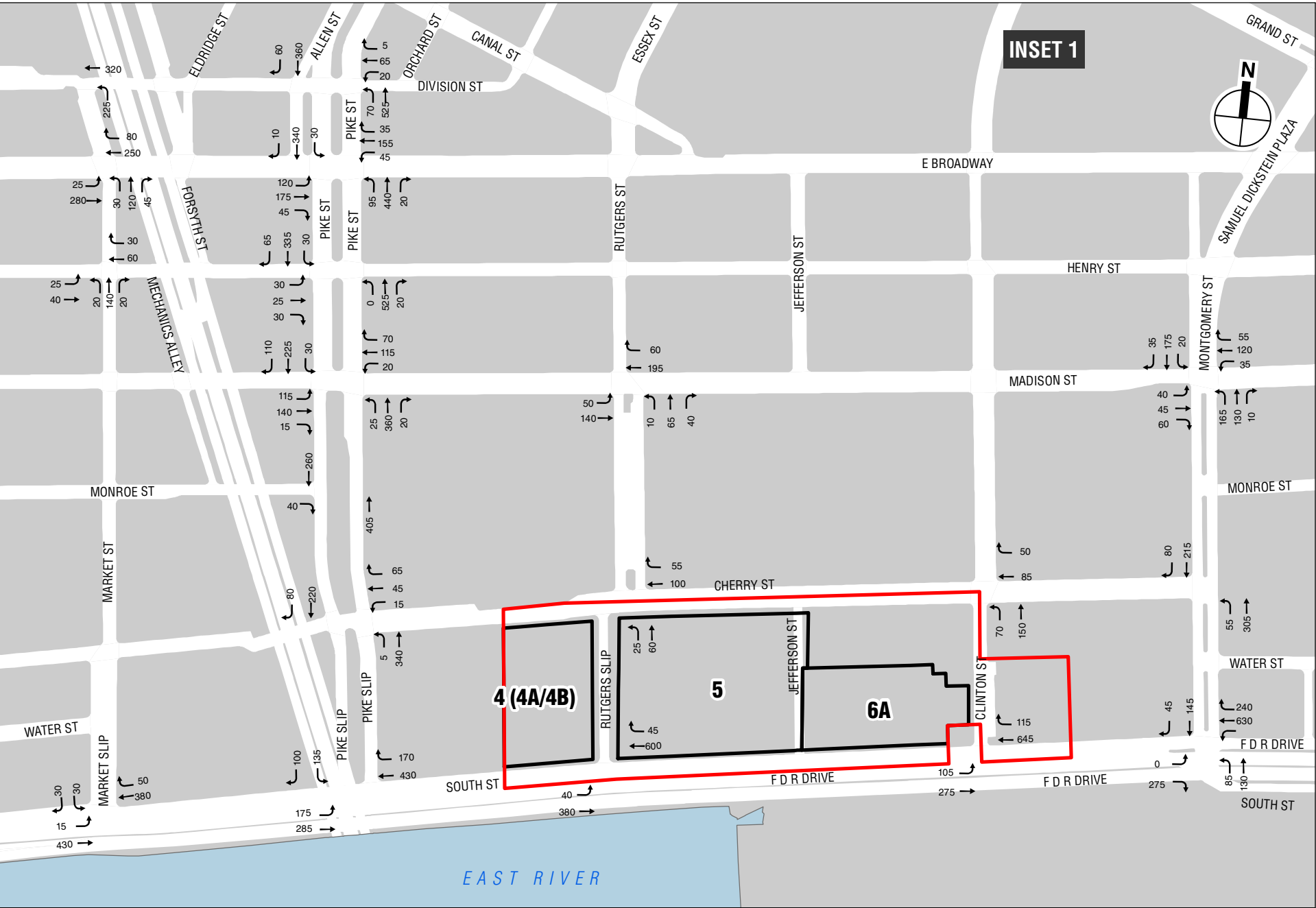


 Project Sites

 Boundary of Two Bridges LSRD

0 400 FEET

Existing Traffic Volumes
Weekday Midday Peak Hour
Figure 14-11



 Project Sites
 Boundary of Two Bridges LSRD

0 400 FEET

Existing Traffic Volumes
Weekday PM Peak Hour
Figure 14-12

Two Bridges LSRD

LEVELS OF SERVICE

A summary of the existing conditions traffic analysis results are presented in **Table 14-15**. Details on level-of-service, v/c ratios, and average delays are presented in **Tables 14-16 and 14-17**. The capacity analysis indicates that most of the study area's intersection approaches/lane groups operate acceptably—at mid-LOS D or better (delays of 45 seconds or less per vehicle for the study area's signalized intersections) during peak hours. Approaches/lane groups operating beyond mid-LOS D and those with v/c ratios of 0.90 or greater are listed below.

Table 14-15
Summary of Existing Traffic Analysis Results

| Level of Service | Analysis Peak Hours | | |
|-----------------------------------|---------------------|----------------|------------|
| | Weekday AM | Weekday Midday | Weekday PM |
| Signalized Intersections | | | |
| Lane Groups at LOS A/B/C | 106 | 107 | 102 |
| Lane Groups at LOS D | 23 | 22 | 19 |
| Lane Groups at LOS E | 3 | 4 | 10 |
| Lane Groups at LOS F | 4 | 3 | 5 |
| Total | 136 | 136 | 136 |
| Lane Groups with v/c ≥ 0.90 | 7 | 4 | 12 |
| Unsignalized Intersections | | | |
| Lane Groups at LOS A/B/C | 3 | 3 | 3 |
| Lane Groups at LOS D | 0 | 0 | 0 |
| Lane Groups at LOS E | 0 | 0 | 0 |
| Lane Groups at LOS F | 0 | 0 | 0 |
| Total | 3 | 3 | 3 |
| Lane Groups with v/c ≥ 0.90 | 0 | 0 | 0 |

Notes: LOS = Level-of-Service; v/c = volume-to-capacity ratio

Table 14-16
Existing Conditions Level of Service Analysis
Signalized Intersections

| Intersection | Weekday AM | | | | Weekday Midday | | | | Weekday PM | | | |
|---|------------|-----------|-------------|-----|----------------|-----------|-------------|-----|------------|-----------|-------------|-----|
| | Lane Group | v/c Ratio | Delay (sec) | LOS | Lane Group | v/c Ratio | Delay (sec) | LOS | Lane Group | v/c Ratio | Delay (sec) | LOS |
| South Street and Market Slip | | | | | | | | | | | | |
| Eastbound | LT | 0.75 | 21.9 | C | LT | 0.52 | 15.4 | B | LT | 0.56 | 16.2 | B |
| Westbound | TR | 0.59 | 16.5 | B | TR | 0.36 | 12.7 | B | TR | 0.51 | 15.0 | B |
| Southbound | LR | 0.09 | 20.3 | C | LR | 0.12 | 20.6 | C | LR | 0.14 | 20.9 | C |
| South Street and Pike Slip | | | | | | | | | | | | |
| Eastbound | L | 0.69 | 19.3 | B | L | 0.36 | 10.6 | B | L | 0.53 | 16.6 | B |
| | T | 0.59 | 25.7 | C | T | 0.44 | 22.6 | C | T | 0.48 | 23.2 | C |
| Westbound | T | 0.53 | 24.1 | C | T | 0.30 | 20.2 | C | T | 0.69 | 28.6 | C |
| | R | 0.35 | 21.5 | C | R | 0.40 | 22.4 | C | R | 0.40 | 22.4 | C |
| Southbound | L | 0.41 | 35.0 | D | L | 0.50 | 37.4 | D | L | 0.55 | 38.5 | D |
| | R | 0.52 | 38.5 | D | R | 0.47 | 36.8 | D | R | 0.43 | 35.6 | D |
| South Street and Rutgers Slip | | | | | | | | | | | | |
| Eastbound | LT | 0.54 | 15.7 | B | LT | 0.50 | 15.0 | B | LT | 0.63 | 17.9 | B |
| Westbound | TR | 0.55 | 15.5 | B | TR | 0.39 | 13.0 | B | TR | 0.67 | 18.3 | B |
| South Street and Clinton Street | | | | | | | | | | | | |
| Eastbound | LT | 0.63 | 19.1 | B | LT | 0.70 | 21.9 | C | LT | 0.96 | 52.7 | D |
| Westbound | T | 0.57 | 16.2 | B | T | 0.51 | 15.1 | B | T | 0.79 | 23.7 | C |
| | R | 0.12 | 10.4 | B | R | 0.12 | 10.4 | B | R | 0.20 | 11.2 | B |
| South Street (North) and Montgomery Street | | | | | | | | | | | | |
| Westbound | LTR | 0.85 | 26.6 | C | LTR | 0.53 | 15.2 | B | LTR | 1.05 | 63.9 | E |
| Northbound | LT | 0.19 | 21.4 | C | LT | 0.19 | 21.5 | C | LT | 0.67 | 33.5 | C |
| Southbound | TR | 0.53 | 28.1 | C | TR | 0.40 | 25.2 | C | TR | 0.50 | 27.4 | C |
| South Street (South) and Montgomery Street | | | | | | | | | | | | |
| Eastbound | LTR | 0.35 | 12.5 | B | LTR | 0.27 | 11.7 | B | LTR | 0.36 | 12.7 | B |
| Northbound | TR | 0.11 | 20.5 | C | TR | 0.15 | 21.1 | C | TR | 0.46 | 25.6 | C |
| Southbound | LT | 0.58 | 29.9 | C | LT | 0.47 | 27.3 | C | LT | 1.05 | 96.3 | F |

Table 14-16 (cont'd)
Existing Conditions Level of Service Analysis
Signalized Intersections

| Intersection | Weekday AM | | | | Weekday Midday | | | | Weekday PM | | | |
|--|------------|-----------|-------------|-----|----------------|-----------|-------------|-----|------------|-----------|-------------|-----|
| | Lane Group | v/c Ratio | Delay (sec) | LOS | Lane Group | v/c Ratio | Delay (sec) | LOS | Lane Group | v/c Ratio | Delay (sec) | LOS |
| Cherry Street and Pike Street | | | | | | | | | | | | |
| Westbound | LTR | 0.24 | 24.4 | C | LTR | 0.21 | 23.9 | C | LTR | 0.35 | 26.2 | C |
| Northbound | L | 0.04 | 36.2 | D | L | 0.04 | 36.2 | D | L | 0.04 | 36.1 | D |
| | T | 0.29 | 10.1 | B | T | 0.22 | 9.5 | A | T | 0.26 | 9.8 | A |
| Southbound | TR | 0.28 | 18.3 | B | TR | 0.31 | 18.6 | B | TR | 0.29 | 18.3 | B |
| Cherry Street and Rutgers Street | | | | | | | | | | | | |
| Westbound | TR | 0.21 | 16.1 | B | TR | 0.19 | 15.9 | B | TR | 0.29 | 17.1 | B |
| Northbound | LT | 0.09 | 17.1 | B | LT | 0.09 | 17.0 | B | LT | 0.19 | 18.3 | B |
| Cherry Street and Montgomery Street | | | | | | | | | | | | |
| Northbound | LT | 0.47 | 17.0 | B | LT | 0.28 | 14.2 | B | LT | 0.68 | 23.0 | C |
| Southbound | TR | 0.60 | 20.2 | C | TR | 0.49 | 17.5 | B | TR | 0.57 | 19.4 | B |
| Madison Street and Pike Street (East) | | | | | | | | | | | | |
| Eastbound | L | 1.05 | 110.1 | F | L | 0.72 | 49.6 | D | L | 0.86 | 73.4 | E |
| | T | 0.31 | 24.1 | C | T | 0.26 | 25.4 | C | T | 0.36 | 27.0 | C |
| Westbound | TR | 0.65 | 33.2 | C | TR | 0.54 | 32.3 | C | TR | 0.72 | 40.0 | D |
| Northbound | L | 0.24 | 40.1 | D | L | 0.24 | 40.2 | D | L | 0.19 | 39.0 | D |
| | TR | 0.46 | 22.0 | C | TR | 0.33 | 20.2 | C | TR | 0.41 | 21.2 | C |
| Madison Street and Pike Street (West) | | | | | | | | | | | | |
| Eastbound | TR | 0.83 | 45.5 | D | TR | 0.73 | 40.2 | D | TR | 0.80 | 45.2 | D |
| Westbound | L | 0.08 | 21.5 | C | L | 0.12 | 24.5 | C | L | 0.19 | 26.4 | C |
| | T | 0.42 | 25.7 | C | T | 0.22 | 24.8 | C | T | 0.30 | 25.9 | C |
| Southbound | L | 0.35 | 43.9 | D | L | 0.24 | 37.2 | D | L | 0.19 | 36.0 | D |
| | TR | 0.36 | 20.7 | C | TR | 0.37 | 18.8 | B | TR | 0.38 | 18.9 | B |
| Madison Street and Rutgers Street | | | | | | | | | | | | |
| Eastbound | LT | 0.37 | 12.8 | B | LT | 0.29 | 12.0 | B | LT | 0.40 | 13.5 | B |
| Westbound | TR | 0.43 | 13.6 | B | TR | 0.38 | 13.0 | B | TR | 0.49 | 14.8 | B |
| Northbound | LT | 0.14 | 21.7 | C | LT | 0.11 | 21.3 | C | LT | 0.19 | 22.2 | C |
| | R | 0.08 | 20.9 | C | R | 0.08 | 21.0 | C | R | 0.11 | 21.2 | C |
| Madison Street and Montgomery Street | | | | | | | | | | | | |
| Eastbound | LTR | 0.46 | 21.0 | C | LTR | 0.43 | 20.2 | C | LTR | 0.39 | 19.3 | B |
| Westbound | LTR | 0.29 | 17.4 | B | LTR | 0.36 | 18.7 | B | LTR | 0.50 | 21.2 | C |
| Northbound | LTR | 0.45 | 20.1 | C | LTR | 0.30 | 17.5 | B | LTR | 0.97 | 64.1 | E |
| Southbound | LTR | 0.48 | 20.4 | C | LTR | 0.45 | 20.0 | C | LTR | 0.47 | 20.5 | C |
| Henry Street and Market Street | | | | | | | | | | | | |
| Eastbound | LT | 0.14 | 15.4 | B | LT | 0.12 | 15.3 | B | LT | 0.19 | 16.1 | B |
| Westbound | TR | 0.24 | 17.0 | B | TR | 0.18 | 16.0 | B | TR | 0.22 | 16.5 | B |
| Northbound | LTR | 0.39 | 18.8 | B | LTR | 0.62 | 24.1 | C | LTR | 0.36 | 18.3 | B |
| Henry Street and Pike Street | | | | | | | | | | | | |
| Eastbound | LTR | 0.17 | 23.4 | C | LTR | 0.21 | 23.8 | C | LTR | 0.23 | 24.3 | C |
| Northbound | TR | 0.59 | 23.2 | C | TR | 0.52 | 21.8 | C | TR | 0.53 | 21.8 | C |
| Southbound | L | 0.14 | 38.1 | D | L | 0.14 | 38.1 | D | L | 0.20 | 39.4 | D |
| | TR | 0.30 | 10.3 | B | TR | 0.30 | 10.3 | B | TR | 0.32 | 10.5 | B |
| East Broadway and Catherine Street | | | | | | | | | | | | |
| Eastbound | TR | 0.49 | 12.0 | B | TR | 0.53 | 12.9 | B | TR | 0.50 | 11.9 | B |
| Westbound | LT | 0.49 | 12.5 | B | LT | 0.49 | 12.7 | B | LT | 0.44 | 11.3 | B |
| Southbound | LTR | 0.02 | 23.7 | C | LTR | 0.05 | 24.2 | C | LTR | 0.05 | 24.1 | C |
| East Broadway and Market Street | | | | | | | | | | | | |
| Eastbound | LT | 0.52 | 16.4 | B | LT | 0.46 | 14.9 | B | LT | 0.52 | 16.0 | B |
| Westbound | TR | 0.56 | 17.5 | B | TR | 0.49 | 15.9 | B | TR | 0.62 | 18.8 | B |
| Northbound | LTR | 0.68 | 35.1 | D | LTR | 0.80 | 42.0 | D | LTR | 0.58 | 30.2 | C |
| East Broadway and Pike Street (East) | | | | | | | | | | | | |
| Eastbound | L | 0.53 | 34.2 | C | L | 0.47 | 31.3 | C | L | 0.80 | 56.0 | E |
| | T | 0.43 | 25.3 | C | T | 0.39 | 24.6 | C | T | 0.40 | 24.7 | C |
| Westbound | TR | 0.63 | 31.9 | C | TR | 0.59 | 30.4 | C | TR | 0.61 | 30.7 | C |
| Northbound | L | 0.59 | 55.0 | E | L | 0.52 | 50.9 | D | L | 0.78 | 71.1 | E |
| | TR | 0.65 | 25.4 | C | TR | 0.51 | 22.5 | C | TR | 0.53 | 22.6 | C |

Table 14-16 (cont'd)
Existing Conditions Level of Service Analysis
Signalized Intersections

| Intersection | Weekday AM | | | | Weekday Midday | | | | Weekday PM | | | |
|---|------------|-----------|-------------|-----|----------------|-----------|-------------|-----|------------|-----------|-------------|-----|
| | Lane Group | v/c Ratio | Delay (sec) | LOS | Lane Group | v/c Ratio | Delay (sec) | LOS | Lane Group | v/c Ratio | Delay (sec) | LOS |
| East Broadway and Pike Street (West) | | | | | | | | | | | | |
| Eastbound | TR | 0.92 | 57.2 | E | TR | 0.95 | 63.1 | E | TR | 0.99 | 70.1 | E |
| Westbound | L | 0.32 | 27.7 | C | L | 0.27 | 26.3 | C | L | 0.42 | 32.3 | C |
| | T | 0.38 | 24.5 | C | T | 0.35 | 23.8 | C | T | 0.32 | 23.3 | C |
| Southbound | L | 0.33 | 46.4 | D | L | 0.33 | 46.0 | D | L | 0.31 | 45.1 | D |
| | T | 0.35 | 21.1 | C | T | 0.35 | 21.0 | C | T | 0.40 | 21.7 | C |
| Division Street and Market Street | | | | | | | | | | | | |
| Westbound | T | 0.26 | 18.0 | B | T | 0.26 | 18.0 | B | T | 0.26 | 18.0 | B |
| Northbound | L | 0.62 | 30.0 | C | L | 0.86 | 47.2 | D | L | 0.57 | 27.7 | C |
| Division Street and Allen Street/Pike Street | | | | | | | | | | | | |
| Westbound | LTR | 0.31 | 27.7 | C | LTR | 0.39 | 29.5 | C | LTR | 0.35 | 28.2 | C |
| Northbound | L | 0.46 | 47.4 | D | L | 0.64 | 58.1 | E | L | 0.51 | 49.2 | D |
| | T | 0.35 | 10.7 | B | T | 0.29 | 10.1 | B | T | 0.33 | 10.4 | B |
| Southbound | T | 0.31 | 18.5 | B | T | 0.28 | 18.2 | B | T | 0.30 | 18.4 | B |
| | R | 0.48 | 24.3 | C | R | 0.42 | 23.0 | C | R | 0.20 | 18.2 | B |
| Allen Street and Canal Street | | | | | | | | | | | | |
| Eastbound | LTR | 1.05 | 87.4 | F | LTR | 0.74 | 35.4 | D | LTR | 1.04 | 83.0 | F |
| Westbound | LTR | 0.27 | 21.1 | C | LTR | 0.32 | 22.2 | C | LTR | 0.30 | 21.5 | C |
| Northbound | TR | 0.61 | 27.7 | C | TR | 0.52 | 25.8 | C | TR | 0.64 | 28.3 | C |
| Southbound | LTR | 0.37 | 14.0 | B | LTR | 0.33 | 13.5 | B | LTR | 0.29 | 13.1 | B |
| Allen Street and Grand Street (East) | | | | | | | | | | | | |
| Eastbound | L | 0.47 | 31.6 | C | L | 0.30 | 28.3 | C | L | 0.36 | 28.6 | C |
| | T | 0.29 | 23.0 | C | T | 0.34 | 26.0 | C | T | 0.49 | 27.9 | C |
| Westbound | TR | 0.52 | 28.2 | C | TR | 0.56 | 32.0 | C | TR | 0.46 | 28.0 | C |
| Northbound | L | 0.39 | 44.8 | D | L | 0.53 | 51.4 | D | L | 0.49 | 48.6 | D |
| | TR | 0.65 | 26.2 | C | TR | 0.51 | 22.7 | C | TR | 0.56 | 24.2 | C |
| Allen Street and Grand Street (West) | | | | | | | | | | | | |
| Eastbound | TR | 0.71 | 35.9 | D | TR | 0.88 | 56.4 | E | TR | 0.88 | 50.6 | D |
| Westbound | L | 0.14 | 22.1 | C | L | 0.27 | 28.3 | C | L | 0.20 | 25.6 | C |
| | T | 0.31 | 23.2 | C | T | 0.25 | 24.5 | C | T | 0.24 | 23.5 | C |
| Southbound | L | 0.31 | 42.6 | D | L | 0.42 | 43.3 | D | L | 0.39 | 41.9 | D |
| | TR | 0.53 | 24.1 | C | TR | 0.47 | 21.0 | C | TR | 0.44 | 21.1 | C |
| Allen Street and Delancey Street | | | | | | | | | | | | |
| Eastbound | T | 0.94 | 48.0 | D | T | 0.84 | 30.4 | C | T | 0.85 | 31.1 | C |
| | R | 0.16 | 25.6 | C | R | 0.20 | 19.3 | B | R | 0.12 | 18.2 | B |
| Westbound | L | 0.86 | 51.6 | D | L | 0.97 | 87.4 | F | L | 1.00 | 93.0 | F |
| | TR | 0.63 | 12.4 | B | TR | 0.54 | 11.0 | B | TR | 0.54 | 11.0 | B |
| Northbound | T | 0.76 | 37.6 | D | T | 0.53 | 30.9 | C | T | 0.52 | 30.6 | C |
| | R | 0.35 | 10.8 | B | R | 0.50 | 19.4 | B | R | 0.60 | 22.5 | C |
| Southbound | TR | 0.40 | 28.7 | C | TR | 0.38 | 28.3 | C | TR | 0.49 | 30.1 | C |
| Bowery and Canal Street | | | | | | | | | | | | |
| Eastbound | T | 0.79 | 29.4 | C | T | 0.79 | 29.3 | C | T | 1.03 | 61.0 | E |
| | R | 0.32 | 20.3 | C | R | 0.24 | 19.1 | B | R | 0.16 | 18.0 | B |
| Westbound | T | 0.80 | 29.5 | C | T | 0.63 | 24.4 | C | T | 0.43 | 20.6 | C |
| Northbound | T | 0.56 | 33.2 | C | T | 0.51 | 32.1 | C | T | 0.43 | 30.6 | C |
| Southbound | DefL | 0.87 | 47.0 | D | DefL | 0.85 | 44.5 | D | DefL | 1.05 | 78.6 | E |
| | TR | 0.64 | 25.9 | C | TR | 0.61 | 25.0 | C | TR | 0.36 | 19.3 | B |
| Bowery and Bayard Street | | | | | | | | | | | | |
| Eastbound | LR | 0.29 | 22.8 | C | LR | 0.57 | 31.3 | C | LR | 0.65 | 35.1 | D |
| Northbound | T | 0.41 | 17.6 | B | T | 0.47 | 18.5 | B | T | 0.56 | 19.7 | B |
| Southbound | T | 0.22 | 15.7 | B | T | 0.19 | 15.4 | B | T | 0.13 | 14.9 | B |
| Bowery and Division Street/Doyers Street | | | | | | | | | | | | |
| Eastbound | R | 0.04 | 26.4 | C | R | 0.07 | 26.8 | C | R | 0.07 | 26.8 | C |
| Westbound | L | 0.66 | 46.2 | D | L | 0.72 | 49.5 | D | L | 0.57 | 41.1 | D |
| | R | 0.57 | 18.8 | B | R | 0.64 | 20.6 | C | R | 0.56 | 18.5 | B |
| Northbound | TR | 0.34 | 20.2 | C | TR | 0.38 | 20.7 | C | TR | 0.58 | 23.7 | C |
| Southbound | T | 0.34 | 20.3 | C | T | 0.35 | 20.3 | C | T | 0.22 | 18.8 | B |

Table 14-16 (cont'd)
Existing Conditions Level of Service Analysis
Signalized Intersections

| Intersection | Weekday AM | | | | Weekday Midday | | | | Weekday PM | | | |
|--|------------|-----------|-------------|-----|----------------|-----------|-------------|-----|------------|-----------|-------------|-----|
| | Lane Group | v/c Ratio | Delay (sec) | LOS | Lane Group | v/c Ratio | Delay (sec) | LOS | Lane Group | v/c Ratio | Delay (sec) | LOS |
| Chatham Square and East Broadway | | | | | | | | | | | | |
| Westbound | L | 0.30 | 17.3 | B | L | 0.23 | 16.3 | B | L | 0.29 | 17.1 | B |
| | R | 0.15 | 15.5 | B | R | 0.13 | 15.3 | B | R | 0.21 | 16.2 | B |
| Northbound | T | 0.22 | 15.8 | B | T | 0.29 | 16.5 | B | T | 0.44 | 18.3 | B |
| | R | 0.48 | 22.0 | C | R | 0.67 | 30.7 | C | R | 0.79 | 37.9 | D |
| Southbound | L | 0.62 | 28.5 | C | L | 0.74 | 37.7 | D | L | 0.61 | 30.9 | C |
| | T | 0.28 | 16.3 | B | T | 0.25 | 16.0 | B | T | 0.18 | 15.4 | B |
| Chatham Square and Worth Street/Oliver Street | | | | | | | | | | | | |
| Eastbound (Worth Street) | L | 1.05 | 140.6 | F | L | 0.98 | 101.1 | F | L | 1.05 | 106.5 | F |
| | LTR | 0.96 | 86.2 | F | LTR | 0.89 | 66.0 | E | LTR | 1.04 | 94.5 | F |
| Eastbound (Mott Street) | LTR | 0.56 | 42.2 | D | LTR | 0.61 | 44.3 | D | LTR | 0.79 | 56.7 | E |
| Westbound | LT | 0.82 | 41.4 | D | LT | 0.53 | 29.3 | C | LT | 0.49 | 28.1 | C |
| | R | 0.69 | 39.0 | D | R | 0.80 | 48.4 | D | R | 0.99 | 78.6 | E |
| Northbound | LTR | 0.08 | 21.4 | C | LTR | 0.11 | 21.7 | C | LTR | 0.08 | 21.4 | C |
| Southbound | L | 0.93 | 73.7 | E | L | 0.65 | 39.3 | D | L | 0.67 | 40.7 | D |
| | TR | 0.88 | 50.6 | D | TR | 1.01 | 80.2 | F | TR | 0.86 | 50.0 | D |
| Worth Street and Centre Street | | | | | | | | | | | | |
| Eastbound | L | 0.30 | 17.5 | B | L | 0.23 | 11.7 | B | L | 0.20 | 11.0 | B |
| | T | 0.50 | 18.0 | B | T | 0.40 | 12.9 | B | T | 0.65 | 17.9 | B |
| Westbound | T | 0.44 | 26.6 | C | T | 0.28 | 19.6 | B | T | 0.24 | 19.0 | B |
| | R | 0.79 | 48.6 | D | R | 0.47 | 25.3 | C | R | 0.39 | 22.2 | C |
| Northbound | L | 0.11 | 17.7 | B | L | 0.22 | 23.7 | C | L | 0.13 | 21.6 | C |
| | TR | 0.59 | 23.8 | C | TR | 0.60 | 28.3 | C | TR | 0.62 | 28.1 | C |
| Worth Street and Lafayette Street | | | | | | | | | | | | |
| Eastbound | TR | 0.53 | 25.8 | C | TR | 0.52 | 25.7 | C | TR | 0.59 | 27.0 | C |
| Westbound | L | 0.65 | 34.0 | C | L | 0.71 | 37.9 | D | L | 0.52 | 30.1 | C |
| Southbound | LT | 0.72 | 27.3 | C | LT | 0.64 | 25.2 | C | LT | 0.70 | 26.1 | C |
| Worth Street and Broadway | | | | | | | | | | | | |
| Eastbound | TR | 0.56 | 25.5 | C | TR | 0.48 | 23.6 | C | TR | 0.53 | 24.6 | C |
| Southbound | LT | 0.47 | 15.9 | B | LT | 0.46 | 15.8 | B | LT | 0.66 | 19.4 | B |

Notes: L = Left Turn, T = Through, R = Right Turn, DefL = Defacto Left Turn, LOS = Level of Service

Table 14-17
Existing Conditions Level of Service Analysis
Unsignalized Intersections

| Intersection | Weekday AM | | | | Weekday Midday | | | | Weekday PM | | | |
|---|------------|-----------|-------------|-----|----------------|-----------|-------------|-----|------------|-----------|-------------|-----|
| | Lane Group | v/c Ratio | Delay (sec) | LOS | Lane Group | v/c Ratio | Delay (sec) | LOS | Lane Group | v/c Ratio | Delay (sec) | LOS |
| Cherry Street and Clinton Street | | | | | | | | | | | | |
| Westbound | TR | 0.14 | 7.9 | A | TR | 0.13 | 7.9 | A | TR | 0.20 | 8.4 | A |
| Northbound | LT | 0.21 | 8.4 | A | LT | 0.23 | 8.6 | A | LT | 0.30 | 9.3 | A |
| Pike Street and Monroe Street | | | | | | | | | | | | |
| Eastbound | R | 0.70 | 11.2 | B | R | 0.08 | 11.4 | B | R | 0.08 | 11.2 | B |

Notes: L = Left Turn, T = Through, R = Right Turn, DefL = Defacto Left Turn, LOS = Level of Service

- Eastbound approach at the South Street and Clinton Street intersection (LOS D with a v/c ratio of 0.96 and a delay of 52.7 seconds per vehicle [spv] during the weekday PM peak hour);
- Westbound approach at the South Street and Montgomery Street (north) intersection (LOS E with a v/c ratio of 1.05 and a delay of 63.9 spv during the weekday PM peak hour);
- Southbound approach at the South Street and Montgomery Street (south) intersection (LOS F with a v/c ratio of 1.05 and a delay of 96.3 spv during the weekday PM peak hour);

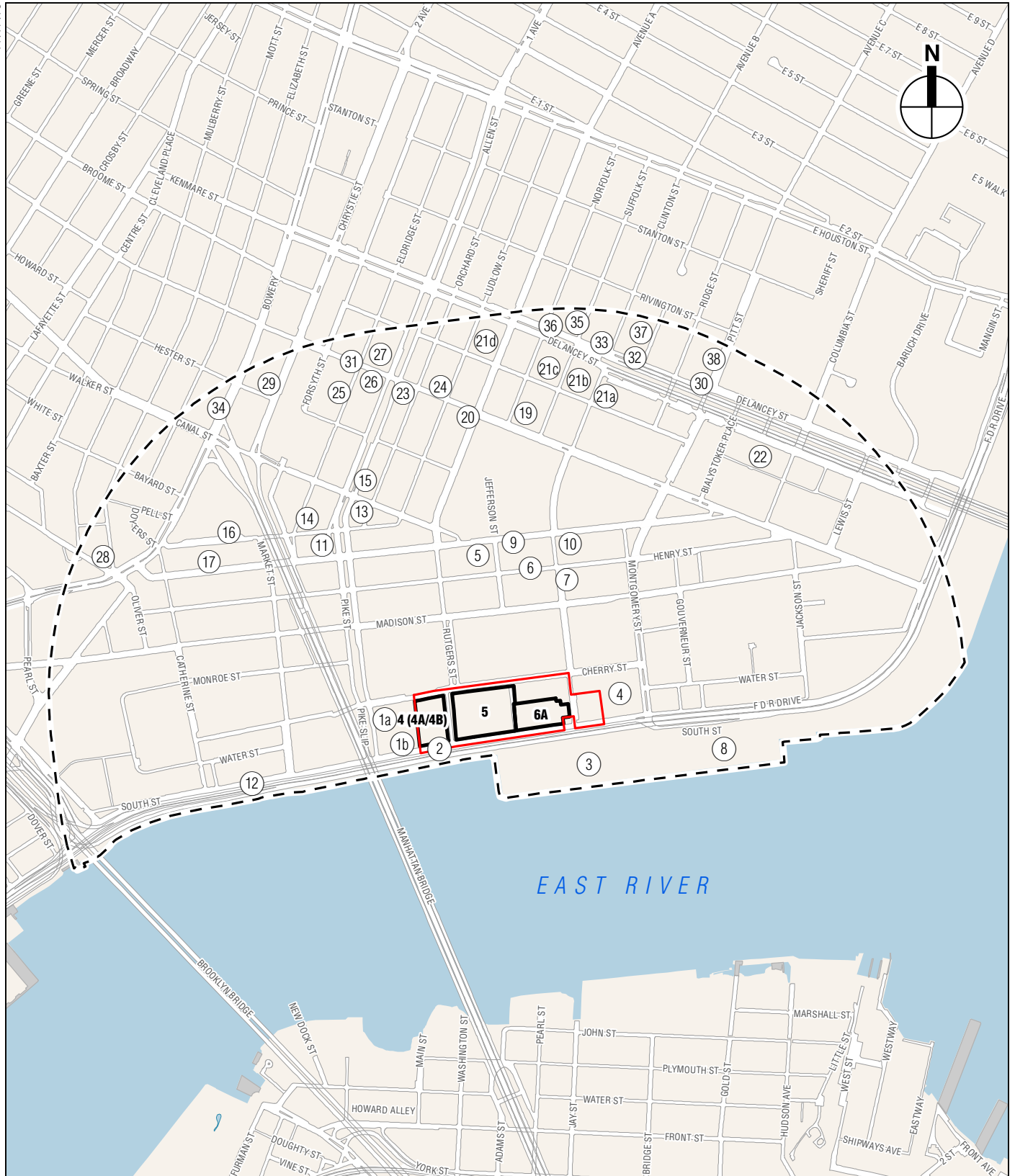
Two Bridges LSRD

- Eastbound left-turn at the Madison Street and Pike Street (east) intersection (LOS F with a v/c ratio of 1.05 and a delay of 110.1 spv during the weekday AM peak hour, LOS D with a v/c ratio of 0.72 and a delay of 49.6 spv during the weekday midday peak hour, and LOS E with a v/c ratio of 0.86 and a delay of 73.4 spv during the weekday PM peak hour);
- Eastbound approach at the Madison Street and Pike Street (west) intersection (LOS D with a v/c ratio of 0.83 and a delay of 45.5 spv during the weekday AM peak hour, and LOS D with a v/c ratio of 0.80 and a delay of 45.2 spv during the weekday PM peak hour);
- Northbound approach at the Madison Street and Montgomery Street intersection (LOS E with a v/c ratio of 0.97 and a delay of 64.1 spv during the weekday PM peak hour);
- Eastbound left-turn at the East Broadway and Pike Street (east) intersection (LOS E with a v/c ratio of 0.80 and a delay of 56.0 spv during the weekday PM peak hour);
- Northbound left-turn at the East Broadway and Pike Street (east) intersection (LOS E with a v/c ratio of 0.59 and a delay of 55.0 spv during the weekday AM peak hour, LOS D with a v/c ratio of 0.52 and a delay of 50.9 spv during the weekday midday peak hour, LOS E with a v/c ratio of 0.78 and a delay of 71.1 spv during the weekday PM peak hour);
- Eastbound approach at the East Broadway and Pike Street (west) intersection (LOS E with a v/c ratio of 0.92 and a delay of 57.2 spv during the weekday AM peak hour, LOS E with a v/c ratio of 0.95 and a delay of 63.1 spv during the weekday midday peak hour, LOS E with a v/c ratio of 0.99 and a delay of 70.1 spv during the weekday PM peak hour);
- Southbound left-turn at the East Broadway and Pike Street (west) intersection (LOS D with a v/c ratio of 0.33 and a delay of 46.4 spv during the weekday AM peak hour, LOS D with a v/c ratio of 0.33 and a delay of 46.0 spv during the weekday midday peak hour, LOS D with a v/c ratio of 0.31 and a delay of 45.1 spv during the weekday PM peak hour);
- Northbound left-turn at the Division Street and Market Street intersection (LOS D with a v/c ratio of 0.86 and a delay of 47.2 spv during the weekday midday peak hour);
- Northbound left-turn at the Division Street and Allen Street/Pike Street intersection (LOS D with a v/c ratio of 0.46 and a delay of 47.4 spv during the weekday AM peak hour, LOS E with a v/c ratio of 0.64 and a delay of 58.1 spv during the weekday midday peak hour, and LOS D with a v/c ratio of 0.51 and a delay of 49.2 spv during the weekday PM peak hour);
- Eastbound approach at Allen Street and Canal Street intersection (LOS F with a v/c ratio of 1.05 and a delay of 87.4 spv during the weekday AM peak hour, and LOS F with a v/c ratio 1.04 and a delay of 83.0 spv during the weekday PM peak hour);
- Northbound left-turn at Allen Street and Grand Street (east) intersection (LOS D with a v/c ratio of 0.53 and a delay of 51.4 spv during the weekday midday peak hour, and LOS D with a v/c ratio of 0.49 and a delay of 48.6 spv during the weekday PM peak hour);
- Eastbound approach at the Allen Street and Grand Street (west) intersection (LOS E with a v/c ratio of 0.88 and 56.4 spv during the weekday midday peak hour, and LOS D with a v/c ratio of 0.88 and a delay of 50.6 spv during the weekday PM peak hour);
- Eastbound through at the Allen Street and Delancey Street intersection (LOS D with a v/c ratio of 0.94 and a delay of 48.0 spv during the weekday AM peak hour);
- Westbound left-turn at the Allen Street and Delancey Street intersection (LOS D with a v/c ratio of 0.86 and a delay of 51.6 spv during the weekday AM peak hour, LOS F with a v/c ratio of 0.97 and a delay of 87.4 spv during the weekday midday peak hour, and LOS F with a v/c ratio of 1.00 and a delay of 93.0 spv during the weekday PM peak hour);

- Eastbound through at The Bowery and Canal Street intersection (LOS E with a v/c ratio of 1.03 and a delay of 61.0 spv during the weekday PM peak hour);
- Southbound defacto left-turn at The Bowery and Canal Street intersection (LOS D with a v/c ratio of 0.87 and a delay of 47.0 spv during the weekday AM peak hour, and LOS E with a v/c ratio of 1.05 and a delay of 78.6 spv during the weekday PM peak hour);
- Westbound left-turn at The Bowery and Division Street/Doyers Street intersection (LOS D with a v/c ratio of 0.66 and a delay of 46.2 spv during the weekday AM peak hour, and LOS D with a v/c ratio of 0.72 and a delay of 49.5 spv during the weekday midday peak hour);
- Eastbound (Worth Street) left-turn at the Chatham Square and Worth Street/Oliver Street intersection (LOS F with a v/c ratio of 1.05 and a delay of 140.6 spv during the weekday AM peak hour, LOS F with a v/c ratio of 0.98 and a delay of 101.1 spv during the weekday midday peak hour, LOS F with a v/c ratio of 1.05 and a delay of 106.5 spv during the weekday PM peak hour);
- Eastbound (Worth Street) shared lane at the Chatham Square and Worth Street/Oliver Street intersection (LOS F with a v/c ratio of 0.96 and a delay of 86.2 spv during the weekday AM peak hour, LOS E with a v/c ratio of 0.89 and a delay of 66.0 spv during the weekday midday peak hour, LOS F with a v/c ratio of 1.04 and a delay of 94.5 spv during the weekday PM peak hour);
- Eastbound (Mott Street) approach at the Chatham Square and Worth Street/Oliver Street intersection (LOS E with a v/c of 0.79 and a delay of 56.7 spv during the weekday PM peak hour);
- Westbound left-turn at the Chatham Square and Worth Street/Oliver Street intersection (LOS D with a v/c ratio of 0.80 and a delay of 48.4 spv during the weekday midday peak hour, and LOS E with a v/c ratio of 0.99 and a delay of 78.6 spv during the weekday PM peak hour);
- Southbound left-turn at the Chatham Square and Worth Street/Oliver Street intersection (LOS E with a v/c ratio of 0.93 and a delay of 73.7 spv during the weekday AM peak hour); and
- Southbound shared lane at the Chatham Square and Worth Street/Oliver Street intersection (LOS D with a v/c ratio of 0.88 and a delay of 50.6 spv during the weekday AM peak hour, LOS F with a v/c ratio of 1.01 and a delay of 80.2 spv during the weekday midday peak hour, LOS D with a v/c ratio of 0.86 and a delay of 50.0 spv during the weekday PM peak hour).

THE FUTURE WITHOUT THE PROPOSED PROJECTS

The No Action condition was developed by increasing the existing traffic levels by the expected growth in overall travel through and within the study area. As per *CEQR Technical Manual* guidelines, an annual background growth rate of 0.25 percent was applied to grow traffic to the proposed projects' anticipated build year of 2021. A total of ~~37~~³⁸ development projects expected to occur in the No Action condition (No Build projects) were identified as being planned for the ½-mile study area (see **Figure 14-13**). After reviewing the development programs for each of the planned projects, it was determined that an additional three percent of background growth will address the increase in traffic and pedestrian levels for the ~~34~~³⁶ small-to moderate-sized projects in the study area. **Table 14-18** and **Figure 14-13** summarize the projects that were accounted for in this future 2021 baseline.



- Project Sites
- Boundary of Two Bridges LSRD
- Study Area (1/2-mile boundary)
- ① No Build Projects

TWO BRIDGES LSRD

No Build Projects
Figure 14-13

Two Bridges LSRD

As discussed above in the “Level 1 Screening Assessment” section of Section B, “Preliminary Analysis Methodology and Screening Assessment,” absent the proposed projects, existing uses on the project sites are expected to remain unchanged.

Table 14-18
No Action-Build Projects Anticipated to be Complete by 2021

| Map No. | Address/Name (Block/Lot) | Program | Transportation Assumptions | Build Year |
|--|---|--|--|----------------------|
| 400-Foot Study Area¹ | | | | |
| 1a | One Manhattan Square— 250 South Street-Extell (248/7501) | 815 DU, 23,167 sf retail | Transportation assumptions from <i>CEQR Technical Manual, Seward Park Mixed Use Development Project FGEIS (2012), U.S. Census Bureau American Community Survey 2011–2015 Journey to Work estimates, and U.S. Census Bureau American Community Survey 2006–2010 Reverse Journey to Work estimates</i> | 2021 |
| 1b | One Manhattan Square— 229 Cherry Street-Extell (248/75014) | 205 DU, 25,516 sf retail | Transportation assumptions from <i>CEQR Technical Manual, Seward Park Mixed Use Development Project FGEIS (2012), U.S. Census Bureau American Community Survey 2011–2015 Journey to Work estimates, and U.S. Census Bureau American Community Survey 2006–2010 Reverse Journey to Work estimates</i> | 2021 |
| <u>2</u> | Lower Manhattan Coastal Resiliency Project (LMCR) ^{3#} | Integrated flood protection system | Included in background growth | 2023 [MOVED] |
| 2 | P.S. 184 Playground (245/7) | Soccer field (1.15 acres) | Included in background growth | 2024 |
| 3 | Pier 35 | 0.02 acres open space | Included in background growth | 2018 2019 |
| 4 | P.S. 184 Playground (245/7) | Soccer field (1.15 acres) | Included in background growth | 2021 [MOVED] |
| ¼-Mile Study Area | | | | |
| <u>5</u> | 183 East Broadway (284/19) | 20 DU, 2,035 sf retail, 1,279 sf CF | Included in background growth | 2021 [MOVED] |
| 4 | Pier 42 | 5.05 acres open space | Included in background growth | 2020 |
| 5 | 205 Henry Street (285/14) | 10 DU, 1,319 sf retail | Included in background growth | 2024 |
| 6 | 193 Henry Street (285/8) | 5 DU, 1,355 sf retail, 384 sf CF | Included in background growth | 2021 |
| <u>7</u> | 205 Henry Street (285/14) | 10 DU, 1,319 sf retail | Included in background growth | 2021 [MOVED] |
| <u>8</u> | Pier 42 | 5.05 acres open space | Included in background growth | 2020 [MOVED] |
| 7 | 183 East Broadway (284/19) | 20 DU, 2,035 sf retail, 1,279 sf CF | Included in background growth | 2024 |
| 8 | 225 East Broadway (286/35) | 22 DU | Included in background growth | 2024 |
| 9 | 201 East Broadway (285/25) | 10 DU, 3,617 sf retail, 1,968 sf CF | Included in background growth | 2021 |
| <u>10</u> | 225 East Broadway (286/35) | 22 DU | Included in background growth | 2021 [MOVED] |
| 12 <u>11</u> | 2 Pike Street/100 East Broadway (282/58) | 58,830 sf office, 4,900 sf CF | Included in background growth | 2021 [MOVED] |
| 13 <u>12</u> | East River Waterfront Esplanade-Phase IV (240/6), btwn Catherine Slip and Pike Slip | Resurfacing, new seating, play equipment | Included in background growth | 2021 [MOVED] |

Table 14-18 (cont'd)
No Action Projects Anticipated to be Complete by 2021

| Map No. | Address/Name (Block/Lot) | Program | Transportation Assumptions | Build Year |
|--|---|---|--|-----------------|
| <u>1/4-Mile / Census Tract Study Area</u> | | | | |
| <u>44</u> <u>13</u> | 9 Orchard Street (294/8) | 60,000 sf office | Included in background growth | 2021 [MOVED] |
| <u>45</u> <u>14</u> | 10 Eldridge Street (293/2) | 7,765 sf retail | Included in background growth | 2021 [MOVED] |
| <u>46</u> <u>15</u> | 61 Canal Street (299/35) | 2,268 sf retail, 6,510 sf CF | Included in background growth | 2021 [MOVED] |
| <u>16</u> | 35 Division Street (281/46) | 14,203 sf CF | Included in background growth | 2021 [MOVED] |
| <u>17</u> | 42 East Broadway (281/19) | 11,485 sf retail | Included in background growth | 2022 [MOVED] |
| <u>18</u> | East Side Coastal Resiliency Project (ESCR) ^{3a} | Integrated flood protection system | Included in background growth | 2023 [MOVED] |
| <u>47</u> <u>19</u> | 50 Norfolk Street (346/1) | 300-488 DU, 34,600 <u>22,000</u> sf retail, 43,400 <u>46,000</u> sf CF | Included in background growth | 2021 [MOVED] |
| <u>20</u> | 355 Grand Street (310/20) | 2 DU, 1,958 sf retail | Included in background growth | 2021 [MOVED] |
| <u>21a</u> | Seward Park Mixed-Use Development – Essex Crossing Program (<u>Site 6: 178 Broome Street</u>) | 100 DU, 7,000 sf retail, 62,547 sf CF | Transportation assumptions from <i>Seward Park Mixed Use Development Technical Memorandum 003 (2015)</i> | 2021 [MOVED] |
| <u>48a</u> | Seward Park Mixed-Use Development – Essex Crossing Program (<u>Site 1: 236 Broome St</u>) | 55-DU, 6,933 sf retail, 43,100 sf | Transportation assumptions from <i>Seward Park Mixed Use Development Technical Memorandum 003 (2015)</i> | 2024 |
| <u>21b</u> | Seward Park Mixed-Use Development – Essex Crossing Program (<u>Site 4: 155 Delancey Street</u>) | 263 DU, 148,067 <u>68,478</u> sf retail, <u>138,210</u> sf office | Transportation assumptions from <i>Seward Park Mixed Use Development Technical Memorandum 003 (2015)</i> | 2021 [MOVED] |
| <u>48b</u> <u>21c</u> | Seward Park Mixed-Use Development – Essex Crossing Program (<u>Site 3: 135 Delancey Street</u>) | 97-83 DU, 72,758 <u>53,634</u> sf retail, 407,902 <u>127,132</u> sf office | Transportation assumptions from <i>Seward Park Mixed Use Development Technical Memorandum 003 (2015)</i> | 2021 [MOVED] |
| <u>21d</u> | Seward Park Mixed-Use Development – Essex Crossing Program (<u>Site 1: 236 Broome Street</u>) | 55 DU, 6,933 sf retail, 43,100 sf | Transportation assumptions from <i>Seward Park Mixed Use Development Technical Memorandum 003 (2015)</i> | 2021 [MOVED] |
| <u>48c</u> | Seward Park Mixed-Use Development – Essex Crossing Program (<u>Site 4</u>) | 263 DU, 148,067 sf retail | Transportation assumptions from <i>Seward Park Mixed Use Development Technical Memorandum 003 (2015)</i> | 2024 |
| <u>48d</u> | Seward Park Mixed-Use Development – Essex Crossing Program (<u>Site 5: 400 Grand Street</u>) | 211 DU, 72,743 sf retail, 75,000 sf CF, 0.34 acres open space | Transportation assumptions from <i>Seward Park Mixed Use Development Technical Memorandum 003 (2015)</i> | 2024 |
| <u>48e</u> | Seward Park Mixed-Use Development – Essex Crossing Program (<u>Site 6: 178 Broome St</u>) | 100 DU, 7,000 sf retail, 62,547 sf CF | Transportation assumptions from <i>Seward Park Mixed Use Development Technical Memorandum 003 (2015)</i> | 2024 |
| <u>48f</u> <u>21e</u> | Seward Park Mixed-Use Development – Essex Crossing Program (<u>Site 8: 140 Essex Street</u>) | 24-92 DU, 9,216 <u>9,700</u> sf retail | Transportation assumptions from <i>Seward Park Mixed Use Development Technical Memorandum 003 (2015)</i> | 2021 [MOVED] |
| <u>22</u> | 42 East Broadway (281/19) | 11,485 sf retail | Included in background growth | 2022 |
| <u>23</u> | Citywide Ferry Landing (Grand Street) (<u>262/25</u>) | Landing to connect to shoreline | Included in background growth | 2024 |
| <u>24</u> | 40 Allen Street (308/30) | 8 DU, 2,200 sf retail, 2,200 sf CF | Included in background growth | 2024 |
| <u>25</u> | 355 Grand Street (310/20) | 2 DU, 1,958 sf retail | Included in background growth | 2024 |

Table 14-18 (cont'd)
No Action Projects Anticipated to be Complete by 2021

| Map No. | Address/Name (Block/Lot) | Program | Transportation Assumptions | Build Year |
|---|--|------------------------------------|--------------------------------------|---------------------------|
| <u>2622</u> | 257 Delancey Street (331/95) | 758 sf CF | Included in background growth | 2021 [MOVED] |
| <u>23</u> | 66 Allen Street (308/14) | 8 DU | Included in background growth | 2021 [MOVED] |
| <u>24</u> | <u>330 Grand Street</u> | <u>12 DU</u> | <u>Included in background growth</u> | <u>2021 [NEW PROGRAM]</u> |
| <u>27</u> | <u>91 Attorney Street (348/64)</u> | <u>44 DU</u> | <u>Included in background growth</u> | <u>2021</u> |
| <u>28</u> | <u>175 Delancey Street (347/46)</u> | <u>400 DU</u> | <u>Included in background growth</u> | <u>2018*</u> |
| <u>2925</u> | 79 Eldridge Street (306/29) | 48 hotel rooms, 1,243 sf CF | Included in background growth | 2021 [MOVED] |
| <u>26</u> | EV/LES Rezoning—PDS #11 (413/25) | 7 DU, 1,945 sf retail | Included in background growth | 2021 [MOVED] |
| <u>27</u> | EV/LES Rezoning—PDS #12 (413/26) | 14 DU, 3,749 sf retail | Included in background growth | 2021 [MOVED] |
| <u>28</u> | 5 Mott Street (164/53) | 2 DU, 4,574 sf retail, 2,121 sf CF | Included in background growth | 2021 [MOVED] |
| <u>29</u> | 77 Chrystie Street (304/34) | 7 DU, 10,520 sf retail | Included in background growth | 2021 [MOVED] |
| <u>30</u> | <u>206-208 Delancey Street (343/68)</u> | 69 DU, 8,352 sf CF | Included in background growth | 2021 |
| <u>31</u> | EV/LES Rezoning—PDS #24 (418/51,52, 53) | 14 DU, 3,726 sf retail | Included in background growth | 2021 [MOVED] |
| <u>3132</u> | EV/LES Rezoning—PDS #160 (348/70) | 18 DU | Included in background growth | 2021 [MOVED] |
| <u>33</u> | EV/LES Rezoning—PDS #159 (348/33) | 17 DU, 2,316 sf retail | Included in background growth | 2021 |
| <u>34</u> | <u>76 Bowery (203/24)</u> | <u>14,488 sf retail</u> | <u>Included in background growth</u> | <u>2021 [NEW]</u> |
| <u>35</u> | EV/LES Rezoning—PDS #32 (353/75,79,80,82,83) | 120 DU, 16,090 sf retail | Included in background growth | 2021 [MOVED] |
| <u>32</u> | EV/LES Rezoning—PDS #154 (343/63) | 18 DU | Included in background growth | 2021 |
| <u>33</u> | EV/LES Rezoning—PDS #159 (348/33) | 17 DU, 2,316 sf retail | Included in background growth | 2021 |
| <u>3436</u> | 98 <u>100</u> Norfolk Street (353/47) | 38 DU, 11,244 sf retail | Included in background growth | 2021 [MOVED] |
| <u>37</u> | 91 Attorney Street (348/64) | 44 DU | Included in background growth | 2021 [MOVED] |
| <u>35</u> | <u>77 Chrystie Street (304/34)</u> | <u>7 DU, 10,520 sf retail</u> | <u>Included in background growth</u> | <u>2021</u> |
| <u>38</u> | EV/LES Rezoning—PDS #154 (343/63) | 18 DU | Included in background growth | 2021 [MOVED] |
| <u>36</u> | EV/LES Rezoning—PDS #32 (353/75,79,80,82,83) | 120 DU, 16,090 sf retail | Included in background growth | 2021 |
| <u>37</u> | 8 Allen Street (294/7) | 9,898 sf retail | Included in background growth | 2021 |
| Note: | | | | |
| * #28 175 Delancey Street (347/46) was completed in January 2018. | | | | |

CHANGES TO THE STUDY AREA STREET NETWORK

In addition to the development projects noted above, as mentioned in the “Existing Conditions” section, ongoing street reconstruction along Worth Street is expected to be completed by 2019. Upon completion, it is anticipated that roadway operations/conditions along Worth Street would return to those prior to construction. Specifically, at the intersection of Worth Street and Lafayette Street, the eastbound approach will consist of one through lane and one dedicated right-turn lane, and the westbound approach one dedicated left-turn lane and one through lane.

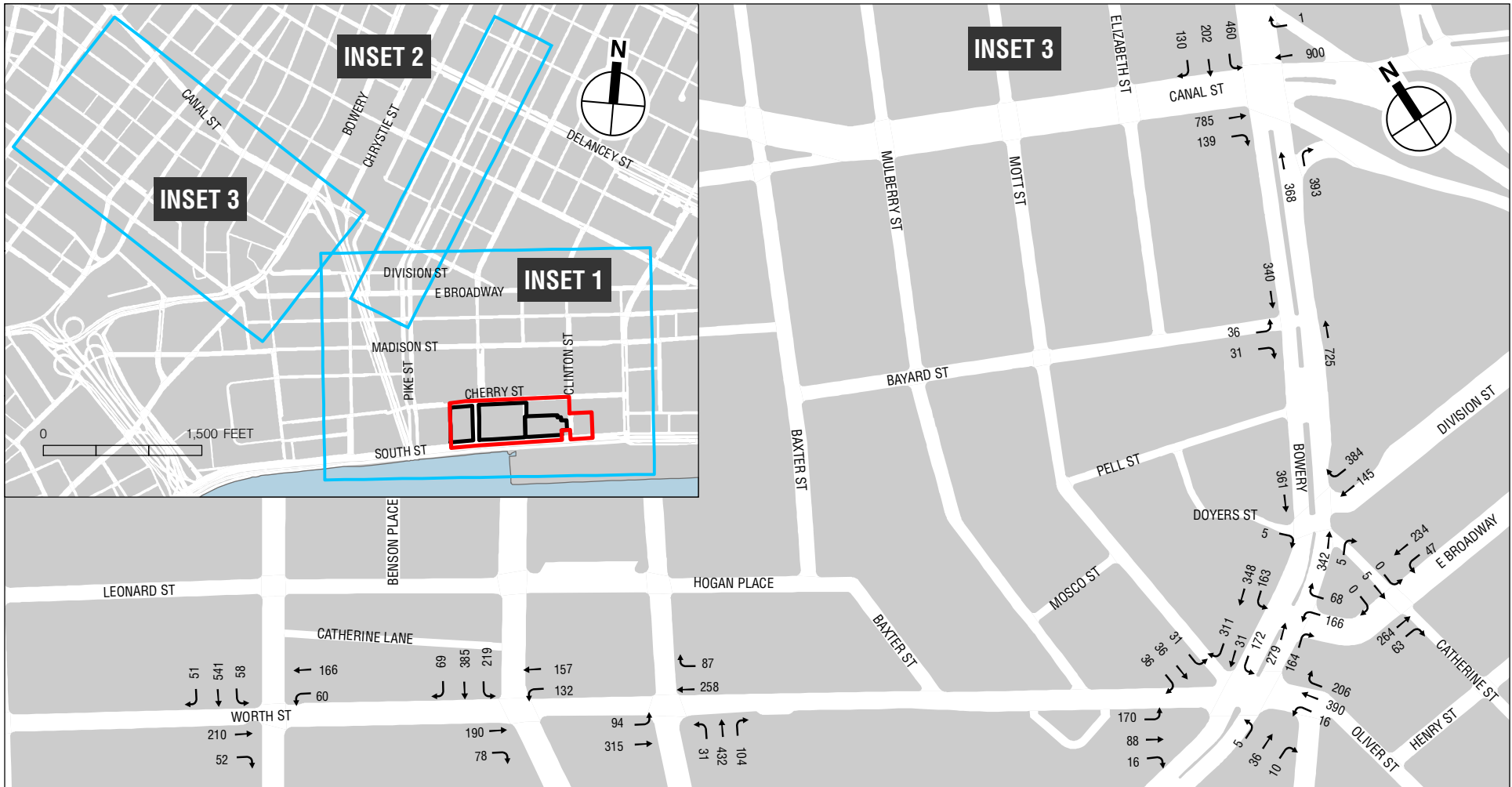
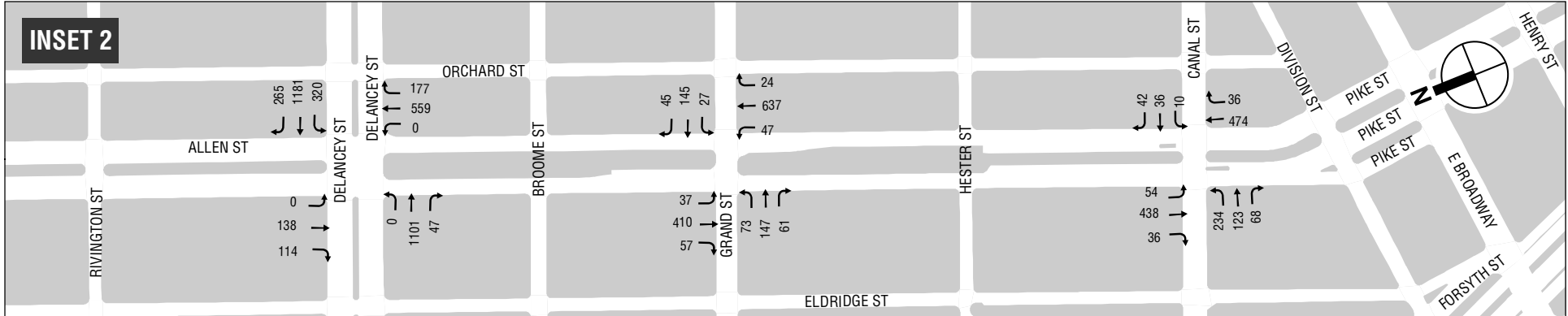
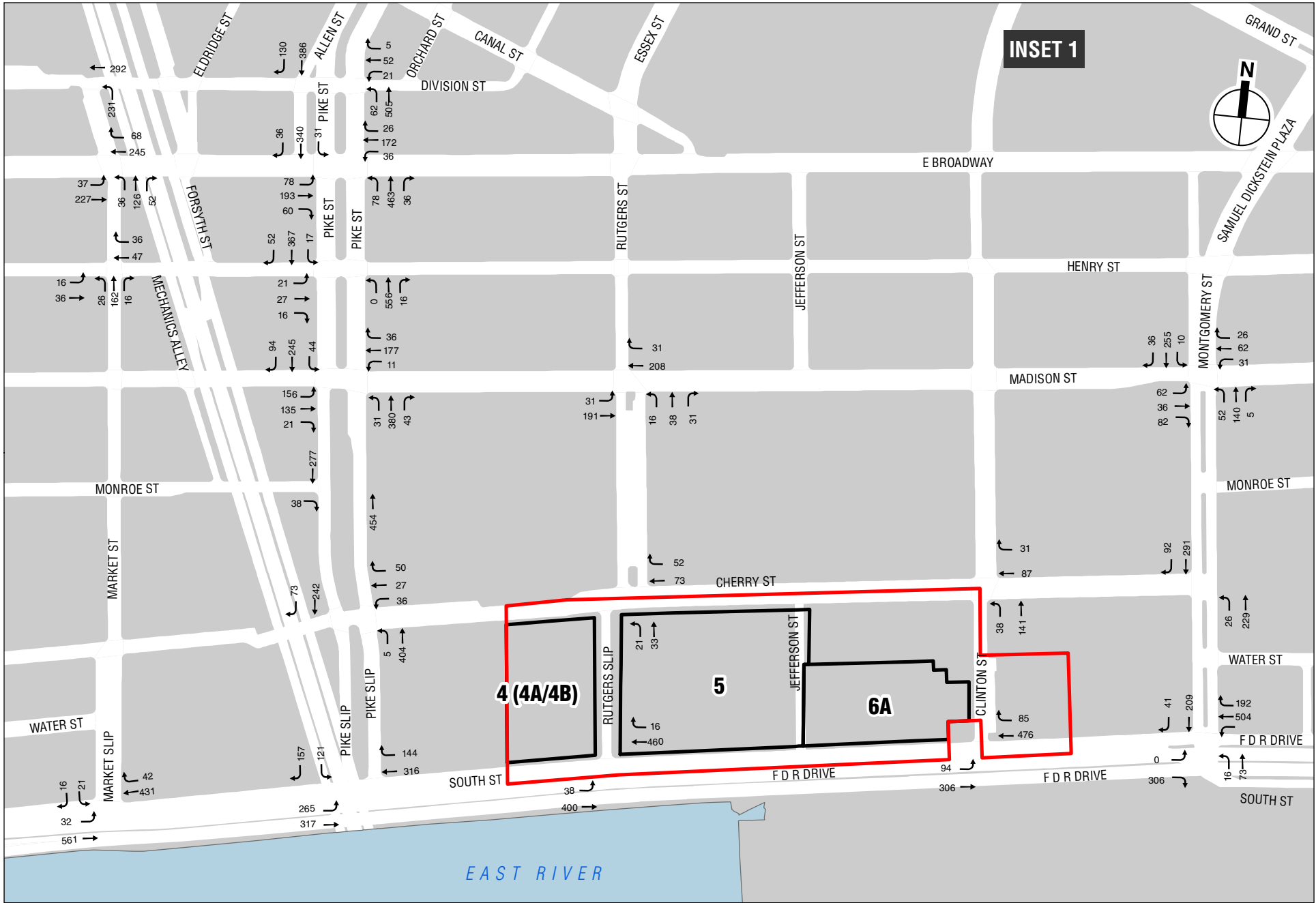
At the intersection of Worth Street and Broadway, westbound approach will consist of one dedicated left-turn lane and one through lane. All changes described above have been incorporated into the No Action analysis for the intersections along Worth Street.

TRAFFIC OPERATIONS

The No Action condition traffic volumes are shown in **Figures 14-14 through 14-16** for the weekday AM, midday, and PM peak hours, respectively. The No Action condition traffic volumes were projected by layering on top of the existing traffic volumes the following: background growth, additional three percent of traffic volume growth to account for small- to moderate-sized No Build projects within a ½-mile of the project sites, trips generated by two discrete No Build projects in the area, and traffic diversions due to current roadway reconstruction of Worth Street. A summary of the 2021 No Action condition traffic analysis results is presented in **Table 14-19**. Details on level-of-service, v/c ratios, and average delays are presented in **Tables 14-20 and 14-21**.

Table 14-19
Summary of 2021 No Action Traffic Analysis Results

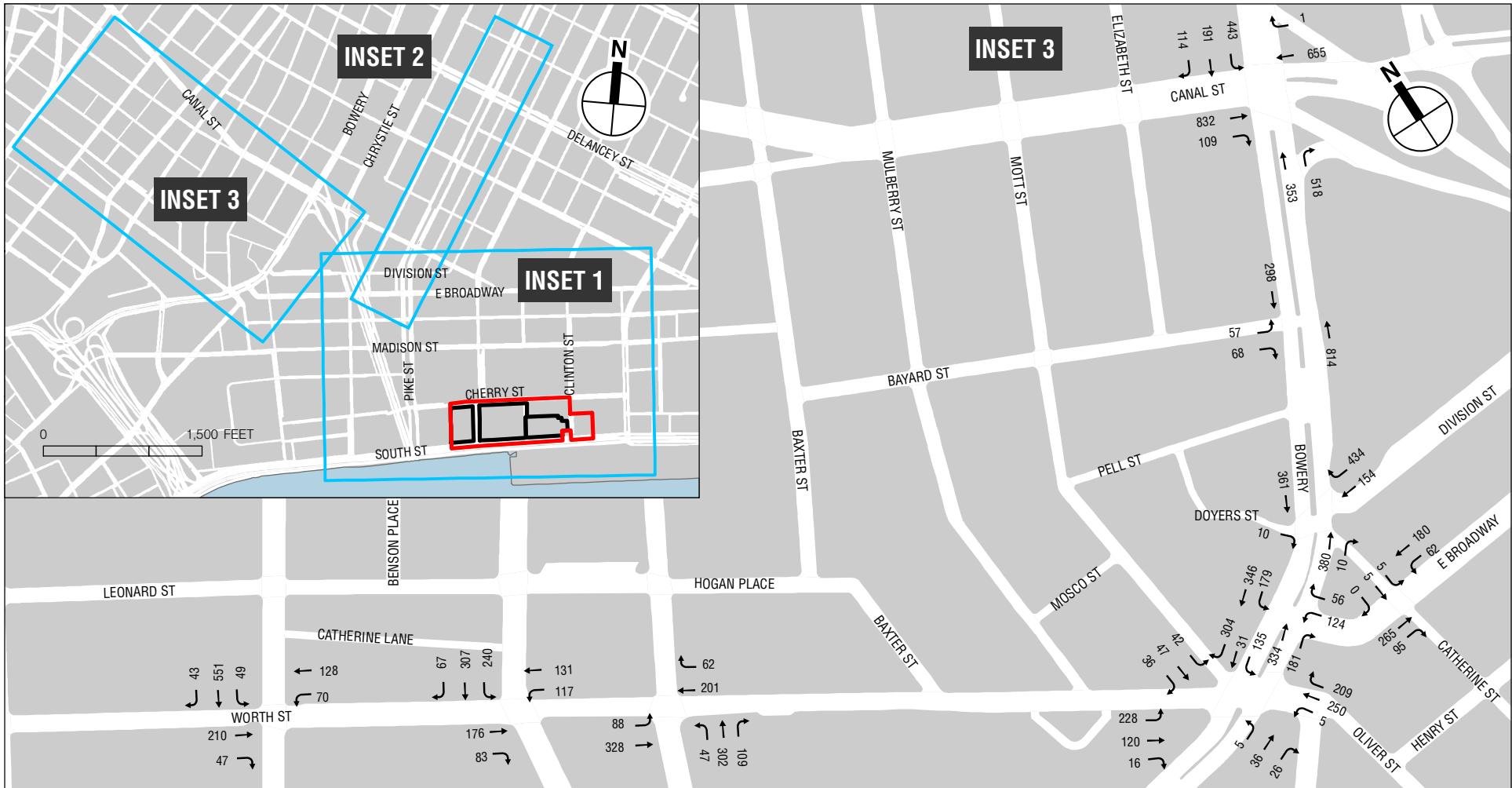
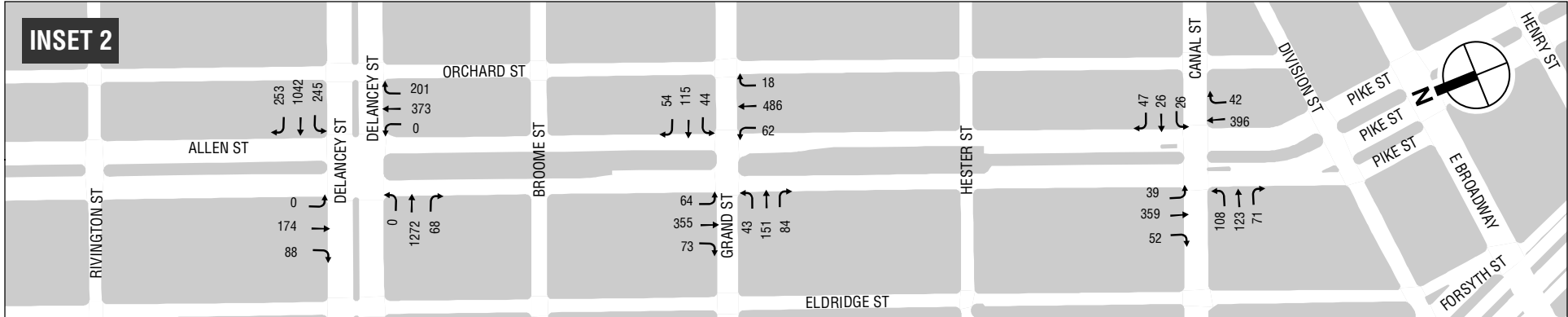
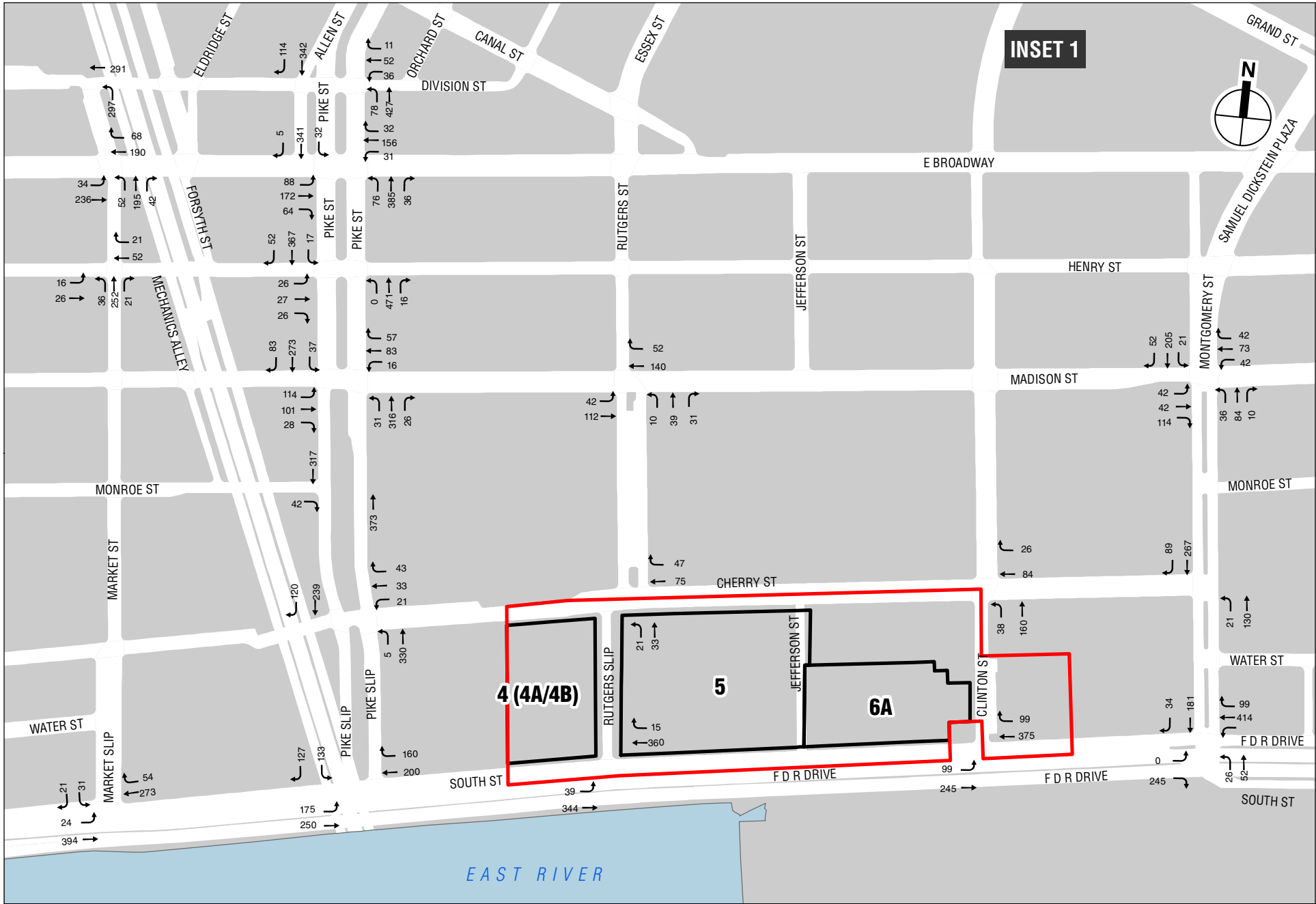
| Level of Service | Analysis Peak Hours | | |
|--|---------------------|----------------|------------|
| | Weekday AM | Weekday Midday | Weekday PM |
| Signalized Intersections | | | |
| Lane Groups at LOS A/B/C | 108 | 110 | 104 |
| Lane Groups at LOS D | 23 | 21 | 19 |
| Lane Groups at LOS E | 5 | 5 | 5 |
| Lane Groups at LOS F | 5 | 5 | 13 |
| Total | 141 | 141 | 141 |
| Lane Groups with v/c ≥ 0.90 | 11 | 8 | 16 |
| Unsignalized Intersections | | | |
| Lane Groups at LOS A/B/C | 3 | 3 | 3 |
| Lane Groups at LOS D | 0 | 0 | 0 |
| Lane Groups at LOS E | 0 | 0 | 0 |
| Lane Groups at LOS F | 0 | 0 | 0 |
| Total | 3 | 3 | 3 |
| Lane Groups with v/c ≥ 0.90 | 0 | 0 | 0 |
| Notes: LOS = Level-of-Service; v/c = volume-to-capacity ratio | | | |



 Project Sites

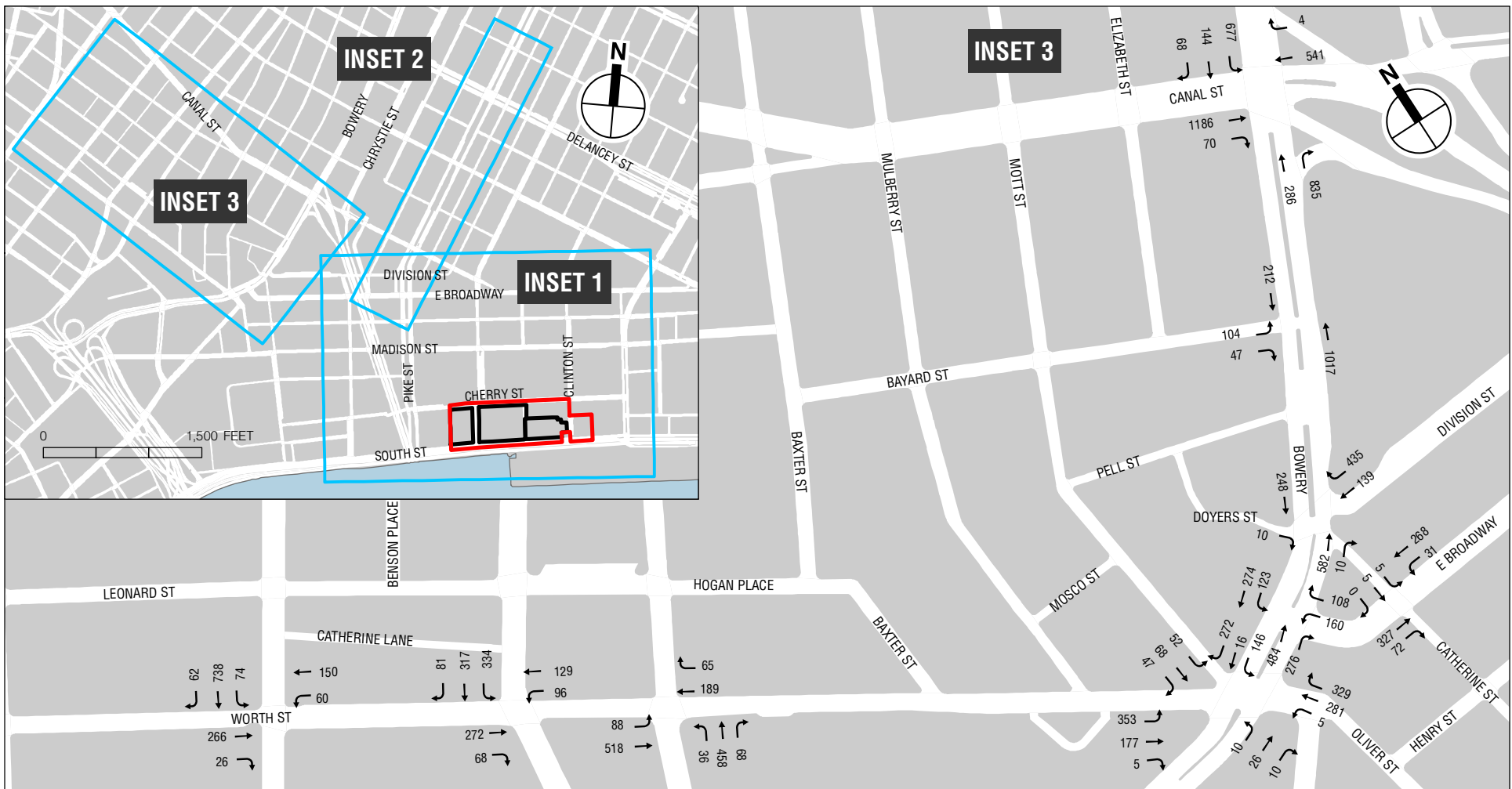
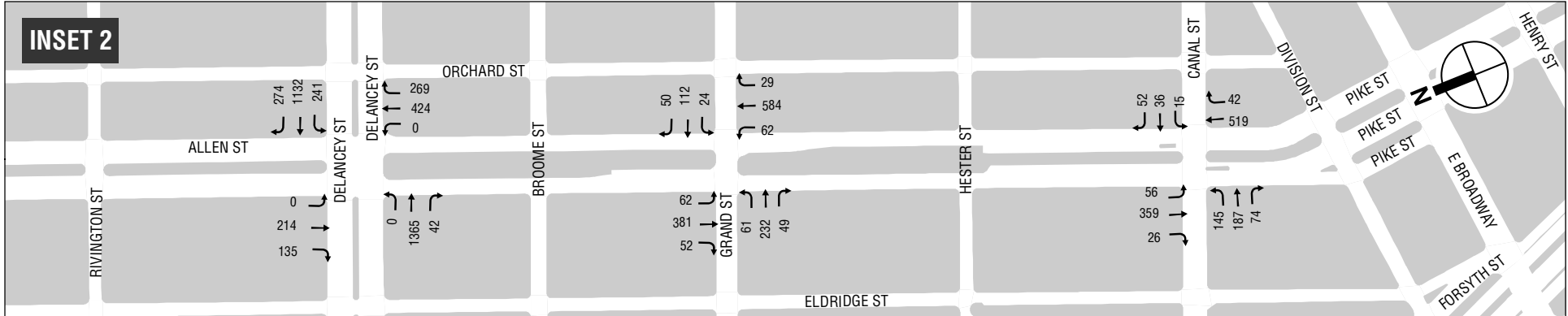
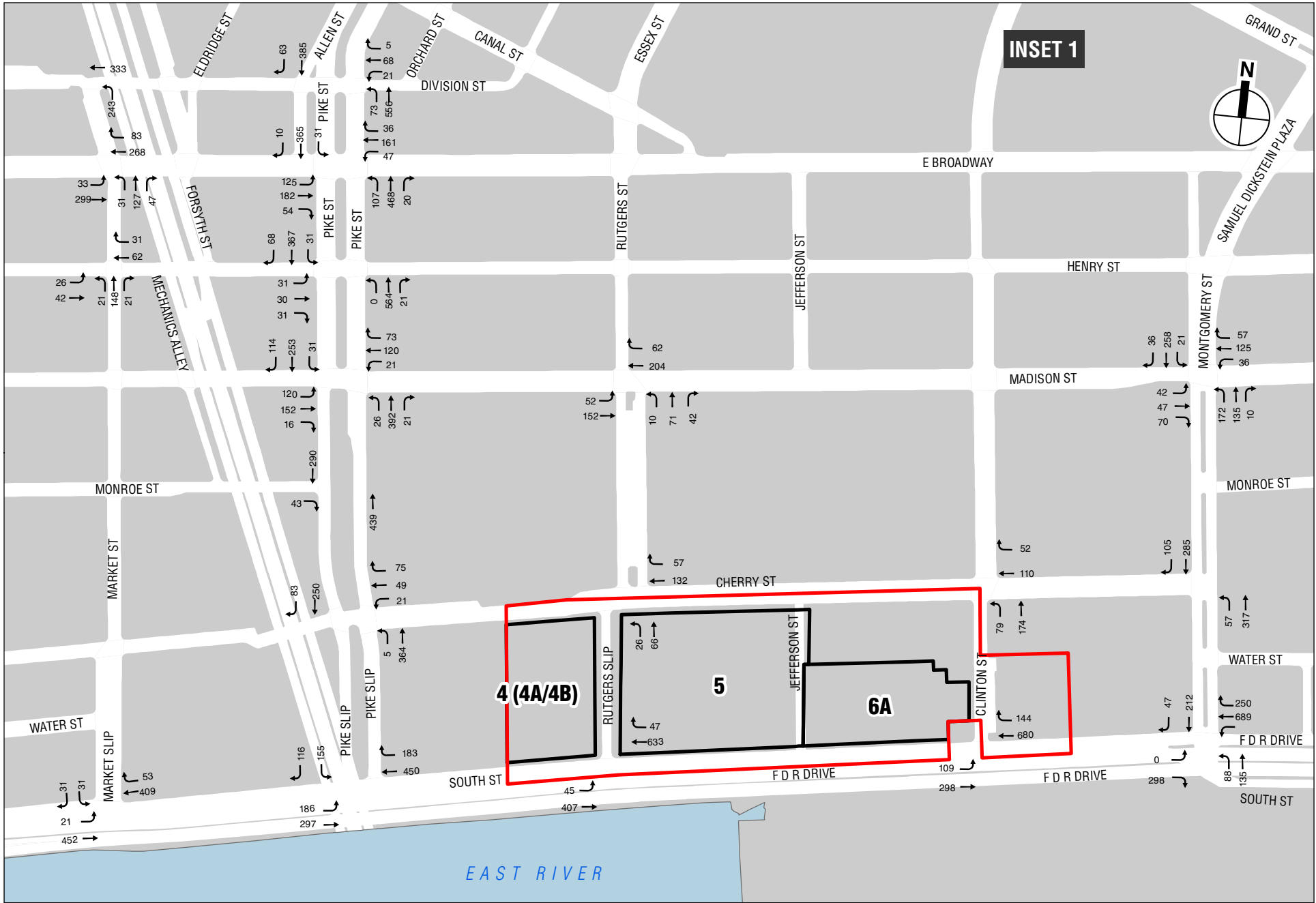
 Boundary of Two Bridges LSRD

2021 No Action Traffic Volumes
Weekday AM Peak Hour
Figure 14-14



 Project Sites
 Boundary of Two Bridges LSRD

2021 No Action Traffic Volumes
Weekday Midday Peak Hour
Figure 14-15



 Project Sites

 Boundary of Two Bridges LSRD

2021 No Action Traffic Volumes
Weekday PM Peak Hour
Figure 14-16

Two Bridges LSRD

Table 14-20

Existing and 2021 No Action Conditions Level of Service Analysis
Signalized Intersections

| Intersection | Weekday AM | | | | | | | | Weekday Midday | | | | | | | | Weekday PM | | | | | | | |
|--|------------|-----------|-------------|-----|------------|-----------|-------------|-----|----------------|-----------|-------------|-----|------------|-----------|-------------|-----|------------|-----------|-------------|-----|------------|-----------|-------------|-----|
| | Existing | | | | No Action | | | | Existing | | | | No Action | | | | Existing | | | | No Action | | | |
| | Lane Group | v/c Ratio | Delay (sec) | LOS | Lane Group | v/c Ratio | Delay (sec) | LOS | Lane Group | v/c Ratio | Delay (sec) | LOS | Lane Group | v/c Ratio | Delay (sec) | LOS | Lane Group | v/c Ratio | Delay (sec) | LOS | Lane Group | v/c Ratio | Delay (sec) | LOS |
| South Street and Market Slip | | | | | | | | | | | | | | | | | | | | | | | | |
| Eastbound | LT | 0.75 | 21.9 | C | LT | 0.79 | 24.2 | C | LT | 0.52 | 15.4 | B | LT | 0.55 | 16.2 | B | LT | 0.56 | 16.2 | B | LT | 0.61 | 17.3 | B |
| Westbound | TR | 0.59 | 16.5 | B | TR | 0.65 | 17.9 | B | TR | 0.36 | 12.7 | B | TR | 0.40 | 13.3 | B | TR | 0.51 | 15.0 | B | TR | 0.55 | 15.7 | B |
| Southbound | LR | 0.09 | 20.3 | C | LR | 0.09 | 20.9 | C | LR | 0.12 | 20.6 | C | LR | 0.12 | 20.3 | C | LR | 0.14 | 20.9 | C | LR | 0.15 | 20.9 | C |
| South Street and Pike Slip | | | | | | | | | | | | | | | | | | | | | | | | |
| Eastbound | L | 0.69 | 19.3 | B | L | 0.75 | 22.8 | C | L | 0.36 | 10.6 | B | L | 0.39 | 11.0 | B | L | 0.53 | 16.6 | B | L | 0.58 | 18.6 | B |
| Westbound | T | 0.59 | 25.7 | C | T | 0.61 | 26.4 | C | T | 0.44 | 22.6 | C | T | 0.46 | 23.0 | C | T | 0.48 | 23.2 | C | T | 0.50 | 23.6 | C |
| | T | 0.53 | 24.1 | C | T | 0.56 | 24.7 | C | T | 0.30 | 20.2 | C | T | 0.32 | 20.4 | C | T | 0.69 | 28.6 | C | T | 0.73 | 29.8 | C |
| | R | 0.35 | 21.5 | C | R | 0.39 | 22.2 | C | R | 0.40 | 22.4 | C | R | 0.42 | 22.9 | C | R | 0.40 | 22.4 | C | R | 0.43 | 23.0 | C |
| Southbound | L | 0.41 | 35.0 | D | L | 0.52 | 38.2 | D | L | 0.50 | 37.4 | D | L | 0.58 | 40.0 | D | L | 0.55 | 38.5 | D | L | 0.63 | 41.7 | D |
| | R | 0.52 | 38.5 | D | R | 0.63 | 42.9 | D | R | 0.47 | 36.8 | D | R | 0.60 | 41.5 | D | R | 0.43 | 35.6 | D | R | 0.51 | 37.7 | D |
| South Street and Rutgers Slip | | | | | | | | | | | | | | | | | | | | | | | | |
| Eastbound | LT | 0.54 | 15.5 | B | LT | 0.59 | 16.9 | B | LT | 0.50 | 15.0 | B | LT | 0.55 | 16.1 | B | LT | 0.63 | 17.9 | B | LT | 0.71 | 20.9 | C |
| Westbound | TR | 0.55 | 15.7 | B | TR | 0.59 | 16.3 | B | TR | 0.39 | 13.0 | B | TR | 0.41 | 13.3 | B | TR | 0.67 | 18.3 | B | TR | 0.71 | 19.4 | C |
| South Street and Clinton Street | | | | | | | | | | | | | | | | | | | | | | | | |
| Eastbound | LT | 0.63 | 19.1 | B | LT | 0.72 | 22.6 | C | LT | 0.70 | 21.9 | C | LT | 0.76 | 25.3 | C | LT | 0.96 | 52.7 | D | LT | 1.07 | 82.3 | F |
| Westbound | T | 0.57 | 16.2 | B | T | 0.61 | 17.2 | B | T | 0.51 | 15.1 | B | T | 0.53 | 15.6 | B | T | 0.79 | 23.7 | C | T | 0.83 | 26.4 | C |
| | R | 0.12 | 10.4 | B | R | 0.16 | 10.8 | B | R | 0.12 | 10.4 | B | R | 0.17 | 10.9 | B | R | 0.20 | 11.2 | B | R | 0.25 | 11.8 | B |
| South Street (North) and Montgomery Street | | | | | | | | | | | | | | | | | | | | | | | | |
| Westbound | LTR | 0.85 | 26.6 | C | LTR | 0.92 | 33.1 | C | LTR | 0.53 | 15.2 | B | LTR | 0.58 | 16.1 | B | LTR | 1.05 | 63.9 | E | LTR | 1.13 | 91.9 | F |
| Northbound | LT | 0.19 | 21.4 | C | LT | 0.20 | 21.5 | C | LT | 0.19 | 21.5 | C | LT | 0.20 | 21.7 | C | LT | 0.67 | 33.5 | C | LT | 0.83 | 47.4 | D |
| Southbound | TR | 0.53 | 28.1 | C | TR | 0.68 | 33.2 | C | TR | 0.40 | 25.2 | C | TR | 0.53 | 28.3 | C | TR | 0.50 | 27.4 | C | TR | 0.67 | 32.9 | C |
| South Street (South) and Montgomery Street | | | | | | | | | | | | | | | | | | | | | | | | |
| Eastbound | LTR | 0.35 | 12.5 | B | LTR | 0.39 | 13.0 | B | LTR | 0.27 | 11.7 | B | LTR | 0.29 | 11.8 | B | LTR | 0.36 | 12.7 | B | LTR | 0.39 | 13.0 | B |
| Northbound | TR | 0.11 | 20.5 | C | TR | 0.11 | 20.5 | C | TR | 0.15 | 21.1 | C | TR | 0.16 | 21.2 | C | TR | 0.46 | 25.6 | C | TR | 0.47 | 26.0 | C |
| Southbound | LT | 0.58 | 29.9 | C | LT | 0.74 | 37.2 | D | LT | 0.47 | 27.3 | C | LT | 0.64 | 32.9 | C | LT | 1.05 | 96.3 | F | LT | 1.43 | 243.3 | F |
| Cherry Street and Pike Street | | | | | | | | | | | | | | | | | | | | | | | | |
| Westbound | LTR | 0.24 | 24.4 | C | LTR | 0.34 | 26.2 | C | LTR | 0.21 | 23.9 | C | LTR | 0.28 | 25.0 | D | LTR | 0.35 | 26.2 | C | LTR | 0.42 | 27.5 | C |
| Northbound | L | 0.04 | 36.2 | D | L | 0.04 | 36.2 | D | L | 0.04 | 36.2 | D | L | 0.04 | 36.2 | D | L | 0.04 | 36.1 | D | L | 0.04 | 36.1 | D |
| Southbound | T | 0.29 | 10.1 | B | T | 0.31 | 10.3 | B | T | 0.22 | 9.5 | A | T | 0.24 | 9.7 | A | T | 0.26 | 9.8 | A | T | 0.27 | 9.9 | A |
| | TR | 0.28 | 18.3 | B | TR | 0.32 | 18.7 | B | TR | 0.31 | 18.6 | B | TR | 0.35 | 19.1 | B | TR | 0.29 | 18.3 | B | TR | 0.32 | 18.6 | B |
| Cherry Street and Rutgers Street | | | | | | | | | | | | | | | | | | | | | | | | |
| Westbound | TR | 0.21 | 16.1 | B | TR | 0.24 | 16.5 | B | TR | 0.19 | 15.9 | B | TR | 0.23 | 16.4 | B | TR | 0.29 | 17.1 | B | TR | 0.36 | 18.1 | B |
| Northbound | LT | 0.09 | 17.1 | B | LT | 0.11 | 17.3 | B | LT | 0.09 | 17.0 | B | LT | 0.11 | 17.4 | B | LT | 0.19 | 18.3 | B | LT | 0.22 | 18.8 | B |
| Cherry Street and Montgomery Street | | | | | | | | | | | | | | | | | | | | | | | | |
| Northbound | LT | 0.47 | 17.0 | B | LT | 0.49 | 17.5 | B | LT | 0.28 | 14.2 | B | LT | 0.30 | 14.4 | B | LT | 0.68 | 23.0 | C | LT | 0.74 | 25.5 | C |
| Southbound | TR | 0.60 | 20.2 | C | TR | 0.73 | 24.9 | C | TR | 0.49 | 17.2 | B | TR | 0.62 | 20.8 | C | TR | 0.57 | 19.4 | C | TR | 0.76 | 26.2 | C |
| Madison Street and Pike Street (East) | | | | | | | | | | | | | | | | | | | | | | | | |
| Eastbound | L | 1.05 | 110.1 | F | L | 1.14 | 140.0 | F | L | 0.72 | 49.6 | D | L | 0.78 | 56.3 | E | L | 0.86 | 73.4 | E | L | 0.93 | 89.3 | F |
| Westbound | T | 0.31 | 24.1 | C | T | 0.33 | 24.3 | C | T | 0.26 | 25.4 | C | T | 0.28 | 25.7 | C | T | 0.36 | 27.0 | C | T | 0.40 | 27.6 | C |
| | TR | 0.65 | 33.2 | C | TR | 0.68 | 34.5 | C | TR | 0.54 | 32.3 | C | TR | 0.57 | 33.2 | C | TR | 0.72 | 40.0 | D | TR | 0.75 | 42.4 | D |
| | L | 0.24 | 40.1 | D | L | 0.25 | 40.4 | D | L | 0.24 | 40.2 | D | L | 0.25 | 40.6 | D | L | 0.19 | 39.0 | D | L | 0.20 | 39.2 | D |
| Southbound | TR | 0.46 | 22.0 | C | TR | 0.51 | 22.9 | C | TR | 0.33 | 20.2 | C | TR | 0.37 | 20.8 | C | TR | 0.41 | 21.2 | C | TR | 0.45 | 21.7 | C |
| Madison Street and Pike Street (West) | | | | | | | | | | | | | | | | | | | | | | | | |
| Eastbound | TR | 0.83 | 45.5 | D | TR | 0.87 | 49.4 | D | TR | 0.73 | 40.2 | D | TR | 0.78 | 43.6 | D | TR | 0.80 | 45.2 | D | TR | 0.86 | 50.8 | D |
| Westbound | L | 0.08 | 21.5 | C | L | 0.10 | 22.0 | C | L | 0.12 | 24.5 | C | L | 0.14 | 25.0 | C | L | 0.19 | 26.4 | C | L | 0.21 | 27.2 | C |
| Southbound | T | 0.42 | 25.7 | C | T | 0.43 | 26.0 | C | T | 0.22 | 24.8 | C | T | 0.23 | 24.9 | C | T | 0.30 | 25.9 | C | T | 0.31 | 26.1 | C |
| | L | 0.35 | 43.9 | D | L | 0.39 | 45.1 | D | L | 0.24 | 37.2 | D | L | 0.25 | 37.4 | D | L | 0.19 | 36.0 | D | L | 0.20 | 36.2 | D |
| | TR | 0.36 | 20.7 | C | TR | 0.42 | 21.5 | C | TR | 0.37 | 18.8 | B | TR | 0.42 | 19.5 | B | TR | 0.38 | 18.9 | B | TR | 0.43 | 19.7 | B |
| Madison Street and Rutgers Street | | | | | | | | | | | | | | | | | | | | | | | | |
| Eastbound | LT | 0.37 | 12.8 | B | LT | 0.39 | 13.2 | B | LT | 0.29 | 12.0 | B | LT | 0.31 | 12.2 | B | LT | 0.40 | 13.5 | B | LT | 0.43 | 14.0 | B |
| Westbound | TR | 0.43 | 13.6 | B | TR | 0.45 | 14.0 | B | TR | 0.38 | 13.0 | B | TR | 0.39 | 13.3 | B | TR | 0.49 | 14.8 | B | TR | 0.51 | 15.2 | B |
| Northbound | LT | 0.14 | 21.7 | C | LT | 0.15 | 21.9 | C | LT | 0.11 | 21.3 | C | LT | 0.13 | 21.5 | C | LT | 0.19 | 22.2 | C | LT | 0.20 | 22.4 | C |
| | R | 0.08 | 20.9 | C | R | 0.08 | 20.9 | C | R | 0.08 | 21.0 | C | R | 0.09 | 21.0 | C | R | 0.11 | 21.2 | C | R | 0.11 | 21.3 | C |
| Madison Street and Montgomery Street | | | | | | | | | | | | | | | | | | | | | | | | |
| Eastbound | LTR | 0.46 | 21.0 | C | LTR | 0.49 | 21.7 | C | LTR | 0.43 | 20.2 | C | LTR | 0.47 | 21.0 | C | LTR | 0.39 | 19.3 | B | LTR | 0.43 | 20.1 | C |
| Westbound | LTR | 0.29 | 17.4 | B | LTR | 0.30 | 17.6 | B | LTR | 0.36 | 18.7 | B | LTR | 0.38 | 19.1 | B | LTR | 0.50 | 21.2 | C | LTR | 0.52 | 21.7 | C |
| Northbound | LTR | 0.45 | 20.1 | C | LTR | 0.47 | 20.7 | C | LTR | 0.30 | 17.5 | B | LTR | 0.31 | 17.8 | B | LTR | 0.97 | 64.1 | E | LTR | 1.14 | 117.4 | F |
| Southbound | LTR | 0.48 | 20.4 | C | LTR | 0.59 | 23.1 | C | LTR | 0.45 | 20.0 | C | LTR | 0.58 | 23.1 | C | LTR | 0.47 | 20.5 | C | LTR | 0.61 | 23.8 | C |
| Henry Street and Market Street | | | | | | | | | | | | | | | | | | | | | | | | |
| Eastbound | LT | 0.14 | 15.4 | B | LT | 0.14 | 15.5 | B | LT | 0.12 | 15.3 | B | LT | 0.13 | 15.3 | B | LT | 0.19 | 16.1 | B | LT | 0.19 | 16.2 | B |
| Westbound | TR | 0.24 | 17.0 | B | TR | 0.25 | 17.1 | B | TR | 0.18 | 16.0 | B | TR | 0.19 | 16.1 | B | TR | 0.22 | 16.5 | B | TR | 0.24 | 16.7 | B |
| Northbound | LTR | 0.39 | 18.8 | B | LTR | 0.41 | 19.3 | B | LTR | 0.62 | 24.1 | C | LTR | 0.65 | 25.1 | C | LTR | 0.36 | 18.3 | B | LTR | 0.38 | 18.6 | B |
| Henry Street and Pike Street | | | | | | | | | | | | | | | | | | | | | | | | |
| Eastbound | LTR | 0.17 | 23.4 | C | LTR | 0.18 | 23.5 | C | LTR | 0.21 | 23.8 | C | LTR | 0.22 | 24.0 | C | LTR | 0.23 | 24.3 | C | LTR | 0.26 | 24.6 | C |
| Northbound | TR | 0.59 | 23.2 | C | TR | 0.64 | 24.3 | C | TR | 0.52 | 21.8 | C | TR | 0.57 | 22.6 | C | TR | 0.53 | 21.8 | C | TR | 0.57 | 22.6 | C |
| Southbound | L | 0.14 | 38.1 | D | L | 0.15 | 38.4 | D | L | 0.14 | 38.1 | D | L | 0.15 | 38.6 | D | L | 0.20 | 39.4 | D | L | 0.21 | 39.5 | D |
| | TR | 0.30 | 10.3 | B | TR | 0.34 | 10.6 | B | TR | 0.30 | 10.3 | B | TR | 0.34 | 10.7 | B | TR | 0.32 | 10.5 | B | TR | 0.35 | 10.7 | B |
| East Broadway and Catherine Street | | | | | | | | | | | | | | | | | | | | | | | | |
| Eastbound | TR | 0.49 | 12.0 | B | TR | 0.53 | 12.6 | B | TR | 0.53 | 12.9 | B | TR | 0.57 | 13.8 | B | TR | 0.50 | 11.9 | B | TR | 0.55 | 12.8 | B |
| Westbound | LT | 0.49 | 12.5 | B | LT | 0.53 | 13.3 | B | LT | 0.49 | 12.7 | B | LT | 0.52 | 13.4 | B | LT | 0.44 | 11.3 | B | LT | 0.47 | 11.8 | B |
| Southbound | LTR | 0.02 | 23.7 | C | LTR | 0.02 | 23.7 | C | LTR | 0.05 | 24.2 | C | LTR | 0.05 | 24.3 | C | LTR | 0.05 | 24.1 | C | LTR | 0.05 | 24.1 | C |

Table 14-20 (cont'd)
Existing and 2021 No Action Conditions Level of Service Analysis
Signalized Intersections

| Intersection | Weekday AM | | | | | | | | Weekday Midday | | | | | | | | Weekday PM | | | | | | | | |
|--|------------|-----------|-------------|-----|------------|-----------|-------------|-----|----------------|-----------|-------------|-----|------------|-----------|-------------|-----|------------|-----------|-------------|------|------------|-----------|-------------|------|---|
| | Existing | | | | No Action | | | | Existing | | | | No Action | | | | Existing | | | | No Action | | | | |
| | Lane Group | v/c Ratio | Delay (sec) | LOS | Lane Group | v/c Ratio | Delay (sec) | LOS | Lane Group | v/c Ratio | Delay (sec) | LOS | Lane Group | v/c Ratio | Delay (sec) | LOS | Lane Group | v/c Ratio | Delay (sec) | LOS | Lane Group | v/c Ratio | Delay (sec) | LOS | |
| East Broadway and Market Street | | | | | | | | | | | | | | | | | | | | | | | | | |
| Eastbound | LT | 0.52 | 16.4 | B | LT | 0.56 | 17.3 | B | LT | 0.46 | 14.9 | B | LT | 0.50 | 15.8 | B | LT | 0.52 | 16.0 | B | LT | 0.59 | 17.6 | B | |
| Westbound | TR | 0.56 | 17.5 | B | TR | 0.61 | 18.7 | B | TR | 0.49 | 15.9 | B | TR | 0.53 | 16.7 | B | TR | 0.62 | 18.8 | B | TR | 0.65 | 20.0 | C | |
| Northbound | LTR | 0.68 | 35.1 | D | LTR | 0.72 | 37.4 | D | LTR | 0.80 | 42.0 | D | LTR | 0.84 | 45.7 | D | LTR | 0.58 | 30.2 | C | LTR | 0.61 | 31.3 | C | |
| East Broadway and Pike Street (East) | | | | | | | | | | | | | | | | | | | | | | | | | |
| Eastbound | L | 0.53 | 34.2 | C | L | 0.56 | 36.2 | D | L | 0.47 | 31.3 | C | L | 0.49 | 32.6 | C | L | 0.80 | 56.0 | E | L | 0.84 | 62.3 | E | |
| | T | 0.43 | 25.3 | C | T | 0.44 | 25.7 | C | T | 0.39 | 24.6 | C | T | 0.41 | 24.9 | C | T | 0.40 | 24.7 | C | T | 0.42 | 25.1 | C | |
| Westbound | TR | 0.63 | 31.9 | C | TR | 0.66 | 33.1 | C | TR | 0.59 | 30.4 | C | TR | 0.62 | 31.2 | C | TR | 0.61 | 30.7 | C | TR | 0.63 | 31.5 | C | |
| Northbound | L | 0.59 | 55.0 | E | L | 0.70 | 64.4 | E | L | 0.52 | 50.9 | D | L | 0.61 | 56.2 | E | L | 0.78 | 71.1 | E | L | 0.88 | 86.3 | F | |
| | TR | 0.65 | 25.4 | C | TR | 0.69 | 26.5 | C | TR | 0.51 | 22.5 | C | TR | 0.55 | 23.1 | C | TR | 0.53 | 22.6 | C | TR | 0.57 | 23.2 | C | |
| East Broadway and Pike Street (West) | | | | | | | | | | | | | | | | | | | | | | | | | |
| Eastbound | TR | 0.92 | 57.2 | E | TR | 0.99 | 72.4 | E | TR | 0.95 | 63.1 | E | TR | 1.02 | 80.0 | E | TR | 0.99 | 70.1 | E | TR | 1.07 | 93.4 | F | |
| Westbound | L | 0.32 | 27.7 | C | L | 0.35 | 29.1 | C | L | 0.27 | 26.3 | C | L | 0.31 | 27.8 | C | L | 0.42 | 32.3 | C | L | 0.48 | 36.3 | D | |
| | T | 0.38 | 24.5 | C | T | 0.40 | 24.8 | C | T | 0.35 | 23.8 | C | T | 0.36 | 24.1 | C | T | 0.32 | 23.3 | C | T | 0.33 | 23.5 | C | |
| Southbound | L | 0.33 | 46.4 | D | L | 0.35 | 47.1 | D | L | 0.33 | 46.0 | D | L | 0.35 | 47.1 | D | L | 0.31 | 45.1 | D | L | 0.33 | 45.7 | D | |
| | T | 0.35 | 21.1 | C | T | 0.39 | 21.6 | C | T | 0.35 | 21.0 | C | T | 0.39 | 21.6 | C | T | 0.40 | 21.7 | C | T | 0.43 | 22.1 | C | |
| Division Street and Market Street | | | | | | | | | | | | | | | | | | | | | | | | | |
| Westbound | T | 0.26 | 18.0 | B | T | 0.27 | 18.2 | B | T | 0.26 | 18.0 | B | T | 0.27 | 18.1 | B | T | 0.26 | 18.0 | B | T | 0.27 | 18.1 | B | |
| Northbound | L | 0.62 | 30.0 | C | L | 0.67 | 32.2 | C | L | 0.86 | 47.2 | D | L | 0.93 | 56.9 | E | L | 0.57 | 27.7 | C | L | 0.63 | 29.5 | C | |
| Division Street and Allen Street/Pike Street | | | | | | | | | | | | | | | | | | | | | | | | | |
| Westbound | LTR | 0.31 | 27.7 | C | LTR | 0.32 | 28.0 | C | LTR | 0.39 | 29.5 | C | LTR | 0.41 | 30.0 | C | LTR | 0.35 | 28.2 | C | LTR | 0.36 | 28.5 | C | |
| Northbound | L | 0.46 | 47.4 | D | L | 0.47 | 48.0 | D | L | 0.64 | 58.1 | E | L | 0.66 | 59.8 | E | L | 0.51 | 49.2 | D | L | 0.53 | 50.2 | D | |
| | T | 0.35 | 10.7 | B | T | 0.37 | 10.9 | B | T | 0.29 | 10.1 | B | T | 0.31 | 10.3 | B | T | 0.33 | 10.4 | B | T | 0.35 | 10.6 | B | |
| Southbound | T | 0.31 | 18.5 | B | T | 0.34 | 18.9 | B | T | 0.28 | 18.2 | B | T | 0.31 | 18.5 | B | T | 0.30 | 18.4 | B | T | 0.32 | 18.6 | B | |
| | R | 0.48 | 24.3 | C | R | 0.50 | 25.1 | C | R | 0.42 | 23.0 | C | R | 0.44 | 23.7 | C | R | 0.20 | 18.2 | B | R | 0.21 | 18.4 | B | |
| Allen Street and Canal Street | | | | | | | | | | | | | | | | | | | | | | | | | |
| Eastbound | LTR | 1.05 | 87.4 | F | LTR | 1.15 | 120.3 | F | LTR | 0.74 | 35.4 | D | LTR | 0.83 | 43.0 | D | LTR | 1.04 | 83.0 | F | LTR | 1.16 | 121.8 | F | |
| Westbound | LTR | 0.27 | 21.1 | C | LTR | 0.28 | 21.3 | C | LTR | 0.32 | 22.2 | C | LTR | 0.34 | 22.6 | C | LTR | 0.30 | 21.5 | C | LTR | 0.31 | 21.7 | C | |
| Northbound | TR | 0.61 | 27.7 | C | TR | 0.65 | 28.7 | C | TR | 0.52 | 25.8 | C | TR | 0.56 | 26.5 | C | TR | 0.64 | 28.3 | C | TR | 0.68 | 29.3 | C | |
| Southbound | LTR | 0.37 | 14.0 | B | LTR | 0.41 | 14.5 | B | LTR | 0.33 | 13.5 | B | LTR | 0.36 | 13.9 | B | LTR | 0.29 | 13.1 | B | LTR | 0.32 | 13.4 | B | |
| Allen Street and Grand Street (East) | | | | | | | | | | | | | | | | | | | | | | | | | |
| Eastbound | L | 0.47 | 31.6 | C | L | 0.54 | 36.0 | D | L | 0.30 | 28.3 | C | L | 0.36 | 30.9 | C | L | 0.36 | 28.6 | C | L | 0.44 | 32.0 | C | |
| | T | 0.29 | 23.0 | C | T | 0.34 | 23.8 | C | T | 0.34 | 26.0 | C | T | 0.43 | 27.7 | C | C | T | 0.49 | 27.9 | C | T | 0.58 | 30.3 | C |
| Westbound | TR | 0.52 | 28.2 | C | TR | 0.64 | 31.9 | C | TR | 0.56 | 32.0 | C | TR | 0.68 | 36.9 | D | TR | 0.46 | 28.0 | C | TR | 0.58 | 31.5 | C | |
| Northbound | L | 0.39 | 44.8 | D | L | 0.41 | 45.5 | D | L | 0.53 | 51.4 | D | L | 0.55 | 52.2 | D | L | 0.49 | 48.6 | D | L | 0.51 | 49.2 | D | |
| | TR | 0.65 | 26.2 | C | TR | 0.70 | 27.4 | C | TR | 0.51 | 22.7 | C | TR | 0.54 | 23.3 | C | TR | 0.56 | 24.2 | C | TR | 0.60 | 25.0 | C | |
| Allen Street and Grand Street (West) | | | | | | | | | | | | | | | | | | | | | | | | | |
| Eastbound | TR | 0.71 | 35.9 | D | TR | 0.79 | 41.4 | D | TR | 0.88 | 56.4 | E | TR | 1.01 | 81.7 | F | TR | 0.88 | 50.6 | D | TR | 1.01 | 76.9 | E | |
| Westbound | L | 0.14 | 22.1 | C | L | 0.21 | 23.8 | C | L | 0.27 | 28.3 | C | L | 0.47 | 37.6 | D | L | 0.20 | 25.6 | C | L | 0.28 | 29.2 | C | |
| | T | 0.31 | 23.2 | C | T | 0.36 | 24.0 | C | T | 0.25 | 24.5 | C | T | 0.29 | 25.2 | C | T | 0.24 | 23.5 | C | T | 0.28 | 24.1 | C | |
| Southbound | L | 0.31 | 42.6 | D | L | 0.33 | 43.1 | D | L | 0.42 | 43.3 | D | L | 0.45 | 44.3 | D | L | 0.39 | 41.9 | D | L | 0.40 | 42.3 | D | |
| | TR | 0.53 | 24.1 | C | TR | 0.57 | 24.8 | C | TR | 0.47 | 21.0 | C | TR | 0.51 | 21.6 | C | TR | 0.44 | 21.1 | C | TR | 0.47 | 21.6 | C | |
| Allen Street and Delancey Street | | | | | | | | | | | | | | | | | | | | | | | | | |
| Eastbound | T | 0.94 | 48.0 | D | T | 1.01 | 61.4 | E | T | 0.84 | 30.4 | C | T | 0.90 | 34.1 | C | T | 0.85 | 31.1 | C | T | 0.91 | 34.8 | C | |
| | R | 0.16 | 25.6 | C | R | 0.17 | 25.8 | C | R | 0.20 | 19.3 | B | R | 0.21 | 19.5 | B | R | 0.12 | 18.2 | B | R | 0.13 | 18.3 | B | |
| Westbound | L | 0.86 | 51.6 | D | L | 0.92 | 60.0 | E | L | 0.97 | 87.4 | F | L | 1.03 | 103.4 | F | L | 1.00 | 93.0 | F | L | 1.04 | 105.7 | F | |
| | TR | 0.63 | 12.4 | B | TR | 0.67 | 12.9 | B | TR | 0.54 | 11.0 | B | TR | 0.57 | 11.4 | B | TR | 0.54 | 11.0 | B | TR | 0.57 | 11.4 | B | |
| Northbound | T | 0.76 | 37.6 | D | T | 0.81 | 40.2 | D | T | 0.53 | 30.9 | C | T | 0.58 | 32.0 | C | T | 0.52 | 30.6 | C | T | 0.58 | 31.6 | C | |
| | R | 0.35 | 10.8 | B | R | 0.37 | 11.2 | B | R | 0.50 | 19.4 | B | R | 0.53 | 20.4 | C | R | 0.60 | 22.5 | C | R | 0.64 | 24.0 | C | |
| Southbound | TR | 0.40 | 28.7 | C | TR | 0.43 | 29.1 | C | TR | 0.38 | 28.3 | C | TR | 0.40 | 28.7 | C | TR | 0.49 | 30.1 | C | TR | 0.53 | 30.8 | C | |
| Bowery and Canal Street | | | | | | | | | | | | | | | | | | | | | | | | | |
| Eastbound | T | 0.79 | 29.4 | C | T | 0.82 | 31.0 | C | T | 0.79 | 29.3 | C | T | 0.82 | 30.9 | C | T | 1.03 | 61.0 | E | T | 1.07 | 74.1 | E | |
| | R | 0.32 | 20.3 | C | R | 0.35 | 20.7 | C | R | 0.24 | 19.1 | B | R | 0.26 | 19.4 | B | R | 0.16 | 18.0 | B | R | 0.18 | 18.2 | B | |
| Westbound | T | 0.80 | 29.5 | C | T | 0.83 | 31.1 | C | T | 0.63 | 24.4 | C | T | 0.66 | 25.0 | C | T | 0.43 | 20.6 | C | T | 0.44 | 20.8 | C | |
| Northbound | T | 0.56 | 33.2 | C | T | 0.59 | 33.8 | C | T | 0.51 | 32.1 | C | T | 0.54 | 32.7 | C | T | 0.43 | 30.6 | C | T | 0.46 | 31.0 | C | |
| Southbound | DefL | 0.87 | 47.0 | D | DefL | 0.90 | 50.7 | D | DefL | 0.85 | 44.5 | D | DefL | 0.87 | 47.2 | D | DefL | 1.05 | 78.6 | E | DefL | 1.10 | 96.2 | F | |
| | TR | 0.64 | 25.9 | C | TR | 0.67 | 27.1 | C | TR | 0.61 | 25.0 | C | TR | 0.64 | 26.0 | C | TR | 0.36 | 19.3 | B | TR | 0.38 | 19.6 | B | |
| Bowery and Bayard Street | | | | | | | | | | | | | | | | | | | | | | | | | |
| Eastbound | LR | 0.29 | 22.8 | C | LR | 0.30 | 23.1 | C | LR | 0.57 | 31.3 | C | LR | 0.59 | 32.4 | C | LR | 0.65 | 35.1 | D | LR | 0.68 | 36.8 | D | |
| Northbound | T | 0.41 | 17.6 | B | T | 0.43 | 17.9 | B | T | 0.47 | 18.5 | B | T | 0.49 | 18.8 | B | T | 0.56 | 19.7 | B | T | 0.58 | 20.1 | C | |
| Southbound | T | 0.22 | 15.7 | B | T | 0.24 | 15.9 | B | T | 0.19 | 15.4 | B | T | 0.20 | 15.5 | B | T | 0.13 | 14.9 | B | T | 0.14 | 15.0 | C | |
| Bowery and Division Street/Doyers Street | | | | | | | | | | | | | | | | | | | | | | | | | |
| Eastbound | R | 0.04 | 26.4 | C | R | 0.04 | 26.4 | C | R | 0.07 | 26.8 | C | R | 0.07 | 26.8 | C | R | 0.07 | 26.8 | C | R | 0.07 | 26.8 | C | |
| Westbound | L | 0.66 | 46.2 | D | L | 0.74 | 51.5 | D | L | 0.72 | 49.5 | D | L | 0.76 | 53.0 | D | L | 0.57 | 41.1 | D | L | 0.61 | 42.9 | D | |
| | R | 0.57 | 18.8 | B | R | 0.59 | 19.5 | B | R | 0.64 | 20.6 | C | R | 0.67 | 21.6 | C | R | 0.56 | 18.5 | B | R | 0.59 | 19.2 | B | |
| Northbound | TR | 0.34 | 20.2 | C | TR | 0.36 | 20.5 | C | TR | 0.38 | 20.7 | C | TR | 0.40 | 21.0 | C | TR | 0.58 | 23.7 | C | TR | 0.60 | 24.3 | C | |
| Southbound | T | 0.34 | 20.3 | C | T | 0.37 | 20.6 | C | T | 0.35 | 20.3 | C | T | 0.37 | 20.6 | C | T | 0.22 | 18.8 | B | T | 0.24 | 19.0 | B | |

Two Bridges LSRD

Table 14-20 (cont'd)
Existing and 2021 No Action Conditions Level of Service Analysis
Signalized Intersections

| Intersection | Weekday AM | | | | | | | | Weekday Midday | | | | | | | | Weekday PM | | | | | | | |
|--|------------|------|-------------|-----|------------|------|-------------|-----|----------------|------|-------------|-----|------------|------|-------------|-----|------------|------|-------------|-----|------------|------|-------------|-----|
| | Existing | | | | No Action | | | | Existing | | | | No Action | | | | Existing | | | | No Action | | | |
| | Lane Group | v/c | Delay (sec) | LOS | Lane Group | v/c | Delay (sec) | LOS | Lane Group | v/c | Delay (sec) | LOS | Lane Group | v/c | Delay (sec) | LOS | Lane Group | v/c | Delay (sec) | LOS | Lane Group | v/c | Delay (sec) | LOS |
| Chatham Square and East Broadway | | | | | | | | | | | | | | | | | | | | | | | | |
| Westbound | L | 0.30 | 17.3 | B | L | 0.32 | 17.7 | B | L | 0.23 | 16.3 | B | L | 0.25 | 16.6 | B | L | 0.29 | 17.1 | B | L | 0.31 | 17.3 | B |
| | R | 0.15 | 15.5 | B | R | 0.18 | 15.9 | B | R | 0.13 | 15.3 | B | R | 0.15 | 15.6 | B | R | 0.21 | 16.2 | B | R | 0.23 | 16.4 | B |
| Northbound | T | 0.22 | 15.8 | B | T | 0.23 | 15.9 | B | T | 0.29 | 16.5 | B | T | 0.30 | 16.7 | B | T | 0.44 | 18.3 | B | T | 0.45 | 18.5 | B |
| | R | 0.48 | 22.0 | C | R | 0.52 | 23.2 | C | R | 0.67 | 30.7 | C | R | 0.73 | 35.1 | D | R | 0.79 | 37.9 | D | R | 0.88 | 49.8 | D |
| Southbound | L | 0.62 | 28.5 | C | L | 0.69 | 32.6 | C | L | 0.74 | 37.7 | D | L | 0.82 | 46.9 | D | L | 0.61 | 30.9 | C | L | 0.71 | 38.5 | D |
| | T | 0.28 | 16.3 | B | T | 0.29 | 16.5 | B | T | 0.25 | 16.0 | B | T | 0.26 | 16.1 | B | T | 0.18 | 15.4 | B | T | 0.19 | 15.5 | B |
| Chatham Square and Worth Street/Oliver Street | | | | | | | | | | | | | | | | | | | | | | | | |
| Eastbound (Worth Street) | L | 1.05 | 140.6 | F | L | 1.24 | 209.1 | F | L | 0.98 | 101.1 | F | L | 1.08 | 131.5 | F | L | 1.05 | 106.5 | F | L | 1.16 | 145.2 | F |
| | LTR | 0.96 | 86.2 | F | LTR | 1.12 | 136.6 | F | LTR | 0.89 | 66.0 | E | LTR | 1.00 | 91.1 | F | LTR | 1.04 | 94.5 | F | LTR | 1.16 | 134.1 | F |
| Eastbound (Mott Street) | LTR | 0.56 | 42.2 | D | LTR | 0.58 | 43.1 | D | LTR | 0.61 | 44.3 | D | LTR | 0.64 | 45.7 | D | LTR | 0.79 | 56.7 | E | LTR | 0.83 | 61.0 | E |
| Westbound | LT | 0.82 | 41.4 | D | LT | 0.85 | 44.5 | D | LT | 0.53 | 29.3 | C | LT | 0.56 | 29.8 | C | LT | 0.49 | 28.1 | C | LT | 0.51 | 28.5 | C |
| | R | 0.69 | 39.0 | D | R | 0.74 | 41.8 | D | R | 0.80 | 48.4 | D | R | 0.84 | 53.4 | D | R | 0.99 | 78.6 | E | R | 1.04 | 92.9 | F |
| Northbound | LTR | 0.08 | 21.4 | C | LTR | 0.08 | 21.5 | C | LTR | 0.11 | 21.7 | C | LTR | 0.11 | 21.8 | C | LTR | 0.08 | 21.4 | C | LTR | 0.08 | 21.5 | C |
| Southbound | L | 0.93 | 73.7 | E | L | 0.99 | 87.8 | F | L | 0.65 | 39.3 | D | L | 0.69 | 42.3 | D | L | 0.67 | 40.7 | D | L | 0.72 | 44.3 | D |
| | TR | 0.88 | 50.6 | D | TR | 0.96 | 65.5 | E | TR | 1.01 | 80.2 | F | TR | 1.09 | 106.9 | F | TR | 0.86 | 50.0 | D | TR | 0.92 | 60.6 | E |
| Worth Street and Centre Street | | | | | | | | | | | | | | | | | | | | | | | | |
| Eastbound | L | 0.30 | 17.5 | B | L | 0.35 | 22.7 | C | L | 0.23 | 11.7 | B | L | 0.25 | 13.5 | B | L | 0.20 | 11.0 | B | L | 0.22 | 12.4 | B |
| | T | 0.50 | 18.0 | B | T | 0.52 | 18.5 | B | T | 0.40 | 12.9 | B | T | 0.43 | 13.2 | B | T | 0.65 | 17.9 | B | T | 0.69 | 19.3 | B |
| Westbound | T | 0.44 | 26.6 | C | T | 0.73 | 36.6 | D | T | 0.28 | 19.6 | B | T | 0.42 | 22.0 | C | T | 0.24 | 19.0 | B | T | 0.39 | 21.4 | C |
| | R | 0.79 | 48.6 | D | R | 0.43 | 28.6 | C | R | 0.47 | 25.3 | C | R | 0.27 | 20.4 | C | R | 0.39 | 22.2 | C | R | 0.21 | 19.0 | B |
| Northbound | L | 0.11 | 17.7 | B | L | 0.12 | 17.8 | B | L | 0.22 | 23.7 | C | L | 0.24 | 24.0 | C | L | 0.13 | 21.6 | C | L | 0.13 | 21.7 | C |
| | TR | 0.59 | 23.8 | C | TR | 0.62 | 24.4 | C | TR | 0.60 | 28.3 | C | TR | 0.63 | 29.0 | C | TR | 0.62 | 28.1 | C | TR | 0.64 | 28.8 | C |
| Worth Street and Lafayette Street | | | | | | | | | | | | | | | | | | | | | | | | |
| Eastbound | - | - | - | - | T | 0.42 | 23.7 | C | - | - | - | - | T | 0.38 | 23.0 | C | - | - | - | - | T | 0.56 | 26.6 | C |
| | TR | 0.53 | 25.8 | C | - | - | - | - | TR | 0.52 | 25.7 | C | - | - | - | - | TR | 0.59 | 27.0 | C | - | - | - | - |
| | - | - | - | - | R | 0.25 | 21.5 | C | - | - | - | - | R | 0.29 | 22.4 | C | - | - | - | - | R | 0.19 | 20.3 | C |
| Westbound | L | 0.65 | 34.0 | C | L | 0.41 | 20.7 | C | L | 0.71 | 37.9 | D | L | 0.41 | 20.2 | C | L | 0.52 | 30.1 | C | L | 0.30 | 20.6 | C |
| | - | - | - | - | T | 0.24 | 14.2 | B | - | - | - | - | T | 0.20 | 13.7 | B | - | - | - | - | T | 0.20 | 13.7 | B |
| Southbound | LT | 0.72 | 27.3 | C | LTR | 0.83 | 32.2 | C | LT | 0.64 | 25.2 | C | LTR | 0.75 | 28.6 | C | LT | 0.70 | 26.1 | C | LTR | 0.81 | 30.5 | C |
| Worth Street and Broadway | | | | | | | | | | | | | | | | | | | | | | | | |
| Eastbound | TR | 0.56 | 25.5 | C | TR | 0.58 | 26.2 | C | TR | 0.48 | 23.6 | C | TR | 0.51 | 24.2 | C | TR | 0.53 | 24.6 | C | TR | 0.56 | 25.4 | C |
| Westbound | - | - | - | - | L | 0.32 | 23.2 | C | - | - | - | - | L | 0.36 | 24.1 | C | - | - | - | - | L | 0.29 | 22.3 | C |
| | - | - | - | - | T | 0.30 | 20.3 | C | - | - | - | - | T | 0.23 | 19.4 | B | - | - | - | - | T | 0.27 | 20.0 | B |
| Southbound | - | - | - | - | L | 0.20 | 13.8 | B | - | - | - | - | L | 0.19 | 13.8 | B | - | - | - | - | L | 0.27 | 14.9 | B |
| | LT | 0.47 | 15.9 | B | - | - | - | - | LT | 0.46 | 15.8 | B | - | - | - | - | LT | 0.66 | 19.4 | B | - | - | - | - |
| | - | - | - | - | TR | 0.50 | 16.4 | B | - | - | - | - | TR | 0.50 | 16.3 | B | - | - | - | - | TR | 0.71 | 20.6 | C |

Notes: L = Left Turn, T = Through, R = Right Turn, DefL = Defacto Left Turn, LOS = Level of Service

Table 14-21
Existing and 2021 No Build Conditions Level of Service Analysis
Unsignalized Intersections

| Intersection | Weekday AM | | | | | | | | Weekday Midday | | | | | | | | Weekday PM | | | | | | | |
|---|------------|------|-------------|-----|------------|------|-------------|-----|----------------|------|-------------|-----|------------|------|-------------|-----|------------|------|-------------|-----|------------|------|-------------|-----|
| | Existing | | | | No Action | | | | Existing | | | | No Action | | | | Existing | | | | No Action | | | |
| | Lane Group | v/c | Delay (sec) | LOS | Lane Group | v/c | Delay (sec) | LOS | Lane Group | v/c | Delay (sec) | LOS | Lane Group | v/c | Delay (sec) | LOS | Lane Group | v/c | Delay (sec) | LOS | Lane Group | v/c | Delay (sec) | LOS |
| Cherry Street and Clinton Street | | | | | | | | | | | | | | | | | | | | | | | | |
| Westbound | TR | 0.14 | 7.9 | A | TR | 0.17 | 8.2 | A | TR | 0.13 | 7.9 | A | TR | 0.17 | 8.3 | A | TR | 0.20 | 8.4 | A | TR | 0.25 | 8.9 | A |
| Northbound | LT | 0.21 | 8.4 | A | LT | 0.25 | 8.8 | A | LT | 0.23 | 8.6 | A | LT | 0.28 | 9.1 | A | LT | 0.30 | 9.3 | A | LT | 0.36 | 10.0 | A |
| Pike Street and Monroe Street | | | | | | | | | | | | | | | | | | | | | | | | |
| Eastbound | R | 0.70 | 11.2 | B | R | 0.08 | 11.6 | B | R | 0.08 | 11.4 | B | R | 0.10 | 11.8 | B | R | 0.08 | 11.2 | B | R | 0.09 | 11.5 | B |

Notes: L = Left Turn, T = Through, R = Right Turn, DefL = Defacto Left Turn, LOS = Level of Service

Based on the analysis results presented in **Tables 14-20 and 14-21**, the majority of the approaches/lane-groups in the No Action condition will operate at the same LOS as in the existing conditions or within acceptable mid-LOS D or better (delays of 45 seconds or less per vehicle for signalized intersections) for all peak hours. The following approaches/lane-groups in the No Action condition are expected to operate at deteriorated LOS when compared to the existing conditions:

- Eastbound approach at the South Street and Clinton Street intersection will deteriorate to LOS F with a v/c ratio of 1.07 and a delay of 82.3 spv during the weekday PM peak hour;

- Westbound approach at the South Street and Montgomery Street (north) intersection will deteriorate to LOS F with a v/c ratio of 1.13 and a delay of 91.9 spv during the weekday PM peak hour;
- Northbound approach at the South Street and Montgomery Street (north) intersection will deteriorate to LOS D with a v/c ratio of 0.83 and a delay of 47.4 spv during the weekday PM peak hour;
- Southbound approach at the South Street and Montgomery Street (south) intersection will deteriorate to LOS D with a v/c ratio of 0.74 and a delay of 37.2 spv during the weekday AM peak hour;
- Eastbound left-turn at the Madison Street and Pike Street (east) intersection will deteriorate to LOS E with a v/c ratio of 0.78 and a delay of 56.3 spv during the weekday midday peak hour, and to LOS F with a v/c ratio of 0.93 and a delay of 89.3 spv during the weekday PM peak hour;
- Northbound approach at the Madison Street and Montgomery Street intersection will deteriorate to LOS F with a v/c ratio of 1.14 and a delay of 117.4 spv during the weekday PM peak hour;
- Eastbound left-turn at the East Broadway and Pike Street (east) intersection will deteriorate to LOS D with a v/c ratio of 0.56 and a delay of 36.2 spv during the weekday AM peak hour;
- Northbound left-turn at the East Broadway and Pike Street (east) intersection will deteriorate to LOS E with a v/c ratio of 0.61 and delay of 56.2 spv during the weekday midday peak hour, and to LOS F with a v/c ratio of 0.88 and a delay of 86.3 spv during the weekday PM peak hour;
- Eastbound approach at the East Broadway and Pike Street (west) intersection will deteriorate to LOS F with a v/c ratio of 1.02 and a delay of 80.0 spv during the weekday midday peak hour, and to LOS F with a v/c ratio of 1.07 and a delay of 93.4 spv during the weekday PM peak hour;
- Westbound left-turn at the East Broadway and Pike Street (west) intersection will deteriorate to LOS D with a v/c ratio of 0.48 and a delay of 36.3 spv during the weekday PM peak hour;
- Northbound left-turn at the Division Street and Market Street intersection will deteriorate to LOS E with a v/c ratio of 0.93 and a delay of 56.9 spv during the weekday midday peak hour;
- Eastbound left-turn at the Allen Street and Grand Street (east) intersection will deteriorate to LOS D with a v/c ratio of 0.54 and a delay of 36.0 spv during the weekday AM peak hour;
- Westbound approach at the Allen Street and Grand Street (east) intersection will deteriorate to LOS D with a v/c ratio of 0.68 and a delay of 36.9 spv during the weekday midday peak hour;
- Eastbound approach at the Allen Street and Grand Street (west) intersection will deteriorate to LOS F with a v/c ratio of 1.01 and a delay of 81.7 spv during the weekday midday peak hour, and to LOS E with a v/c ratio of 1.01 and a delay of 76.9 spv during the weekday PM peak hour;
- Westbound left-turn at the Allen Street and Grand Street (west) intersection will deteriorate to LOS D with a v/c ratio of 0.47 and a delay of 37.6 spv during the weekday midday peak hour;

Two Bridges LSRD

- Eastbound through at the Allen Street and Delancey Street intersection will deteriorate to LOS E with a v/c ratio of 1.01 and a delay of 61.4 spv during the weekday AM peak hour;
- Westbound left-turn at the Allen Street and Delancey Street intersection will deteriorate to LOS E with a v/c ratio of 0.92 and a delay of 60.0 spv during the weekday AM peak hour;
- Defacto left-turn at The Bowery and Canal Street intersection will deteriorate to LOS F with a v/c ratio of 1.10 and a delay of 96.2 spv during the weekday PM peak hour;
- Northbound right-turn at the Chatham Square and East Broadway intersection will deteriorate to LOS D with a v/c ratio of 0.73 and a delay of 35.1 spv during the weekday midday peak hour;
- Southbound left-turn at the Chatham Square and East Broadway intersection will deteriorate to LOS D with a v/c ratio of 0.71 and a delay of 38.5 spv during the weekday PM peak hour;
- Eastbound (Worth Street) shared lane at the Chatham Square and Worth Street/Oliver Street intersection will deteriorate to LOS F with a v/c ratio of 1.00 and a delay of 91.1 spv during the weekday midday peak hour;
- Westbound right-turn at the Chatham Square and Worth Street/Oliver Street intersection will deteriorate to LOS F with a v/c ratio of 1.04 and a delay of 92.9 spv during the weekday PM peak hour;
- Southbound left-turn at the Chatham Square and Worth Street/Oliver Street intersection will deteriorate to LOS F with a v/c ratio of 0.99 and a delay of 87.8 spv during the weekday AM peak hour;
- Southbound shared lane at the Chatham Square and Worth Street/Oliver Street intersection will deteriorate to LOS E with a v/c ratio of 0.96 and a delay of 65.5 spv during the weekday AM peak hour, and to LOS E with a v/c ratio of 0.92 and a delay of 60.6 spv during the weekday PM peak hour; and
- Westbound through at the Worth Street and Centre Street intersection will deteriorate to LOS D with a v/c ratio of 0.73 and a delay of 36.6 spv during the weekday AM peak hour.

THE FUTURE WITH THE PROPOSED PROJECTS

As noted above, in the future with the proposed projects, the project sites would be developed with a total of approximately 2,775 new dwelling units, 10,858 gsf of new local retail, and approximately 17,028 gsf of new community facility use. The proposed community facility space on Site 5 is as yet unprogrammed; however, for the purposes of a conservative analysis, it is assumed that this space could be utilized as an accessory early childhood educational facility. The proposed projects would result in approximately 435, 214, and 424 incremental vehicle trips during the weekday AM, midday, and PM peak hours, respectively. The incremental auto trips were assigned to off-street parking facilities. Taxi trips were distributed to the various project site entrances. All delivery trips were assigned to the development site via DOT-designated truck routes.

As described in Chapter 1, "Project Description," the Site 4 (4A/4B) existing curb cuts on Rutgers Slip and Cherry Street would be removed and the existing curb cut on South Street would remain; no new curb cuts would be required. Additionally, the Cherry Street sidewalk adjacent to Site 4 (4A/4B) would be modestly widened to accommodate the installation of Con Edison vaults. This widening would better align the roadway curbs on this side of Cherry Street, while not affecting the adjacent parking and moving lanes; therefore, it would not affect traffic

operations or have the potential for significant adverse impacts. Its approval would be subject to separate review by the Permit Management Office of DOT. On Site 5, two existing curb cuts north of 265 and 275 Cherry Street would be closed and replaced with a single central curb cut in this area on Cherry Street. On South Street, two existing curb cuts would be used to access the resident and visitor drop-off and the lower level parking garage in the new building. Two other existing curb cuts on South Street may be modified. The Jefferson Street walkway curb cuts would be maintained on Cherry and South Streets. No new curb cuts would be required. The Site 6A existing curb cuts on South Street would remain; no new curb cuts would be required.

In addition, as contemplated by the original Two Bridges Urban Renewal Plan, a 10-foot wide easement, abutting the northerly street line of South Street from Market Slip to a point 161 feet easterly of the east street line of Clinton Street, was added to the City Map in 1972. The easement would remain with the proposed actions permitting use by pedestrians on, over, and across those portions of the landscape/public areas that are subject to this permanent and perpetual non-exclusive surface easement.

TRAFFIC OPERATIONS

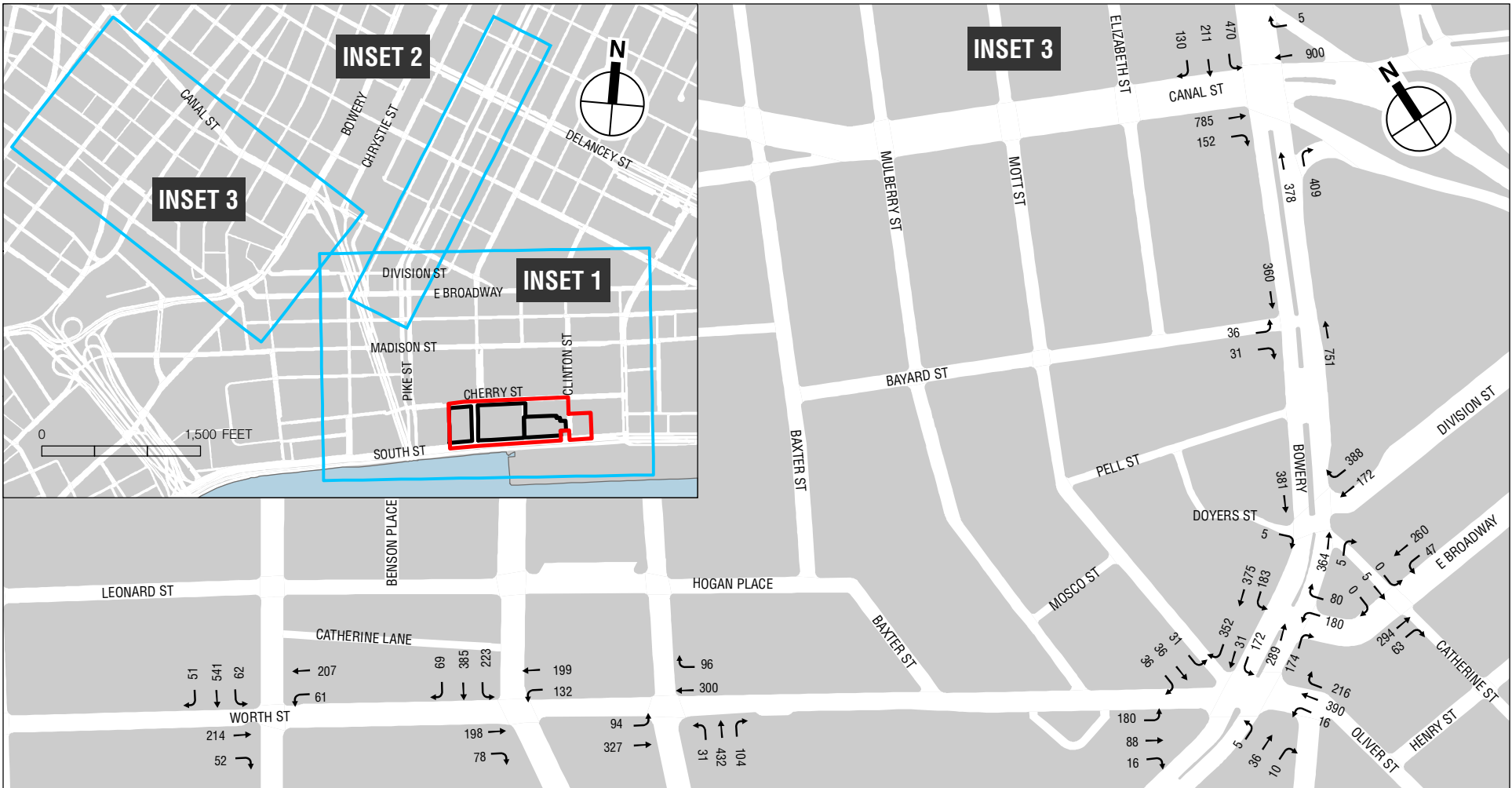
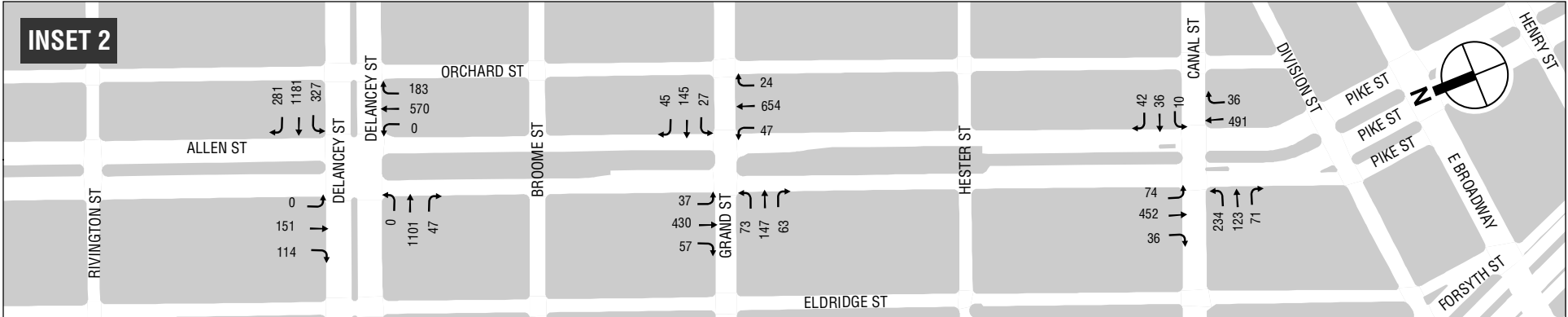
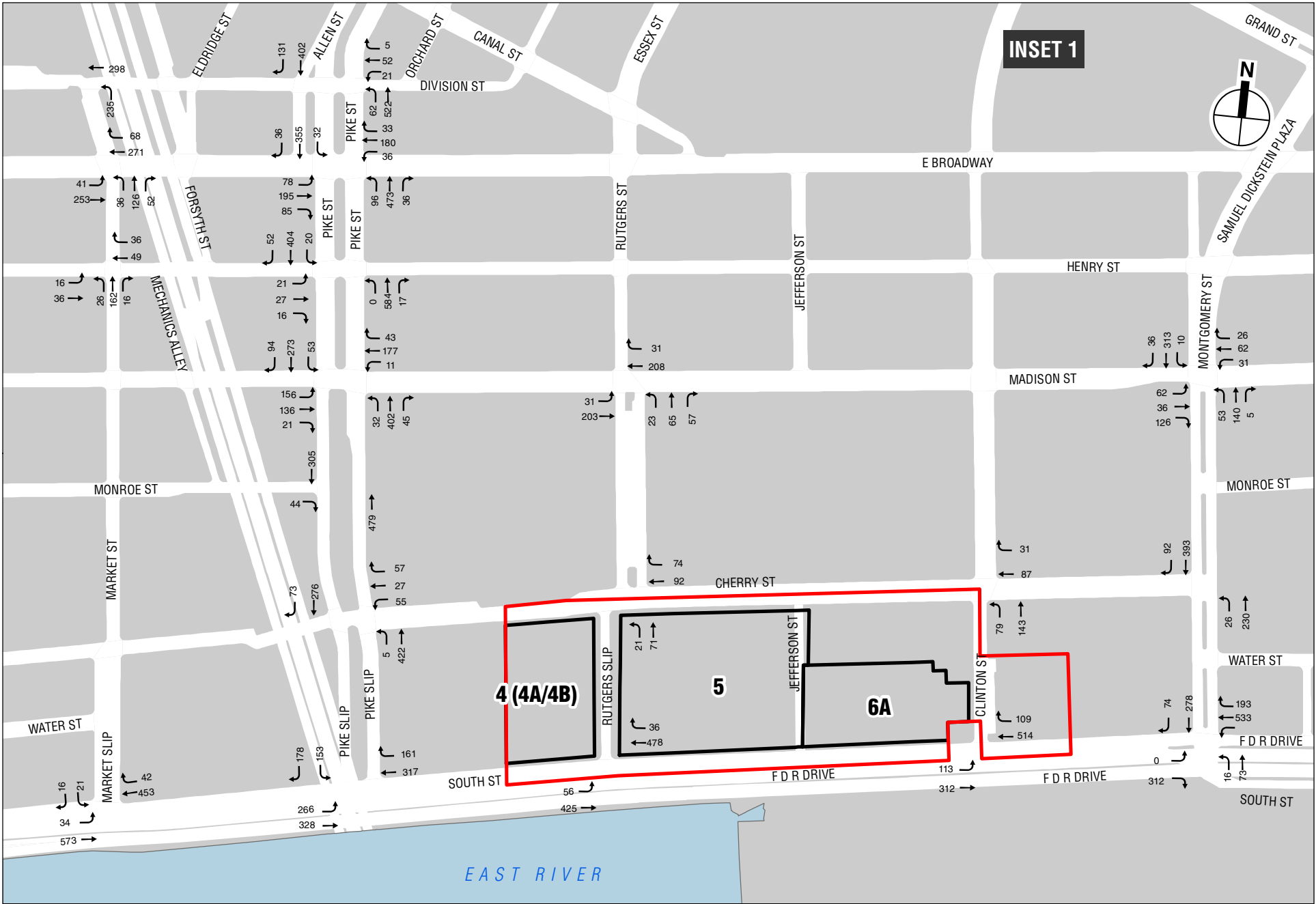
The 2021 With Action condition traffic volumes are shown in **Figures 14-17 through 14-19** for the weekday AM, midday, and PM peak hours. The 2021 With Action traffic volumes were constructed by layering on top of the No Action condition traffic volumes the incremental vehicle trips shown in **Figures 14-2 through 14-4**. A summary of the 2021 With Action condition traffic analysis results is presented in **Table 14-22**.

Table 14-22
Summary of 2021 With Action Traffic Analysis Results

| Level of Service | Analysis Peak Hours | | |
|--|---------------------|----------------|------------|
| | Weekday AM | Weekday Midday | Weekday PM |
| Signalized Intersections | | | |
| Lane Groups at LOS A/B/C | 102 | 109 | 101 |
| Lane Groups at LOS D | 26 | 21 | 20 |
| Lane Groups at LOS E | 5 | 5 | 7 |
| Lane Groups at LOS F | 8 | 6 | 13 |
| Total | 141 | 141 | 141 |
| Lane Groups with v/c \geq 0.90 | 14 | 8 | 20 |
| Unsignalized Intersections | | | |
| Lane Groups at LOS A/B/C | 3 | 3 | 3 |
| Lane Groups at LOS D | 0 | 0 | 0 |
| Lane Groups at LOS E | 0 | 0 | 0 |
| Lane Groups at LOS F | 0 | 0 | 0 |
| Total | 3 | 3 | 3 |
| Lane Groups with v/c \geq 0.90 | 0 | 0 | 0 |
| Notes: LOS = Level-of-Service; v/c = volume-to-capacity ratio | | | |

Significant Adverse Impacts

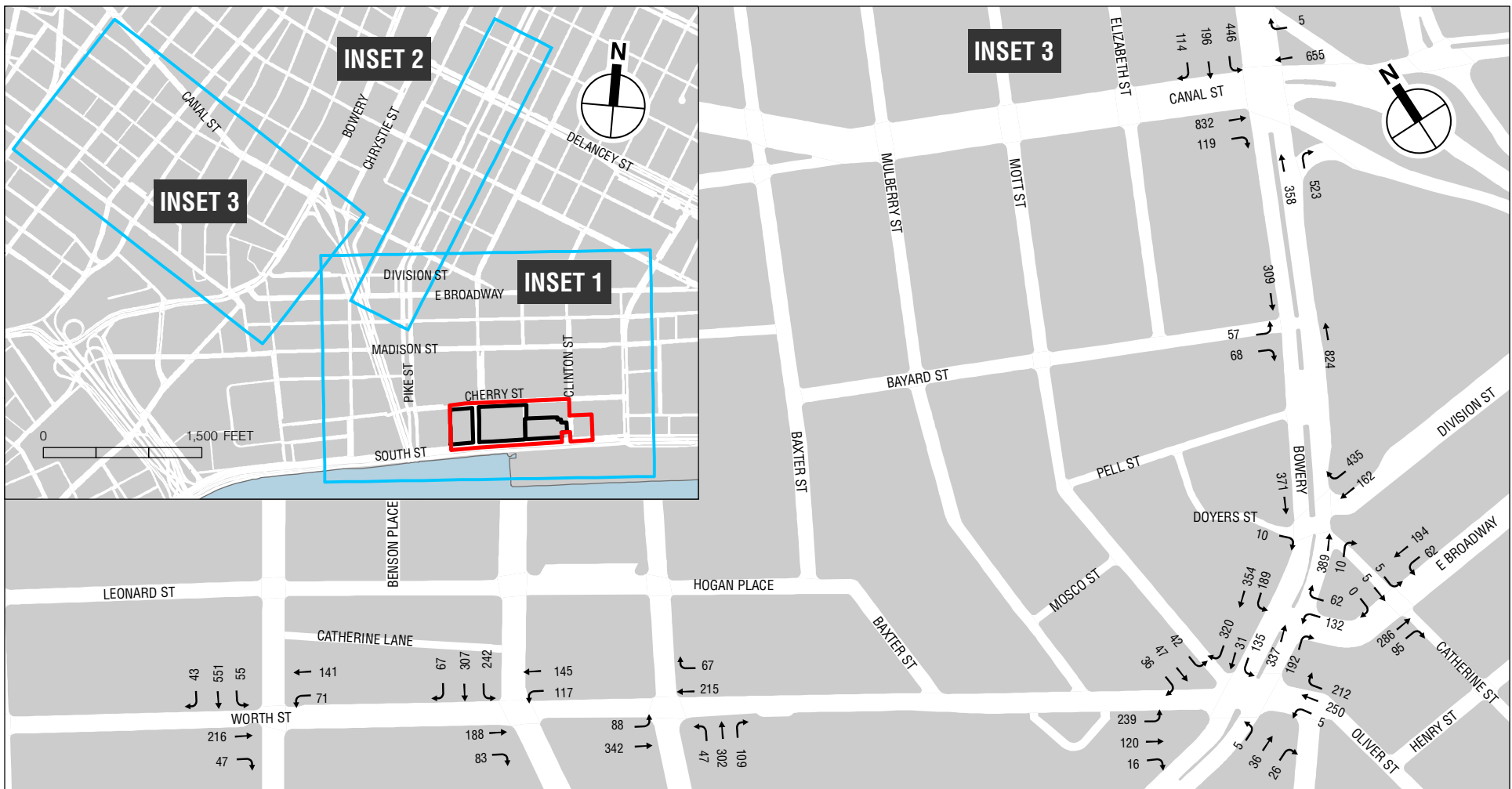
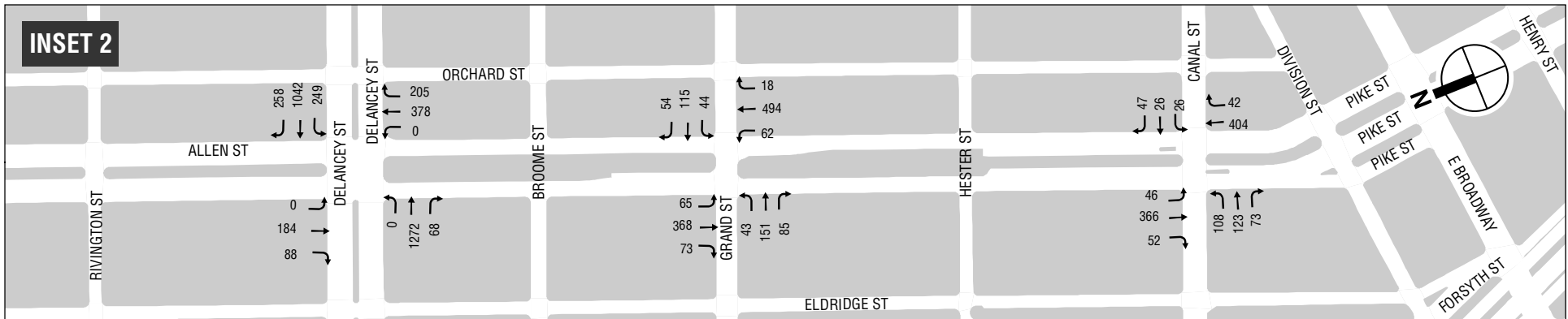
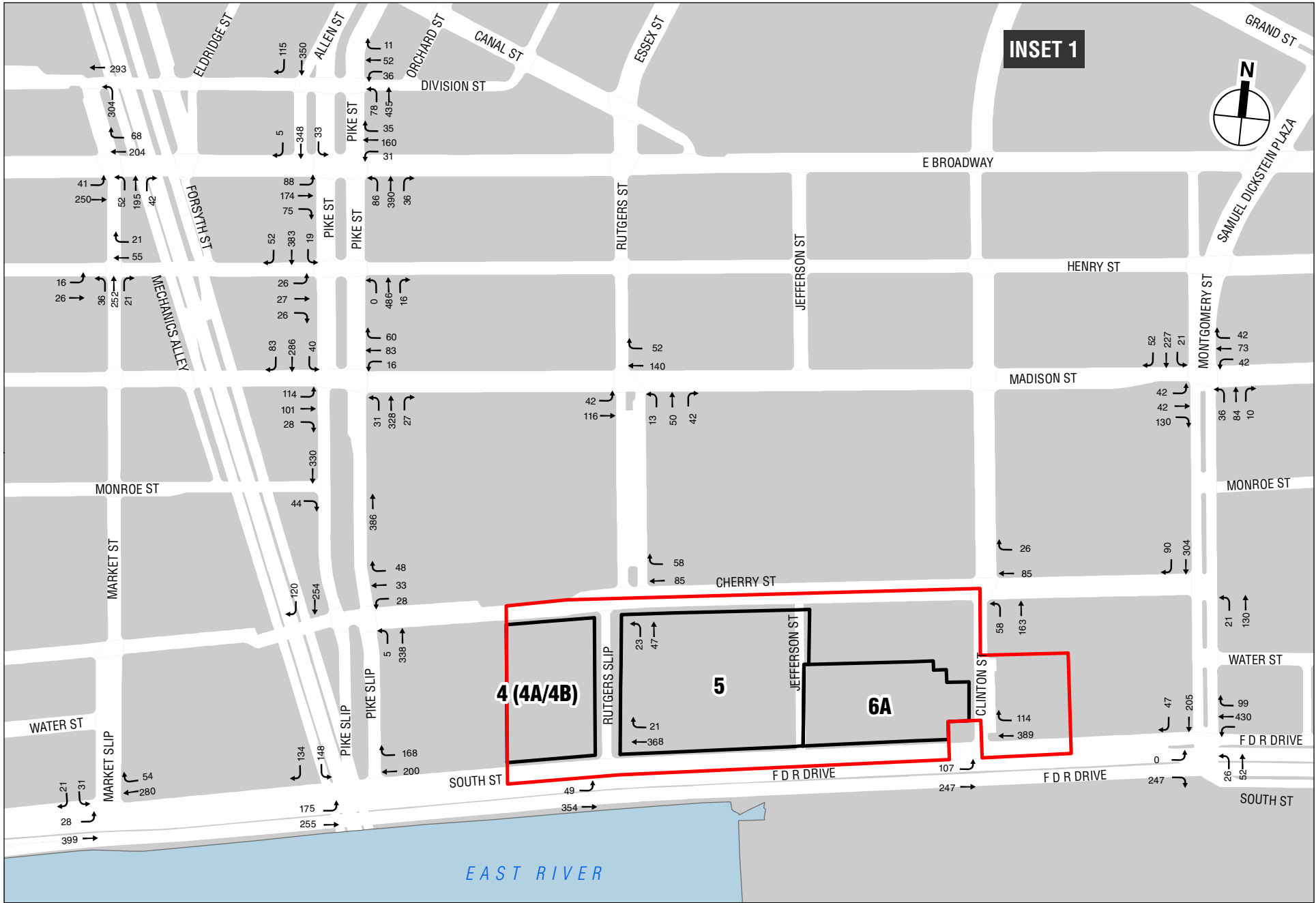
Details on LOS, v/c ratios, and average delays are presented in **Tables 14-23 and 14-24**. As discussed below, significant adverse traffic impacts were identified at 22 approaches/lane groups (of 13 different intersections). Potential measures that can be implemented to mitigate these significant adverse traffic impacts are discussed in Chapter 21, "Mitigation."



Project Sites
 Boundary of Two Bridges LSRD

0 400 FEET

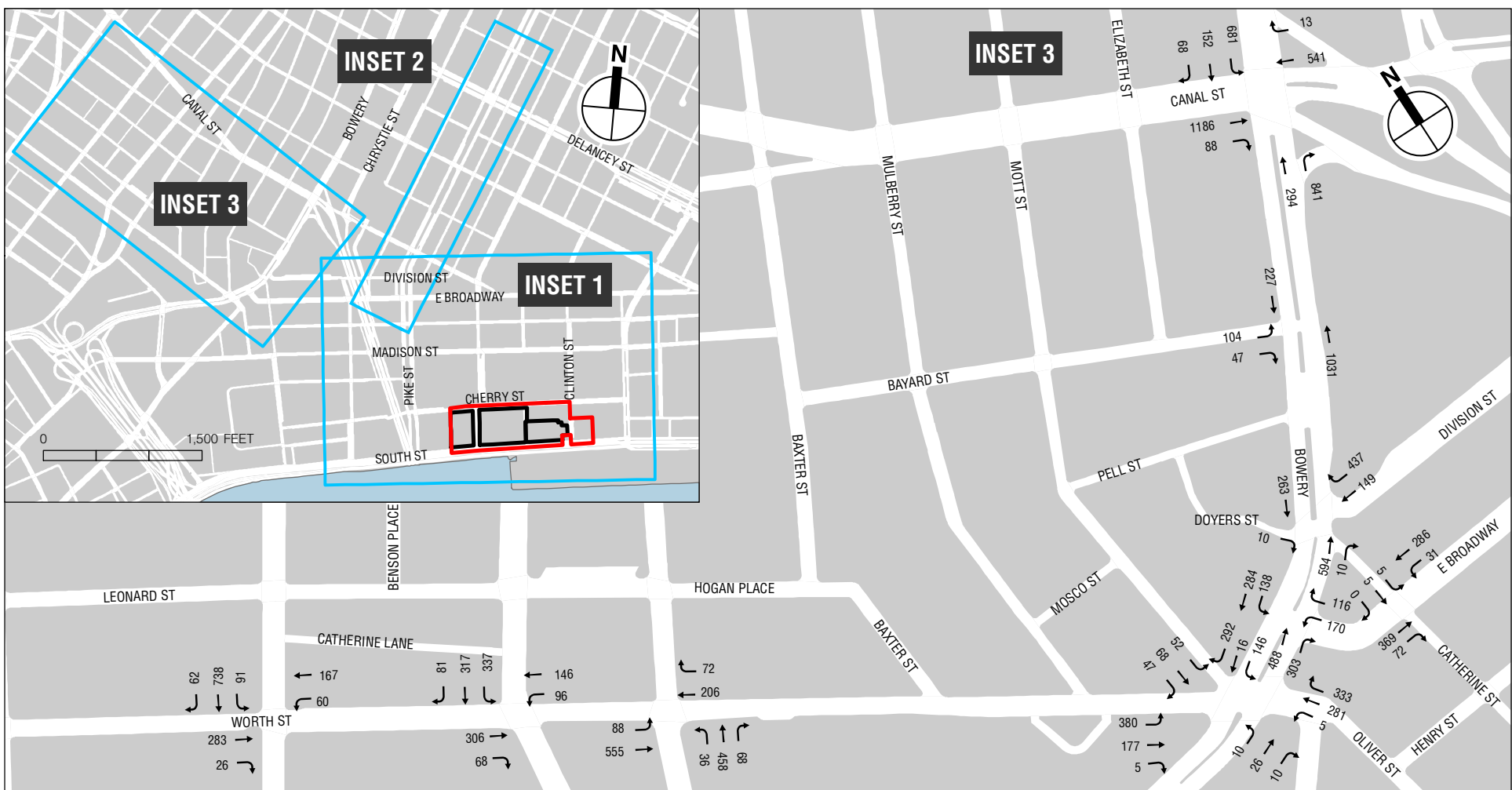
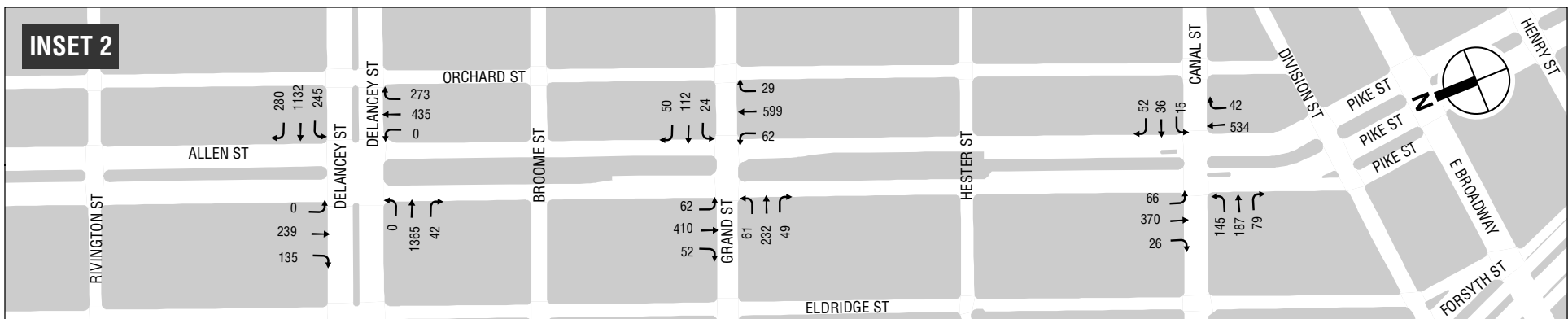
2021 With Action Traffic Volumes
Weekday AM Peak Hour
Figure 14-17



 Project Sites
 Boundary of Two Bridges LSRD

0 400 FEET

2021 With Action Traffic Volumes
Weekday Midday Peak Hour
Figure 14-18



0 400 FEET

TWO BRIDGES LSRD

Table 14-23 (cont'd)
2021 No Action and With Action Conditions Level of Service Analysis
Signalized Intersections

| Intersection | Weekday AM | | | | | | | | Weekday Midday | | | | | | | | Weekday PM | | | | | | | |
|--|------------|-----------|-------------|------|-------------|-----------|-------------|------|----------------|-----------|-------------|------|-------------|-----------|-------------|------|------------|-----------|-------------|------|-------------|-----------|-------------|-------|
| | No Action | | | | With Action | | | | No Action | | | | With Action | | | | No Action | | | | With Action | | | |
| | Lane Group | v/c Ratio | Delay (sec) | LOS | Lane Group | v/c Ratio | Delay (sec) | LOS | Lane Group | v/c Ratio | Delay (sec) | LOS | Lane Group | v/c Ratio | Delay (sec) | LOS | Lane Group | v/c Ratio | Delay (sec) | LOS | Lane Group | v/c Ratio | Delay (sec) | LOS |
| East Broadway and Market Street | | | | | | | | | | | | | | | | | | | | | | | | |
| Eastbound | LT | 0.56 | 17.3 | B | LT | 0.63 | 19.3 | B | LT | 0.50 | 15.8 | B | LT | 0.55 | 17.1 | B | LT | 0.59 | 17.6 | B | LT | 0.71 | 22.2 | C |
| Westbound | TR | 0.61 | 18.7 | B | TR | 0.65 | 20.0 | B | TR | 0.53 | 16.7 | B | TR | 0.55 | 17.2 | B | TR | 0.65 | 20.0 | B | TR | 0.68 | 20.9 | C |
| Northbound | LTR | 0.72 | 37.4 | D | LTR | 0.72 | 37.4 | D | LTR | 0.84 | 45.7 | D | LTR | 0.84 | 45.7 | D | LTR | 0.61 | 31.3 | C | LTR | 0.62 | 31.6 | C |
| East Broadway and Pike Street (East) | | | | | | | | | | | | | | | | | | | | | | | | |
| Eastbound | L | 0.56 | 36.2 | D | L | 0.58 | 37.8 | D | L | 0.49 | 32.6 | C | L | 0.51 | 33.3 | C | L | 0.84 | 62.3 | E | L | 0.87 | 69.1 | E |
| Westbound | T | 0.44 | 25.7 | C | T | 0.45 | 25.8 | C | T | 0.41 | 24.9 | C | T | 0.41 | 25.0 | C | T | 0.42 | 25.1 | C | T | 0.38 | 24.3 | C |
| | TR | 0.66 | 33.1 | C | TR | 0.71 | 35.6 | D | TR | 0.62 | 31.2 | C | TR | 0.64 | 32.3 | C | TR | 0.63 | 31.5 | C | TR | 0.67 | 33.1 | C |
| | Northbound | L | 0.70 | 64.4 | E | L | 0.87 | 87.2 | F | L | 0.61 | 56.2 | E | L | 0.69 | 63.1 | E | L | 0.88 | 86.3 | F | L | 0.98 | 107.9 |
| | TR | 0.69 | 26.5 | C | TR | 0.70 | 26.9 | C | TR | 0.55 | 23.1 | C | TR | 0.55 | 23.2 | C | TR | 0.57 | 23.2 | C | TR | 0.57 | 23.4 | C |
| East Broadway and Pike Street (West) | | | | | | | | | | | | | | | | | | | | | | | | |
| Eastbound | TR | 0.99 | 72.4 | E | TR | 1.11 | 107.5 | F | TR | 1.02 | 80.0 | E | TR | 1.08 | 98.4 | F | TR | 1.07 | 93.4 | F | TR | 1.14 | 118.6 | F |
| Westbound | L | 0.35 | 29.1 | C | L | 0.38 | 30.9 | C | L | 0.31 | 27.8 | C | L | 0.32 | 28.5 | C | L | 0.48 | 36.3 | D | L | 0.51 | 38.5 | D |
| Southbound | L | 0.40 | 24.8 | C | L | 0.42 | 25.2 | C | L | 0.36 | 24.1 | C | L | 0.37 | 24.2 | C | L | 0.33 | 23.5 | C | L | 0.34 | 23.7 | C |
| | T | 0.35 | 47.1 | D | L | 0.36 | 47.5 | D | L | 0.35 | 47.1 | D | L | 0.36 | 47.4 | D | L | 0.33 | 45.7 | D | L | 0.33 | 45.7 | D |
| | T | 0.39 | 21.6 | C | T | 0.41 | 21.9 | C | T | 0.39 | 21.6 | C | T | 0.40 | 21.7 | C | T | 0.43 | 22.1 | C | T | 0.45 | 22.3 | C |
| Division Street and Market Street | | | | | | | | | | | | | | | | | | | | | | | | |
| Westbound | T | 0.27 | 18.2 | B | T | 0.28 | 18.2 | B | T | 0.27 | 18.1 | B | T | 0.27 | 18.1 | B | T | 0.27 | 18.1 | B | T | 0.27 | 18.1 | B |
| Northbound | L | 0.67 | 32.2 | C | L | 0.68 | 32.8 | C | L | 0.93 | 56.9 | E | L | 0.95 | 61.2 | E | L | 0.63 | 29.5 | C | L | 0.68 | 31.7 | C |
| Division Street and Allen Street/Pike Street | | | | | | | | | | | | | | | | | | | | | | | | |
| Westbound | LTR | 0.32 | 28.0 | C | LTR | 0.32 | 28.0 | C | LTR | 0.41 | 30.0 | C | LTR | 0.41 | 30.0 | C | LTR | 0.36 | 28.5 | C | LTR | 0.36 | 28.5 | C |
| Northbound | L | 0.47 | 48.0 | D | L | 0.47 | 48.0 | D | L | 0.66 | 59.8 | E | L | 0.66 | 59.8 | E | L | 0.53 | 50.2 | D | L | 0.53 | 50.2 | D |
| | T | 0.37 | 10.9 | B | T | 0.38 | 11.0 | B | T | 0.31 | 10.3 | B | T | 0.32 | 10.4 | B | T | 0.35 | 10.6 | B | T | 0.36 | 10.7 | B |
| | Southbound | L | 0.34 | 18.9 | B | L | 0.35 | 19.1 | B | L | 0.31 | 18.5 | B | L | 0.32 | 18.6 | B | L | 0.32 | 18.6 | B | L | 0.33 | 18.7 |
| | R | 0.50 | 25.1 | C | R | 0.51 | 25.3 | C | R | 0.44 | 23.7 | C | R | 0.45 | 23.8 | C | R | 0.21 | 18.4 | B | R | 0.22 | 18.6 | B |
| Allen Street and Canal Street | | | | | | | | | | | | | | | | | | | | | | | | |
| Eastbound | LTR | 1.15 | 120.3 | F | LTR | 1.16 | 123.0 | F | LTR | 0.83 | 43.0 | D | LTR | 0.84 | 43.8 | D | LTR | 1.16 | 121.8 | F | LTR | 1.17 | 127.2 | F |
| Westbound | LTR | 0.28 | 21.3 | C | LTR | 0.28 | 21.3 | C | LTR | 0.34 | 22.6 | C | LTR | 0.34 | 22.6 | C | LTR | 0.31 | 21.7 | C | LTR | 0.31 | 21.7 | C |
| Northbound | TR | 0.65 | 28.7 | C | TR | 0.67 | 29.2 | C | TR | 0.56 | 26.5 | C | TR | 0.57 | 26.7 | C | TR | 0.68 | 29.3 | C | TR | 0.70 | 29.8 | C |
| Southbound | LTR | 0.41 | 14.5 | B | LTR | 0.44 | 14.8 | B | LTR | 0.36 | 13.9 | B | LTR | 0.37 | 14.0 | B | LTR | 0.32 | 13.4 | B | LTR | 0.33 | 13.5 | B |
| Allen Street and Grand Street (East) | | | | | | | | | | | | | | | | | | | | | | | | |
| Eastbound | L | 0.54 | 36.0 | D | L | 0.54 | 36.0 | D | L | 0.36 | 30.9 | C | L | 0.36 | 30.9 | C | L | 0.44 | 32.0 | C | L | 0.44 | 32.0 | C |
| Westbound | T | 0.34 | 23.8 | C | T | 0.34 | 23.8 | C | T | 0.43 | 27.7 | C | T | 0.43 | 27.7 | C | T | 0.58 | 30.3 | C | T | 0.58 | 30.3 | C |
| | TR | 0.64 | 31.9 | C | TR | 0.64 | 31.9 | C | TR | 0.68 | 36.9 | D | TR | 0.68 | 36.9 | D | TR | 0.58 | 31.5 | C | TR | 0.58 | 31.5 | C |
| | Northbound | L | 0.41 | 45.5 | D | L | 0.41 | 45.5 | D | L | 0.55 | 52.2 | D | L | 0.55 | 52.2 | D | L | 0.51 | 49.2 | D | L | 0.51 | 49.2 |
| | TR | 0.70 | 27.4 | C | TR | 0.71 | 27.9 | C | TR | 0.54 | 23.3 | C | TR | 0.55 | 23.5 | C | TR | 0.60 | 25.0 | C | TR | 0.62 | 25.3 | C |
| Allen Street and Grand Street (West) | | | | | | | | | | | | | | | | | | | | | | | | |
| Eastbound | TR | 0.79 | 41.4 | D | TR | 0.80 | 42.2 | D | TR | 1.01 | 81.7 | F | TR | 1.01 | 83.3 | F | TR | 1.01 | 76.9 | E | TR | 1.01 | 76.9 | E |
| Westbound | L | 0.21 | 23.8 | C | L | 0.21 | 23.8 | C | L | 0.47 | 37.6 | D | L | 0.47 | 37.6 | D | L | 0.28 | 29.2 | C | L | 0.28 | 29.2 | C |
| Southbound | T | 0.36 | 24.0 | C | T | 0.36 | 24.0 | C | T | 0.29 | 25.2 | C | T | 0.29 | 25.2 | C | T | 0.28 | 24.1 | C | T | 0.33 | 25.2 | C |
| | L | 0.33 | 43.1 | D | L | 0.33 | 43.1 | D | L | 0.45 | 44.3 | D | L | 0.46 | 44.5 | D | L | 0.40 | 42.3 | D | L | 0.40 | 42.3 | D |
| | TR | 0.57 | 24.8 | C | TR | 0.59 | 25.3 | C | TR | 0.51 | 21.6 | C | TR | 0.52 | 21.9 | C | TR | 0.47 | 21.6 | C | TR | 0.50 | 22.1 | C |
| Allen Street and Delancey Street | | | | | | | | | | | | | | | | | | | | | | | | |
| Eastbound | T | 1.01 | 61.4 | E | T | 1.01 | 61.4 | E | T | 0.90 | 34.1 | C | T | 0.90 | 34.1 | C | T | 0.91 | 34.8 | C | T | 0.91 | 34.8 | C |
| Westbound | R | 0.17 | 25.8 | C | R | 0.17 | 25.8 | C | R | 0.21 | 19.5 | B | R | 0.21 | 19.5 | B | R | 0.13 | 18.3 | B | R | 0.13 | 18.3 | B |
| | L | 0.92 | 60.0 | E | L | 0.93 | 63.2 | E | L | 1.03 | 103.4 | F | L | 1.05 | 109.3 | F | L | 1.04 | 105.7 | F | L | 1.06 | 110.4 | F |
| Northbound | L | 0.67 | 12.9 | B | L | 0.67 | 13.1 | B | L | 0.57 | 11.4 | B | L | 0.57 | 11.4 | B | L | 0.57 | 11.4 | B | L | 0.58 | 11.4 | B |
| | T | 0.81 | 40.2 | D | T | 0.83 | 41.3 | D | T | 0.58 | 32.0 | C | T | 0.59 | 32.2 | C | T | 0.58 | 31.6 | C | T | 0.59 | 32.0 | C |
| Southbound | R | 0.37 | 11.2 | B | R | 0.39 | 11.4 | B | R | 0.53 | 20.4 | C | R | 0.54 | 20.6 | C | R | 0.64 | 24.0 | C | R | 0.65 | 24.4 | C |
| | TR | 0.43 | 29.1 | C | TR | 0.44 | 29.4 | C | TR | 0.40 | 28.7 | C | TR | 0.42 | 28.9 | C | TR | 0.53 | 30.8 | C | TR | 0.56 | 31.4 | C |
| Bowery and Canal Street | | | | | | | | | | | | | | | | | | | | | | | | |
| Eastbound | T | 0.82 | 31.0 | C | T | 0.82 | 31.0 | C | T | 0.82 | 30.9 | C | T | 0.82 | 30.9 | C | T | 1.07 | 74.1 | E | T | 1.07 | 74.1 | E |
| Westbound | R | 0.35 | 20.7 | C | R | 0.38 | 21.3 | C | R | 0.26 | 19.4 | B | R | 0.29 | 19.8 | B | R | 0.18 | 18.2 | B | R | 0.22 | 18.9 | B |
| | T | 0.83 | 31.1 | C | T | 0.83 | 31.1 | C | T | 0.66 | 25.0 | C | T | 0.66 | 25.0 | C | T | 0.44 | 20.8 | C | T | 0.44 | 20.8 | C |
| Northbound | T | 0.59 | 33.8 | C | T | 0.61 | 34.2 | C | T | 0.54 | 32.7 | C | T | 0.55 | 32.8 | C | T | 0.46 | 31.0 | C | T | 0.47 | 31.2 | C |
| Southbound | DefL | 0.90 | 50.7 | D | DefL | 0.92 | 52.5 | D | DefL | 0.87 | 47.2 | D | DefL | 0.88 | 47.5 | D | DefL | 1.10 | 96.2 | F | DefL | 1.10 | 96.5 | F |
| | TR | 0.67 | 27.1 | C | TR | 0.69 | 27.6 | C | TR | 0.64 | 26.0 | C | TR | 0.65 | 26.3 | C | TR | 0.38 | 19.6 | B | TR | 0.39 | 19.8 | B |
| Bowery and Bayard Street | | | | | | | | | | | | | | | | | | | | | | | | |
| Eastbound | LR | 0.30 | 23.1 | C | LR | 0.30 | 23.1 | C | LR | 0.59 | 32.4 | C | LR | 0.59 | 32.4 | C | LR | 0.68 | 36.8 | D | LR | 0.68 | 36.8 | D |
| Northbound | T | 0.43 | 17.9 | B | T | 0.44 | 18.1 | B | T | 0.49 | 18.8 | B | T | 0.50 | 18.9 | B | T | 0.58 | 20.1 | C | T | 0.59 | 20.2 | C |
| Southbound | T | 0.24 | 15.9 | B | T | 0.25 | 16.0 | B | T | 0.20 | 15.5 | B | T | 0.21 | 15.6 | B | T | 0.14 | 15.0 | C | T | 0.15 | 15.1 | C |
| Bowery and Division Street/Doyers Street | | | | | | | | | | | | | | | | | | | | | | | | |
| Eastbound | R | 0.04 | 26.4 | C | R | 0.04 | 26.4 | C | R | 0.07 | 26.8 | C | R | 0.07 | 26.8 | C | R | 0.07 | 26.8 | C | R | 0.07 | 26.8 | C |
| Westbound | L | 0.74 | 51.5 | D | L | 0.87 | 67.2 | E | L | 0.76 | 53.0 | D | L | 0.80 | 56.8 | E | L | 0.61 | 42.9 | D | L | 0.65 | 45.0 | D |
| | R | 0.59 | 19.5 | B | R | 0.60 | 19.7 | B | R | 0.67 | 21.6 | C | R | 0.67 | 21.6 | C | R | 0.59 | 19.2 | B | R | 0.59 | 19.2 | B |
| Northbound | TR | 0.36 | 20.5 | C | TR | 0.39 | 20.8 | C | TR | 0.40 | 21.0 | C | TR | 0.41 | 21.1 | C | TR | 0.60 | 24.3 | C | TR | 0.62 | 24.5 | C |
| Southbound | T | 0.37 | 20.6 | C | T | 0.39 | 20.8 | C | T | 0.37 | 20.6 | C | T | 0.38 | 20.7 | C | T | 0.24 | 19.0 | B | T | 0.25 | 19.1 | B |

Table 14-23 (cont'd)
2021 No Action and With Action Conditions Level of Service Analysis
Signalized Intersections

| Intersection | Weekday AM | | | | | | | | Weekday Midday | | | | | | | | Weekday PM | | | | | | | |
|--|------------|------|-------------|-----|-------------|------|-------------|-----|----------------|------|-------------|-----|-------------|------|-------------|-----|------------|------|-------------|-----|-------------|------|-------------|-----|
| | No Action | | | | With Action | | | | No Action | | | | With Action | | | | No Action | | | | With Action | | | |
| | Lane Group | v/c | Delay (sec) | LOS | Lane Group | v/c | Delay (sec) | LOS | Lane Group | v/c | Delay (sec) | LOS | Lane Group | v/c | Delay (sec) | LOS | Lane Group | v/c | Delay (sec) | LOS | Lane Group | v/c | Delay (sec) | LOS |
| Chatham Square and East Broadway | | | | | | | | | | | | | | | | | | | | | | | | |
| Westbound | L | 0.32 | 17.7 | B | L | 0.35 | 18.1 | B | L | 0.25 | 16.6 | B | L | 0.26 | 16.8 | B | L | 0.31 | 17.3 | B | L | 0.33 | 17.6 | B |
| | R | 0.18 | 15.9 | B | R | 0.21 | 16.3 | B | R | 0.15 | 15.6 | B | R | 0.16 | 15.8 | B | R | 0.23 | 16.4 | B | R | 0.24 | 16.6 | B |
| Northbound | T | 0.23 | 15.9 | B | T | 0.24 | 16.0 | B | T | 0.30 | 16.7 | B | T | 0.30 | 16.7 | B | T | 0.45 | 18.5 | B | T | 0.46 | 18.6 | B |
| | R | 0.52 | 23.2 | C | R | 0.55 | 24.2 | C | R | 0.73 | 35.1 | D | R | 0.78 | 39.0 | D | R | 0.88 | 49.8 | D | R | 0.97 | 66.0 | E + |
| Southbound | L | 0.69 | 32.6 | C | L | 0.78 | 39.5 | D | L | 0.82 | 46.9 | D | L | 0.87 | 53.7 | D | L | 0.71 | 38.5 | D | L | 0.80 | 48.1 | D |
| | T | 0.29 | 16.5 | B | T | 0.32 | 16.8 | B | T | 0.26 | 16.1 | B | T | 0.26 | 16.2 | B | T | 0.19 | 15.5 | B | T | 0.20 | 15.5 | B |
| Chatham Square and Worth Street/Oliver Street | | | | | | | | | | | | | | | | | | | | | | | | |
| Eastbound (Worth Street) | L | 1.24 | 209.1 | F | L | 1.32 | 236.4 | F + | L | 1.08 | 131.5 | F | L | 1.13 | 148.1 | F + | L | 1.16 | 145.2 | F | L | 1.25 | 177.7 | F + |
| | LTR | 1.12 | 136.6 | F | LTR | 1.22 | 173.5 | F + | LTR | 1.00 | 91.1 | F | LTR | 1.05 | 104.5 | F + | LTR | 1.16 | 134.1 | F | LTR | 1.25 | 167.5 | F + |
| Eastbound (Mott Street) | L | 0.58 | 43.1 | D | L | 0.58 | 43.1 | D | L | 0.64 | 45.7 | D | L | 0.64 | 45.7 | D | L | 0.83 | 61.0 | E | L | 0.83 | 61.0 | E |
| Westbound | LT | 0.85 | 44.5 | D | LT | 0.85 | 44.5 | D | LT | 0.56 | 29.8 | C | LT | 0.56 | 29.8 | C | LT | 0.51 | 28.5 | C | LT | 0.51 | 28.5 | C |
| | R | 0.74 | 41.8 | D | R | 0.77 | 44.5 | D | R | 0.84 | 53.4 | D | R | 0.85 | 54.8 | D | R | 1.04 | 92.9 | F | R | 1.06 | 96.6 | F + |
| Northbound | LTR | 0.08 | 21.5 | C | LTR | 0.08 | 21.5 | C | LTR | 0.11 | 21.8 | C | LTR | 0.11 | 21.8 | C | LTR | 0.08 | 21.5 | C | LTR | 0.08 | 21.5 | C |
| Southbound | L | 0.99 | 87.8 | F | L | 0.99 | 87.8 | F | L | 0.69 | 42.3 | D | L | 0.69 | 42.3 | D | L | 0.72 | 44.3 | D | L | 0.72 | 44.3 | D |
| | TR | 0.96 | 65.5 | E | TR | 1.09 | 101.8 | F + | TR | 1.09 | 106.9 | F | TR | 1.16 | 129.4 | F + | TR | 0.92 | 60.6 | E | TR | 0.99 | 76.1 | E + |
| Worth Street and Centre Street | | | | | | | | | | | | | | | | | | | | | | | | |
| Eastbound | L | 0.35 | 22.7 | C | L | 0.37 | 25.3 | C | L | 0.25 | 13.5 | B | L | 0.25 | 14.0 | B | L | 0.22 | 12.4 | B | L | 0.22 | 12.9 | B |
| | R | 0.52 | 18.5 | B | R | 0.54 | 19.0 | B | R | 0.43 | 13.2 | B | R | 0.44 | 13.5 | B | R | 0.69 | 19.3 | B | R | 0.74 | 21.2 | C |
| Westbound | T | 0.73 | 36.6 | D | T | 0.85 | 46.2 | D + | T | 0.42 | 22.0 | C | T | 0.45 | 22.5 | C | T | 0.39 | 21.4 | C | T | 0.43 | 22.1 | C |
| | R | 0.43 | 28.6 | C | R | 0.47 | 30.0 | C | R | 0.27 | 20.4 | C | R | 0.29 | 20.8 | C | R | 0.21 | 19.0 | C | R | 0.24 | 21.3 | C |
| Northbound | L | 0.12 | 17.8 | B | L | 0.12 | 17.8 | B | L | 0.24 | 24.0 | C | L | 0.24 | 24.0 | C | L | 0.13 | 21.7 | C | L | 0.13 | 21.7 | C |
| | TR | 0.62 | 24.4 | C | TR | 0.62 | 24.4 | C | TR | 0.63 | 29.0 | C | TR | 0.63 | 29.0 | C | TR | 0.64 | 28.8 | C | TR | 0.64 | 28.8 | C |
| Worth Street and Lafayette Street | | | | | | | | | | | | | | | | | | | | | | | | |
| Eastbound | T | 0.42 | 23.7 | C | T | 0.44 | 24.0 | C | T | 0.38 | 23.0 | C | T | 0.41 | 23.4 | C | T | 0.56 | 26.6 | C | T | 0.63 | 28.7 | C |
| | R | 0.25 | 21.5 | C | R | 0.25 | 21.5 | C | R | 0.29 | 22.4 | C | R | 0.29 | 22.4 | C | R | 0.19 | 20.3 | C | R | 0.19 | 20.3 | C |
| Westbound | T | 0.41 | 20.7 | C | T | 0.41 | 21.1 | C | L | 0.41 | 20.2 | C | L | 0.41 | 20.8 | C | L | 0.30 | 20.6 | C | L | 0.31 | 22.4 | C |
| | T | 0.24 | 14.2 | B | T | 0.31 | 15.0 | B | T | 0.20 | 13.7 | B | T | 0.22 | 13.9 | B | T | 0.20 | 13.7 | B | T | 0.23 | 14.0 | B |
| Southbound | LTR | 0.83 | 32.2 | C | LTR | 0.83 | 32.6 | C | LTR | 0.75 | 28.6 | C | LTR | 0.75 | 28.7 | C | LTR | 0.81 | 30.5 | C | LTR | 0.81 | 30.7 | C |
| Worth Street and Broadway | | | | | | | | | | | | | | | | | | | | | | | | |
| Eastbound | TR | 0.58 | 26.2 | C | TR | 0.59 | 26.4 | C | TR | 0.51 | 24.2 | C | TR | 0.52 | 24.4 | C | TR | 0.56 | 25.4 | C | TR | 0.59 | 26.2 | C |
| Westbound | L | 0.32 | 23.2 | C | L | 0.33 | 23.5 | C | L | 0.36 | 24.1 | C | L | 0.37 | 24.5 | C | L | 0.29 | 22.3 | C | L | 0.30 | 22.7 | C |
| | T | 0.30 | 20.3 | C | T | 0.37 | 21.5 | C | T | 0.23 | 19.4 | B | T | 0.25 | 19.7 | B | T | 0.27 | 20.0 | B | T | 0.31 | 20.4 | C |
| Southbound | L | 0.20 | 13.8 | B | L | 0.21 | 14.0 | B | L | 0.19 | 13.8 | B | L | 0.22 | 14.3 | B | L | 0.27 | 14.9 | B | L | 0.33 | 16.1 | B |
| | TR | 0.50 | 16.4 | B | TR | 0.50 | 16.4 | B | TR | 0.50 | 16.3 | B | TR | 0.50 | 16.3 | B | TR | 0.71 | 20.6 | C | TR | 0.71 | 20.6 | C |

Notes: L = Left Turn, T = Through, R = Right Turn, DefL = Defacto Left Turn, LOS = Level of Service
+ Denotes a significant adverse traffic impact

Table 14-24
2021 No Action and With Action Conditions Level of Service Analysis
Unsignalized Intersections

| Intersection | Weekday AM | | | | | | | | Weekday Midday | | | | | | | | Weekday PM | | | | | | | |
|---|------------|------|-------------|-----|-------------|------|-------------|-----|----------------|------|-------------|-----|-------------|------|-------------|-----|------------|------|-------------|-----|-------------|------|-------------|-----|
| | No Action | | | | With Action | | | | No Action | | | | With Action | | | | No Action | | | | With Action | | | |
| | Lane Group | v/c | Delay (sec) | LOS | Lane Group | v/c | Delay (sec) | LOS | Lane Group | v/c | Delay (sec) | LOS | Lane Group | v/c | Delay (sec) | LOS | Lane Group | v/c | Delay (sec) | LOS | Lane Group | v/c | Delay (sec) | LOS |
| Cherry Street and Clinton Street | | | | | | | | | | | | | | | | | | | | | | | | |
| Westbound | TR | 0.17 | 8.2 | A | TR | 0.17 | 8.3 | A | TR | 0.17 | 8.3 | A | TR | 0.17 | 8.4 | A | TR | 0.25 | 8.9 | A | TR | 0.26 | 9.2 | A |
| Northbound | LT | 0.25 | 8.8 | A | LT | 0.30 | 9.3 | A | LT | 0.28 | 9.1 | A | LT | 0.31 | 9.4 | A | LT | 0.36 | 10.0 | A | LT | 0.43 | 10.8 | B |
| Pike Street and Monroe Street | | | | | | | | | | | | | | | | | | | | | | | | |
| Eastbound | R | 0.08 | 11.6 | B | R | 0.09 | 11.8 | B | R | 0.10 | 11.8 | B | R | 0.09 | 11.8 | B | R | 0.09 | 11.5 | B | R | 0.09 | 11.6 | B |

Notes: L = Left Turn, T = Through, R = Right Turn, DefL = Defacto Left Turn, LOS = Level of Service
+ Denotes a significant adverse traffic impact

- Southbound left-turn at the South Street and Pike Slip intersection would deteriorate within LOS D (from a v/c ratio of 0.63 and 41.7 spv of delay to a v/c ratio of 0.73 and 47.5 spv of delay), an increase in delay of more than 3 seconds during the weekday PM peak hour. This projected increase in delay constitutes a significant adverse impact;
- Eastbound approach at the South Street and Clinton Street intersection would deteriorate within LOS F (from a v/c ratio of 1.07 and 82.3 spv of delay to a v/c ratio of 1.25 and 151.0 spv of delay), an increase in delay of more than 3 seconds during the weekday PM peak hour. This projected increase in delay constitutes a significant adverse impact;
- Westbound approach at the South Street and Montgomery Street (north) intersection would deteriorate within LOS F (from a v/c ratio of 1.13 and 91.9 spv of delay to a v/c ratio of 1.17 and 106.2 spv of delay), and increase of more than 3 seconds during the weekday PM peak hour. This projected increase in delay constitutes a significant adverse impact;

- Northbound approach at the South Street and Montgomery Street (north) intersection would deteriorate from LOS D (v/c ratio of 0.83 and 47.4 spv of delay) to LOS E (v/c ratio of 0.97 and 75.6 spv of delay), an increase in delay of more than 5 seconds during the weekday PM peak hour. This projected increase in delay constitutes a significant adverse impact;
- Southbound approach at the South Street and Montgomery Street (north) intersection would deteriorate from LOS C (v/c ratio of 0.68 and 33.2 spv of delay) to LOS E (v/c ratio of 0.97 and 63.8 spv of delay), an increase of more than 5 seconds during the weekday AM peak hour. This projected increase in delay constitutes a significant adverse impact;
- Southbound approach at the South Street and Montgomery Street (south) intersection would deteriorate from LOS D (v/c ratio of 0.74 and 37.2 spv of delay) to LOS E (v/c ratio of 0.96 and 64.8 spv of delay), and within LOS F (from a v/c ratio of 1.43 and 243.3 spv of delay to a v/c ratio of 1.63 and 330.2 spv of delay), an increase in delay of more than 5 seconds and 3 seconds during the weekday AM and PM peak hour, respectively. These projected increases in delay constitute a significant adverse impacts;
- Eastbound left-turn at the Madison Street and Pike Street (east) intersection would deteriorate within LOS F (from a v/c ratio of 1.14 and 140.0 spv of delay to a v/c ratio of 1.16 and 150.3 spv of delay), and within LOS F (from a v/c ratio of 0.93 and 89.3 spv of delay to a v/c ratio of 0.96 and 98.7 spv of delay), increases in delay of more than 3 seconds, during the weekday AM and PM peak hours, respectively. These projected increases in delay constitute significant adverse impacts;
- Northbound approach at the Madison Street and Montgomery Street Intersection would deteriorate within LOS F (from a v/c ratio of 1.14 and 117.4 spv of delay to a v/c ratio of 1.18 and 133.3 spv of delay), an increase in delay of more than 3 seconds during the weekday PM peak hour. This projected increase in delay constitutes a significant adverse impact;
- Eastbound left-turn at the East Broadway and Pike Street (east) intersection would deteriorate within LOS E (from a v/c ratio of 0.84 and 62.3 spv of delay to a v/c ratio of 0.87 and 69.1 spv of delay), an increase in delay of more than 5 seconds during the weekday PM peak hour. This projected increase in delay constitutes a significant adverse impact;
- Northbound left-turn at the East Broadway and Pike Street (east) intersection would deteriorate from LOS E (v/c ratio of 0.70 and 64.4 spv of delay) to LOS F (v/c ratio of 0.87 and 87.2 spv of delay), within LOS E (from a v/c ratio of 0.61 and 56.2 spv of delay to a v/c ratio of 0.69 and 63.1 spv of delay), and within LOS F (from a v/c ratio of 0.88 and 86.3 spv of delay to a v/c ratio of 0.98 and 107.9 spv of delay), increases in delay of more than 4 seconds, 4 seconds, and 3 seconds, during the weekday AM, midday and PM peak hours, respectively. These projected increases in delay constitute significant adverse impacts;
- Eastbound approach at the East Broadway and Pike Street (west) intersection would deteriorate from LOS E (v/c ratio of 0.99 and 72.4 spv of delay) to LOS F (v/c ratio of 1.11 and 107.5 spv of delay), within LOS F (from a v/c ratio of 1.02 and 80.0 spv of delay to a v/c ratio of 1.08 and 98.4 spv of delay), and within LOS F (from a v/c ratio of 1.07 and 93.4 spv of delay to a v/c ratio of 1.14 and 118.6 spv of delay), increases in delay of more than 4 seconds, 3 seconds, and 3 seconds, during the weekday AM, midday and PM peak hours, respectively. These projected increases in delay constitute significant adverse impacts;
- Northbound left-turn at the Division Street and Market Street intersection would deteriorate within LOS E (from a v/c ratio of 0.93 and 56.9 spv of delay to a v/c ratio of 0.95 and 61.2

- spv of delay), an increase in delay of more than 4 seconds during the weekday midday peak hour. This projected increase in delay constitutes a significant adverse impact;
- Eastbound approach at the Canal Street and Allen Street intersection would deteriorate within LOS F (from a v/c ratio of 1.16 and 121.8 spv of delay to a v/c ratio of 1.17 and 127.2 spv of delay), an increase in delay of more than 3 seconds during the weekday PM peak hour. This projected increase in delay constitutes a significant adverse impact;
 - Westbound left-turn at the Allen Street and Delancey Street intersection would deteriorate within LOS F (from a v/c ratio of 1.03 and 103.4 spv of delay to a v/c ratio of 1.05 and 109.3 spv of delay), and within LOS F (from a v/c ratio of 1.04 and 105.7 spv of delay to a v/c ratio of 1.06 and 110.4 spv of delay), increases in delay of more than 3 seconds during the weekday midday and PM peak hours. These projected increases in delay constitute significant adverse impacts;
 - Westbound left-turn at The Bowery and Division Street/Doyers Street intersection would deteriorate from LOS D (v/c ratio of 0.74 and 51.5 spv of delay) to LOS E (v/c ratio of 0.87 and 67.2 spv of delay), an increase in delay of more than 5 seconds, during the weekday AM peak hour. This projected increase in delay constitutes a significant adverse impact;
 - Northbound right-turn at the Chatham Square and East Broadway intersection would deteriorate from LOS D (v/c ratio of 0.88 and 49.8 spv of delay) to LOS E (v/c ratio of 0.97 and 66.0 spv of delay), an increase in delay of more than 5 seconds during the weekday PM peak hour. This projected increase in delay constitutes a significant adverse impact;
 - Southbound left-turn at the Chatham Square and East Broadway intersection would deteriorate within LOS D (from a v/c ratio of 0.82 and 46.9 spv of delay to a v/c ratio of 0.87 and 53.7 spv of delay), and within LOS D (from a v/c ratio of 0.71 and 38.5 spv of delay to a v/c ratio of 0.80 and 48.1 spv of delay), increases in delay of more than 5 seconds during the weekday midday and PM peak hours. These projected increases in delay constitute significant adverse impacts;
 - Eastbound (Worth Street) left-turn at the Chatham Square and Worth Street/Oliver Street intersection would deteriorate within LOS F (from a v/c ratio of 1.24 and 209.1 spv of delay to a v/c ratio of 1.32 and 236.4 spv of delay), within LOS F (from a v/c ratio of 1.08 and 131.5 spv of delay to a v/c ratio of 1.13 and 148.1 spv of delay), and within LOS F (from a v/c ratio of 1.16 and 145.2 spv of delay to a v/c ratio of 1.25 and 177.7 spv of delay), increases in delay of more than 3 seconds during the weekday AM, midday and PM peak hours. These projected increases in delay constitute significant adverse impacts;
 - Eastbound (Worth Street) shared lane at the Chatham Square and Worth Street/Oliver Street intersection would deteriorate within LOS F (from a v/c ratio of 1.12 and 136.6 spv of delay to a v/c ratio of 1.22 and 173.5 spv of delay), within LOS F (from a v/c ratio of 1.00 and 91.1 spv of delay to a v/c ratio of 1.05 and 104.5 spv of delay), and within LOS F (from a v/c ratio of 1.16 and 134.1 spv of delay to a v/c ratio of 1.25 and 167.5 spv of delay), increases in delay of more than 3 seconds during the weekday AM, midday and PM peak hours. These projected increases in delay constitute significant adverse impacts;
 - Westbound right-turn at the Chatham Square and Worth Street/Oliver Street intersection would deteriorate within LOS F (from a v/c ratio of 1.04 and 92.9 spv of delay to a v/c ratio of 1.06 and 96.6 spv of delay), an increase of more than 3 seconds during the weekday PM peak hour. This projected increase in delay constitutes a significant adverse impact;

- Southbound shared lane at the Chatham Square and Worth Street/Oliver Street intersection would deteriorate from LOS E (v/c ratio of 0.96 and 65.5 spv of delay) to LOS F (v/c ratio of 1.09 and 101.8 spv of delay), within LOS F (from a v/c ratio of 1.09 and 106.9 spv of delay to a v/c ratio of 1.16 and 129.4 spv of delay), and within LOS E (from a v/c ratio of 0.92 and 60.6 spv of delay to a v/c ratio of 0.99 and 76.1 spv of delay), increases in delay of more than 4 seconds, 3 seconds, and 4 seconds during the weekday AM, midday and PM peak hours, respectively. These projected increases in delay constitute significant adverse impacts; and
- Westbound through at the Worth Street and Centre Street intersection would deteriorate within LOS D (from a v/c ratio of 0.73 and 36.6 spv of delay to a v/c ratio of 0.85 and 46.2 spv of delay), an increase of more than 5 seconds during the weekday AM peak hour. This projected increase in delay constitutes a significant adverse impact.

E. DETAILED TRANSIT ANALYSIS

As described above in Section B, “Preliminary Analysis Methodology and Screening Assessment,” the East Broadway Station (F line) has been selected for station analysis for the weekday AM and PM peak hours. Subway line-haul analysis for F line was also conducted for weekday AM and PM peak hours.

EXISTING CONDITIONS

SUBWAY SERVICE

Subway station data collection was conducted in March 2017 during the hours of 7:00 to 10:00 AM and 4:00 to 7:00 PM to establish the baseline volumes for the subway station analysis. As shown in **Tables 14-25 and 14-26**, all analyzed vertical circulation elements and control areas currently operate at acceptable levels during the weekday AM and PM peak periods, exception for the S1 stairway at the East Broadway-Rutgers Street Station during the AM peak period (v/c ratio of 1.15).

With regard to subway line-haul conditions, ridership, and train throughput data from NYCT were reviewed to identify ridership levels for the F line’s peak load points in the peak direction of travel. As summarized in **Table 14-27**, the F line is currently operating at approximately 87-percent capacity in the peak northbound direction during the weekday AM peak hour and at approximately 85-percent capacity in the peak southbound direction during the weekday PM peak hour.

THE FUTURE WITHOUT THE PROPOSED PROJECTS

SUBWAY SERVICE

Estimates of peak hour transit volumes in the 2021 No Action condition were developed by applying the *CEQR Technical Manual* recommended annual background growth rates. An additional three percent of transit volume growth to account for small- to moderate-sized No Build projects within a ½-mile of the project sites, and trips generated by two discrete No Build projects in the area were also incorporated into the future No Action transit volumes.

Table 14-25

Existing Conditions Subway Vertical Circulation Element Analysis
East Broadway-Rutgers Street Station

| Stair | Location | Effective Width (ft.) | Peak Hour Volumes | | Peak 15-Minute Volumes | | Surge Factor | | Friction Factor | V/C Ratio | LOS |
|--------------|--------------|-----------------------|-------------------|------|------------------------|------|--------------|------|-----------------|-----------|-----|
| | | | Entry | Exit | Entry | Exit | Up | Down | | | |
| AM Peak Hour | | | | | | | | | | | |
| P3 | Platform | 4.00 | 907 | 346 | 283 | 108 | 0.75 | 1.00 | 0.90 | 0.79 | C |
| P4 | Platform | 4.00 | 69 | 298 | 22 | 93 | 0.75 | 1.00 | 0.90 | 0.27 | A |
| S1 | Street Level | 3.50 | 978 | 685 | 306 | 214 | 0.90 | 1.00 | 0.90 | 1.15 | D |
| PM Peak Hour | | | | | | | | | | | |
| P3 | Platform | 4.00 | 340 | 352 | 106 | 110 | 0.75 | 1.00 | 0.90 | 0.47 | B |
| P4 | Platform | 4.00 | 49 | 331 | 15 | 103 | 0.75 | 1.00 | 0.90 | 0.28 | A |
| S1 | Street Level | 3.50 | 351 | 753 | 110 | 235 | 0.90 | 1.00 | 0.90 | 0.79 | C |

Table 14-26

Existing Conditions Fare Array Analysis
East Broadway-Rutgers Street Station

| Control Element | Quantity | Peak Hour Volumes | | Peak 15-Minute Volumes | | Surging Factor | Friction Factor | V/C Ratio | LOS |
|--------------------|----------|-------------------|------|------------------------|------|----------------|-----------------|-----------|-----|
| | | Entry | Exit | Entry | Exit | | | | |
| Weekday AM | | | | | | | | | |
| Two-Way Turnstiles | 3 | 993 | 630 | 310 | 197 | 0.80 | 0.90 | 0.41 | A |
| Weekday PM | | | | | | | | | |
| Two-Way Turnstiles | 3 | 374 | 681 | 117 | 213 | 0.80 | 0.90 | 0.26 | A |

Table 14-27

Existing Conditions Subway Line-haul Analysis
F Line

| Subway Line/Direction | Max. Load Point | Average Trains/hr | Cars/Train | Average Number of Cars/hr | Average Passenger/hr | Peak Hour Capacity | V/C Ratio |
|-----------------------------|-----------------------------|-------------------|------------|---------------------------|----------------------|--------------------|-----------|
| Weekday AM Peak Hour | | | | | | | |
| F/NB | Second Avenue | 13.9 | 10 | 139 | 16,244 | 18,765 | 0.87 |
| Weekday PM Peak Hour | | | | | | | |
| F/SB | Broadway – Lafayette Street | 14.1 | 10 | 141 | 16,184 | 19,035 | 0.85 |

Source: MTA 2014 cordon counts, grown to 2017 existing conditions volumes

As shown in **Tables 14-28 to 14-30**, the levels of service at the analyzed subway station vertical circulation elements and control area at the East Broadway-Rutgers Street subway station would operate at acceptable levels, with the exception of the S1 and P3 stairways during the AM and PM peak periods. The line-haul capacity for the F line will operate at deteriorated levels when compared to the existing condition.

Table 14-28

**No Action Condition Subway Vertical Circulation Element Analysis
East Broadway-Rutgers Street Station**

| Stair | Location | Effective Width (ft.) | Peak Hour Volumes | | Peak 15-Minute Volumes | | Surge Factor | | Friction Factor | V/C Ratio | LOS |
|--------------|--------------|-----------------------|-------------------|-------|------------------------|------|--------------|------|-----------------|-----------|-----|
| | | | Entry | Exit | Entry | Exit | Up | Down | | | |
| AM Peak Hour | | | | | | | | | | | |
| P3 | Platform | 4.00 | 1,225 | 389 | 383 | 122 | 0.75 | 1.00 | 0.90 | 1.01 | D |
| P4 | Platform | 4.00 | 93 | 335 | 29 | 105 | 0.75 | 1.00 | 0.90 | 0.31 | A |
| S1 | Street Level | 3.50 | 1320 | 767 | 413 | 240 | 0.9 | 1.00 | 0.90 | 1.44 | E |
| PM Peak Hour | | | | | | | | | | | |
| P3 | Platform | 4.00 | 471 | 519 | 147 | 162 | 0.75 | 1.00 | 0.90 | 0.67 | B |
| P4 | Platform | 4.00 | 68 | 487 | 21 | 152 | 0.75 | 1.00 | 0.90 | 0.41 | A |
| S1 | Street Level | 3.50 | 501 | 1,078 | 157 | 337 | 0.90 | 1.00 | 0.90 | 1.12 | D |

Table 14-29

**2021 No Action Condition Fare Array Analysis
East Broadway-Rutgers Street Station**

| Control Element | Quantity | Peak Hour Volumes | | Peak 15-Minute Volumes | | Surging Factor | Friction Factor | V/C Ratio | LOS |
|--------------------|----------|-------------------|-------|------------------------|------|----------------|-----------------|-----------|-----|
| | | Entry | Exit | Entry | Exit | | | | |
| Weekday AM | | | | | | | | | |
| Two-Way Turnstiles | 3 | 1,336 | 710 | 418 | 222 | 0.80 | 0.90 | 0.53 | B |
| Weekday PM | | | | | | | | | |
| Two-Way Turnstiles | 3 | 524 | 1,003 | 164 | 313 | 0.80 | 0.90 | 0.37 | A |

Table 14-30

**2021 No Action Condition Subway Line-haul Analysis
F Line**

| Subway Line/Direction | Max. Load Point | Average Trains/hr | Cars/Train | Average Number of Cars/hr | Average Passenger/hr | Peak Hour Capacity | V/C Ratio |
|-----------------------------|-----------------------------|-------------------|------------|---------------------------|----------------------|--------------------|-----------|
| Weekday AM Peak Hour | | | | | | | |
| F/NB | Second Avenue | 13.9 | 10 | 139 | 17,021 | 18,765 | 0.92 |
| Weekday PM Peak Hour | | | | | | | |
| F/SB | Broadway – Lafayette Street | 14.1 | 10 | 141 | 16,958 | 19,035 | 0.91 |

THE FUTURE WITH THE PROPOSED PROJECTS

SUBWAY SERVICE

The P3 and P4 platform stairways are approximately 80 feet apart and connect to the intermediate mezzanine level, which has a ramp leading to a single control area at the upper mezzanine level. As usage of the P3 stairway (which is closer to the adjacent control area) is operating over capacity, a shift in subway rider preference to the P4 stairway is anticipated to occur under With Action condition. Approximately 80 percent of the project-generated outbound subway trips were assigned to the P3 stairway with the remaining trips to the P4 stairway. This behavior pattern was accounted for in the analyses presented below in consultant with NYCT.

As shown in **Table 14-31 through 14-32**, the subway station vertical elements and control area level of service would operate at acceptable levels of service with the exception of the S1

stairway during the AM and PM peak periods and the P3 stairway during the AM peak period. For the S1 stairway, corresponding WITs for the AM and PM peak periods have been calculated at 19.1 and 6.6, respectively. Since these values are greater than the CEQR impact thresholds depicted in **Table 14-11**, it is determined that the proposed projects would result in a significant adverse impact on the S1 stairway at the East Broadway-Rutgers Street Station. The corresponding WIT for the P3 stairway during the AM peak period has been calculated at 6.4. Since this value is above the CEQR impact thresholds depicted in **Table 14-11**, the projected condition for the P3 stairway constitutes significant adverse impact. Potential measures to mitigate these projected impacts are described in Chapter 21, “Mitigation.”

Table 14-31

With Action Condition Subway Vertical Circulation Element Analysis
East Broadway-Rutgers Street Station

| Stair | Location | Effective Width (ft.) | Peak Hour Volumes | | Peak 15-Minute Volumes | | Surge Factor | | Friction Factor | V/C Ratio | LOS |
|--------------|--------------|-----------------------|-------------------|-------|------------------------|------|--------------|------|-----------------|-----------|-----|
| | | | Entry | Exit | Entry | Exit | Up | Down | | | |
| AM Peak Hour | | | | | | | | | | | |
| P3 | Platform | 4.00 | 1,868 | 463 | 584 | 145 | 0.75 | 1.00 | 0.90 | 1.44 | E |
| P4 | Platform | 4.00 | 254 | 399 | 79 | 125 | 0.75 | 1.00 | 0.90 | 0.45 | B |
| S1 | Street Level | 3.50 | 2,124 | 905 | 664 | 283 | 0.90 | 1.00 | 0.90 | 2.07 | F |
| PM Peak Hour | | | | | | | | | | | |
| P3 | Platform | 4.00 | 764 | 837 | 239 | 262 | 0.75 | 1.00 | 0.90 | 1.09 | D |
| P4 | Platform | 4.00 | 110 | 786 | 34 | 246 | 0.75 | 1.00 | 0.90 | 0.67 | B |
| S1 | Street Level | 3.50 | 836 | 1,695 | 261 | 530 | 0.90 | 1.00 | 0.90 | 1.80 | F |

Table 14-32

2021 With Action Condition Fare Array Analysis
East Broadway-Rutgers Street Station

| Control Element | Quantity | Peak Hour Volumes | | Peak 15-Minute Volumes | | Surging Factor | Friction Factor | V/C Ratio | LOS |
|--------------------|----------|-------------------|-------|------------------------|------|----------------|-----------------|-----------|-----|
| | | Entry | Exit | Entry | Exit | | | | |
| Weekday AM | | | | | | | | | |
| Two-Way Turnstiles | 3 | 2,140 | 848 | 669 | 265 | 0.80 | 0.90 | 0.78 | C |
| Weekday PM | | | | | | | | | |
| Two-Way Turnstiles | 3 | 859 | 1,620 | 268 | 506 | 0.80 | 0.90 | 0.60 | B |

With regard to subway line-haul conditions, trip increments associated with the proposed project would be expected to result in increases in ridership levels for the F line. However, as shown in **Table 14-33**, no significant adverse line-haul impacts would be expected from these increases in ridership levels.

Table 14-33

2021 With Action Condition Subway Line-haul Analysis
F Line

| Subway Line/Direction | Max. Load Point | Average Trains/hr | Cars/Train | Average Number of Cars/hr | Average Passenger/hr | Peak Hour Capacity | V/C Ratio |
|-----------------------------|-----------------------------|-------------------|------------|---------------------------|----------------------|--------------------|-----------|
| Weekday AM Peak Hour | | | | | | | |
| F/NB | Second Avenue | 13.9 | 10 | 139 | 18,233 | 18,765 | 0.97 |
| Weekday PM Peak Hour | | | | | | | |
| F/SB | Broadway – Lafayette Street | 14.1 | 10 | 141 | 18,315 | 19,035 | 0.96 |

F. DETAILED PEDESTRIANS ANALYSIS

As described above in Section B, “Preliminary Analysis Methodology, and Screening Assessment,” Level 1 and Level 2 screening analyses were prepared to identify the pedestrian elements that warranted a detailed analysis. Based on the assignment of pedestrian trips, 18 sidewalks, 16 corner reservoirs, and 12 crosswalks were selected for analysis for the weekday AM, midday, and PM peak hours.

EXISTING CONDITIONS

Pedestrian data were collected in May 2016 and March 2017 in accordance with procedures outlined in the *CEQR Technical Manual* during the weekday hours of 7:00 AM–10:00 AM, 11:00 AM–2:00 PM, and 4:00 PM–7:00 PM.

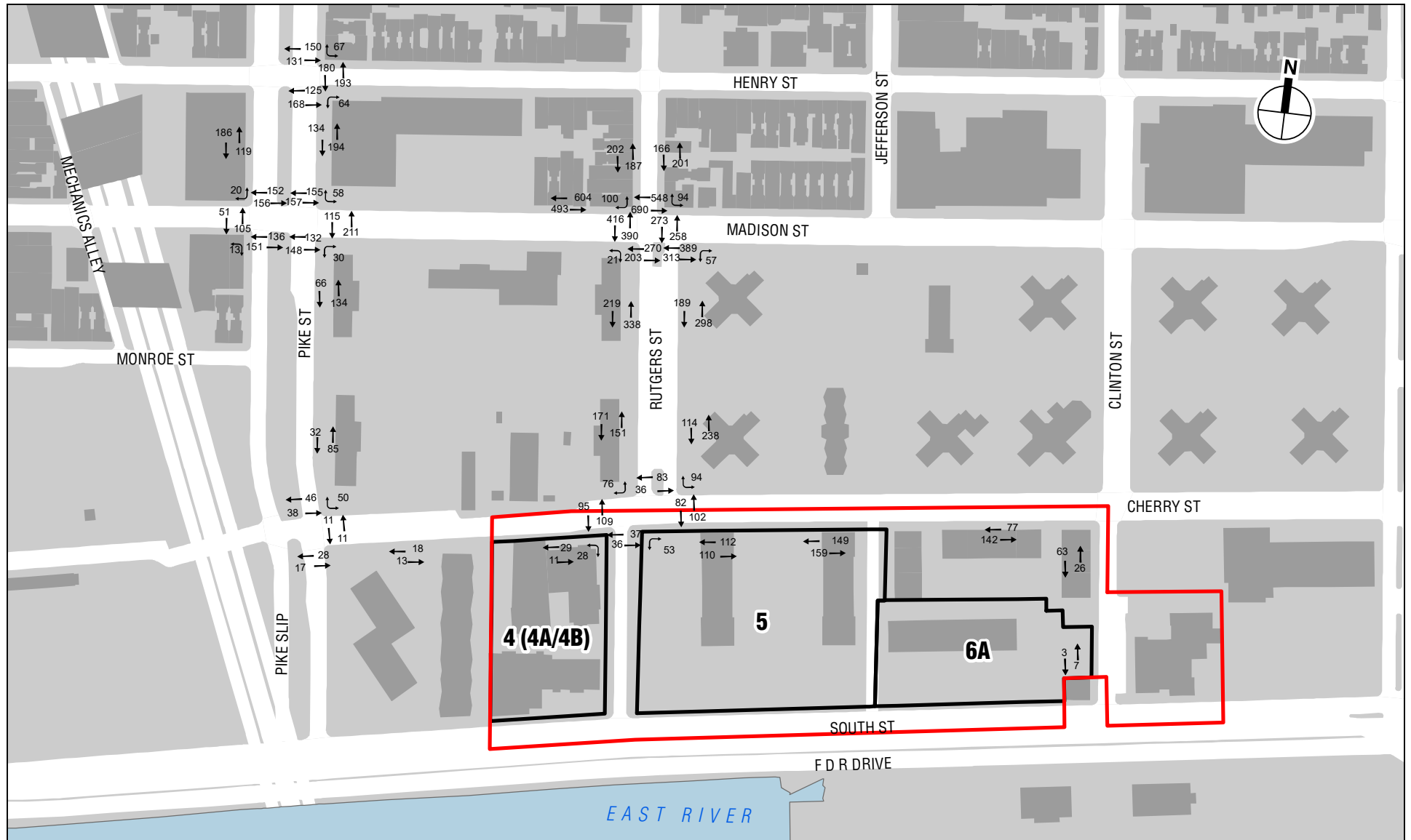
STREET-LEVEL PEDESTRIAN OPERATIONS

Peak hours were determined by comparing rolling hourly averages and the highest 15-minute volumes within the selected peak hours were selected for analysis. The existing peak hour pedestrian volumes are shown in **Figures 14-20 through 14-22**. A summary of the existing conditions pedestrian analysis results is presented in **Table 14-34**.

Table 14-34
Summary of Existing Pedestrian Analysis Results

| Level of Service | Analysis Peak Hours | | |
|--|---------------------|----------------|------------|
| | Weekday AM | Weekday Midday | Weekday PM |
| Sidewalks | | | |
| Sidewalks at LOS A/B/C | 18 | 18 | 18 |
| Sidewalks at LOS D | 0 | 0 | 0 |
| Sidewalks at LOS E | 0 | 0 | 0 |
| Sidewalks at LOS F | 0 | 0 | 0 |
| Total | 18 | 18 | 18 |
| Corners* | | | |
| Crosswalks at LOS A/B/C | 15 | 15 | 15 |
| Crosswalks at LOS D | 0 | 0 | 0 |
| Crosswalks at LOS E | 0 | 0 | 0 |
| Crosswalks at LOS F | 0 | 0 | 0 |
| Total | 15 | 15 | 15 |
| Crosswalks | | | |
| Corners at LOS A/B/C | 11 | 12 | 12 |
| Corners at LOS D | 1 | 0 | 0 |
| Corners at LOS E | 0 | 0 | 0 |
| Corners at LOS F | 0 | 0 | 0 |
| Total | 12 | 12 | 12 |
| Notes: LOS = Level-of-Service. * While there are 16 corners included in analysis, one of the corners were closed under existing conditions due to construction activities. | | | |

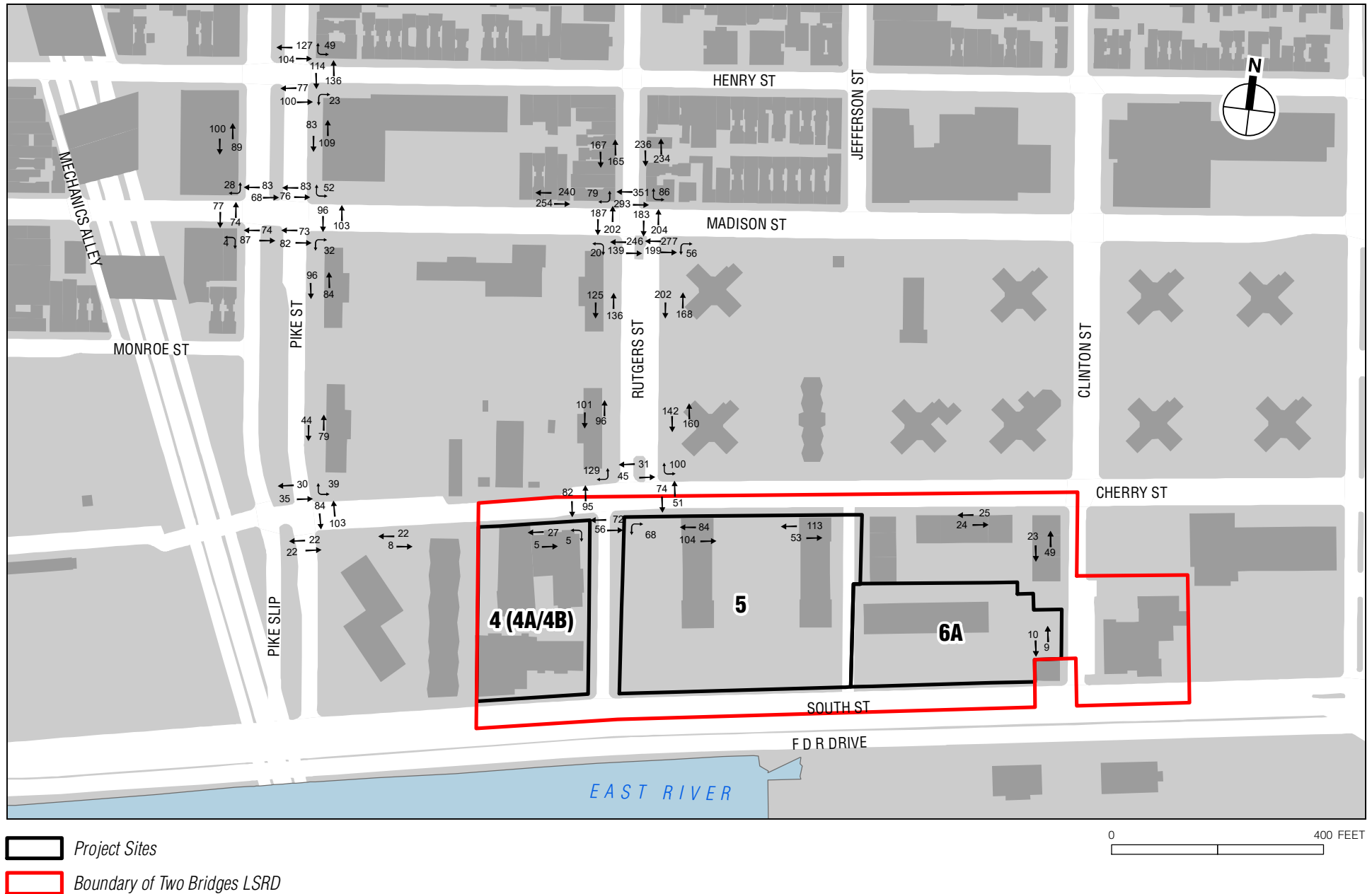
As shown in **Tables 14-35 through 14-37**, all sidewalk, corner reservoir, and crosswalk analysis locations currently operate at favorable LOS C or better, except for the North Crosswalk at Rutgers Street and Madison Street in AM peak hour (minimum of 31.5 SFP platoon flow for sidewalks; minimum of 19.5 SFP for corners and crosswalk).



- Project Sites
- Boundary of Two Bridges LSRD

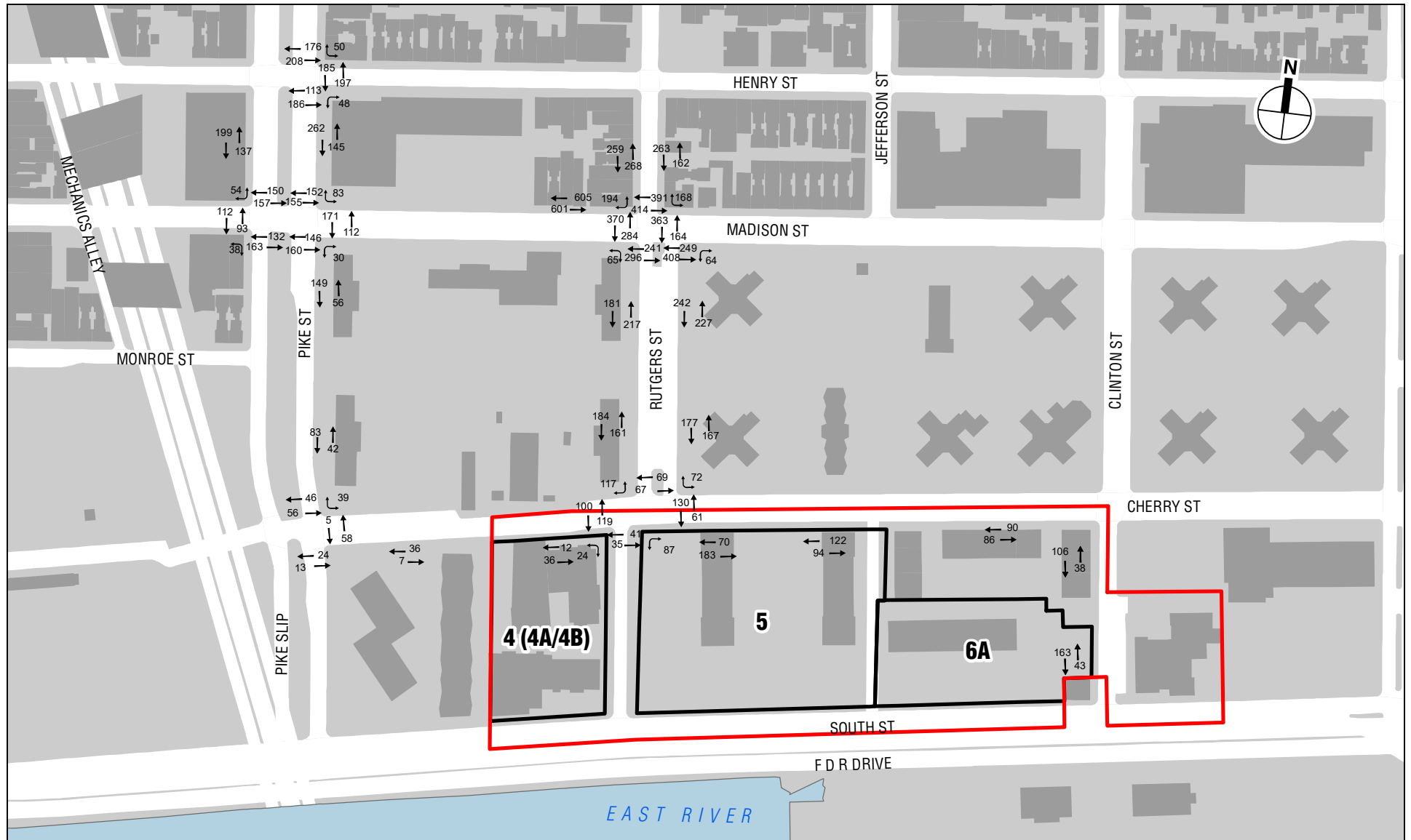
0 400 FEET

Existing Pedestrian Volumes
Weekday AM Peak Hour



Existing Pedestrian Volumes
Weekday Midday Peak Hour

Figure 14-21



Project Sites

Boundary of Two Bridges LSRD

Table 14-35
Existing Conditions: Sidewalk Analysis

| Location | Sidewalk | Effective Width (ft) | Two-way Peak Hour Volume | PHF | SFP | Platoon LOS |
|--|----------|----------------------|--------------------------|-----------------|-------------------------------|-------------|
| Weekday AM Peak Hour | | | | | | |
| Pike Street between Henry Street and Madison Street | East | 5.5 | 328 | <u>0.800.65</u> | <u>212.2172.3</u> | B |
| Pike Street between Henry Street and Madison Street | West | 4.5 | 305 | 0.86 | 200.7 | B |
| Rutgers Street between Madison Street and Henry Street | East | 3.5 | 367 | <u>0.800.75</u> | <u>120.4112.8</u> | B |
| Rutgers Street between Madison Street and Henry Street | West | 2.5 | 389 | <u>0.800.77</u> | <u>80.877.7</u> | C |
| Pike Street between Madison Street and Monroe Street | East | 6.5 | 200 | 0.81 | 416.9 | B |
| Rutgers Street between Madison Street and Monroe Street | West | 6.5 | 557 | <u>0.800.78</u> | <u>147.5143.8</u> | B |
| Madison Street between Rutgers Street and Pike Street | North | 5.0 | 1097 | <u>0.800.69</u> | <u>56.848.7</u> | C |
| Rutgers Street between Madison Street and Monroe Street | East | 9.0 | 487 | 0.91 | 266.2 | B |
| Pike Street between Monroe Street and Cherry Street | East | 6.5 | 117 | 0.81 | 712.7 | A |
| Cherry Street between Pike Street and Site 4 (4A/4B) Residential Entrance | South | 2.5 | 31 | <u>0.800.65</u> | <u>1021.9</u> <u>830.3</u> | A |
| Rutgers Street between Monroe Street and Cherry Street | East | 8.5 | 352 | 0.85 | 325.0 | B |
| Cherry Street between Frank T. Modica Way (Rutgers Street) and Site 5 Entrance | South | 8.5 | 222 | <u>0.800.62</u> | <u>485.1</u> <u>375.9</u> | B |
| Cherry Street between Frank T. Modica Way (Rutgers Street) and Site 4 (4A/4B) Residential Entrance | South | 6.5 | 40 | 0.83 | 2136.4 | A |
| Rutgers Street between Cherry Street and Monroe Street | West | 6.5 | 322 | 0.85 | 271.6 | B |
| Cherry Street Between Site 5 Entrance and Jefferson Street | South | 10.0 | 308 | <u>0.800.74</u> | <u>411.3</u> <u>380.4</u> | B |
| Clinton Street between Cherry Street and Plaza Entrance | West | 6.5 | 89 | <u>0.800.72</u> | <u>925.4832.9</u> | A |
| Cherry Street between Jefferson Street and Clinton Street | South | 5.5 | 219 | <u>0.800.62</u> | <u>348.1246.4</u> | B |
| Clinton Street between Plaza Entrance and South Street | West | 5.5 | 10 | <u>0.800.63</u> | <u>6969.65488.6</u> | A |
| Weekday Midday Peak Hour | | | | | | |
| Pike Street between Henry Street and Madison Street | East | 5.5 | 192 | 0.81 | 367.4 | B |
| Pike Street between Henry Street and Madison Street | West | 4.5 | 189 | 0.89 | 335.5 | B |
| Rutgers Street between Madison Street and Henry Street | East | 3.5 | 470 | 0.90 | 105.6 | B |
| Rutgers Street between Madison Street and Henry Street | West | 2.5 | 332 | 0.84 | 99.7 | B |
| Pike Street between Madison Street and Monroe Street | East | 6.5 | 180 | 0.87 | 497.5 | B |
| Rutgers Street between Madison Street and Monroe Street | West | 6.5 | 261 | 0.86 | 339.1 | B |
| Madison Street between Rutgers Street and Pike Street | North | 5.0 | 494 | 0.89 | 142.3 | B |
| Rutgers Street between Madison Street and Monroe Street | East | 9.0 | 370 | 0.88 | 338.9 | B |
| Pike Street between Monroe Street and Cherry Street | East | 6.5 | 123 | <u>0.800.73</u> | <u>669.6611.0</u> | A |
| Cherry Street between Pike Street and Site 4 (4A/4B) Residential Entrance | South | 2.5 | 30 | <u>0.800.68</u> | <u>1055.9</u> <u>897.5</u> | A |
| Rutgers Street between Monroe Street and Cherry Street | East | 8.5 | 302 | <u>0.800.77</u> | <u>356.5343.1</u> | B |
| Cherry Street between Frank T. Modica Way (Rutgers Street) and Site 5 Entrance | South | 8.5 | 188 | <u>0.800.67</u> | <u>572.8</u> <u>479.7</u> | AB |
| Cherry Street between Frank T. Modica Way (Rutgers Street) and Site 4 (4A/4B) Residential Entrance | South | 6.5 | 32 | 0.80 | 2574.0 | A |
| Rutgers Street between Cherry Street and Monroe Street | West | 6.5 | 197 | 0.93 | 485.9 | B |
| Cherry Street Between Site 5 Entrance and Jefferson Street | South | 10.0 | 166 | 0.94 | 896.9 | A |
| Clinton Street between Cherry Street and Plaza Entrance | West | 6.5 | 72 | <u>0.800.67</u> | <u>1444.0958.0</u> | A |
| Cherry Street between Jefferson Street and Clinton Street | South | 5.5 | 49 | <u>0.800.64</u> | <u>1422.31137.8</u> | A |
| Clinton Street between Plaza Entrance and South Street | West | 5.5 | 19 | <u>0.800.59</u> | <u>3668.22705.3</u> | A |
| Weekday PM Peak Hour | | | | | | |
| Pike Street between Henry Street and Madison Street | East | 5.5 | 407 | <u>0.800.76</u> | <u>170.9162.3</u> | B |
| Pike Street between Henry Street and Madison Street | West | 4.5 | 336 | <u>0.800.71</u> | <u>169.4150.3</u> | B |
| Rutgers Street between Madison Street and Henry Street | East | 3.5 | 425 | 0.93 | 120.9 | B |
| Rutgers Street between Madison Street and Henry Street | West | 2.5 | 527 | 0.83 | 61.5 | C |
| Pike Street between Madison Street and Monroe Street | East | 6.5 | 205 | 0.87 | 436.8 | B |
| Rutgers Street between Madison Street and Monroe Street | West | 6.5 | 398 | 0.93 | 240.3 | B |
| Madison Street between Rutgers Street and Pike Street | North | 5.0 | 1206 | 0.83 | 53.5 | C |
| Rutgers Street between Madison Street and Monroe Street | East | 9.0 | 469 | 0.88 | 267.3 | B |
| Pike Street between Monroe Street and Cherry Street | East | 6.5 | 125 | 0.92 | 757.7 | A |
| Cherry Street between Pike Street and Site 4 (4A/4B) Residential Entrance | South | 2.5 | 43 | <u>0.800.51</u> | <u>736.7469.6</u> | AB |
| Rutgers Street between Monroe Street and Cherry Street | East | 8.5 | 344 | 0.83 | 324.7 | B |

Table 14-35 (cont'd)
Existing Conditions: Sidewalk Analysis

| Location | Sidewalk | Effective Width (ft) | Two-way Peak Hour Volume | PHF | SFP | Platoon LOS |
|--|----------|----------------------|--------------------------|-----------------|---------------------|-------------|
| Weekday PM Peak Hour (cont'd) | | | | | | |
| Cherry Street between Frank T. Modica Way (Rutgers Street) and Site 5 Entrance | South | 8.5 | 253 | 0.80 | 425.9 | B |
| Cherry Street between Frank T. Modica Way (Rutgers Street) and Site 4 (4A/4B) Residential Entrance | South | 6.5 | 48 | <u>0.800.63</u> | <u>1716.01351.3</u> | A |
| Rutgers Street between Cherry Street and Monroe Street | West | 6.5 | 345 | 0.94 | 280.3 | B |
| Cherry Street Between Site 5 Entrance and Jefferson Street | South | 10.0 | 216 | 0.83 | 608.6 | A |
| Clinton Street between Cherry Street and Plaza Entrance | West | 6.5 | 144 | <u>0.800.61</u> | <u>571.9436.0</u> | AB |
| Cherry Street between Jefferson Street and Clinton Street | South | 5.5 | 176 | <u>0.800.70</u> | <u>395.9346.3</u> | B |
| Clinton Street between Plaza Entrance and South Street | West | 5.5 | 206 | <u>0.800.55</u> | <u>338.2232.4</u> | B |
| Note: SFP = square feet per pedestrian. | | | | | | |

Table 14-36
Existing Conditions: Corner Analysis

| Location | Corner | Weekday AM Peak Hour | | Weekday Midday Peak Hour | | Weekday PM Peak Hour | |
|--|-----------|----------------------|-----|--------------------------|-----|----------------------|-----|
| | | SFP | LOS | SFP | LOS | SFP | LOS |
| Pike Street and Henry Street | Northeast | <u>477.6171.3</u> | A | <u>262.1261.1</u> | A | <u>450.8149.8</u> | A |
| | Southeast | <u>475.8156.2</u> | A | 344.8 | A | <u>475.4167.5</u> | A |
| Pike Street and Madison Street (West) | Northwest | <u>206.8195.6</u> | A | <u>317.1352.9</u> | A | 190.9 | A |
| | Southwest | <u>227.2214.9</u> | A | <u>333.3352.6</u> | A | <u>489.9185.0</u> | A |
| Pike Street and Madison Street (East) | Northeast | <u>474.5163.7</u> | A | 317.5 | A | 186.3 | A |
| | Southeast | <u>225.0218.2</u> | A | 388.5 | A | 229.8 | A |
| Rutgers Street and Madison Street | Northwest | <u>49.949.6</u> | B | 119.8 | A | 78.1 | A |
| | Northeast | <u>51.850.1</u> | B | 102.6 | A | 75.9 | A |
| | Southwest | <u>97.697.3</u> | A | <u>181.8180.5</u> | A | <u>415.1114.8</u> | A |
| | Southeast | <u>169.5163.7</u> | A | <u>263.5262.7</u> | A | 214.7 | A |
| Pike Street and Cherry Street* | Northeast | <u>1079.0983.6</u> | A | <u>538.5381.5</u> | A | <u>770.7442.7</u> | A |
| | Southeast | N/A | N/A | N/A | N/A | N/A | N/A |
| Cherry Street and Rutgers Street | Northeast | <u>359.9278.8</u> | A | <u>466.9437.8</u> | A | <u>355.4341.4</u> | A |
| | Southwest | 307.2 | A | <u>300.4289.3</u> | A | <u>295.9288.0</u> | A |
| | Northwest | 952.8 | A | <u>869.5818.0</u> | A | <u>672.3568.2</u> | A |
| | Southeast | 941.7 | A | 584.4 | A | <u>695.9686.3</u> | A |
| Note: SFP = square foot per pedestrian | | | | | | | |
| * The southeast corner at this intersection was closed under existing conditions due to construction activities. | | | | | | | |

Table 14-37

Existing Conditions: Crosswalk Analysis

| Location | Crosswalk | Crosswalk Length (ft) | Crosswalk Width (ft) | Two-way Peak Hour Volume | SFP | LOS |
|---|----------------------------|-----------------------|----------------------|--------------------------|--------------------------|-----|
| Weekday AM Peak Hour | | | | | | |
| Pike Street and Henry Street | East | 30.5 | 14.5 | 373 | 87.6 | A |
| Pike Street and Madison Street (East) | East | 50.0 | 15.0 | 326 | 88.4 | A |
| Rutgers Street and Madison Street | North | 29.5 | 14.0 | 1238 | 23.3 | D |
| | East | 50.5 | 14.0 | 531 | 42.9 42.4 | B |
| | South (West of the Median) | 23.0 | 15.0 | 473 | 69.8 | A |
| | West | 50.0 | 15.0 | 806 | 31.6 | C |
| | South (East of the Median) | 23.0 | 15.0 | 702 | 45.5 | B |
| Pike Street and Cherry Street | East | 52.0 | 14.0 | 22 | 2265.4 1953.4 | A |
| Rutgers Street and Cherry Street | North | 71.0 | 16.0 | 119 | 278.8 | A |
| | East | 50.5 | 13.5 | 184 | 183.3 | A |
| | South | 21.5 | 14.5 | 73 | 323.6 | A |
| | West | 50.5 | 13.0 | 204 | 158.5 | A |
| Weekday Midday Peak Hour | | | | | | |
| Pike Street and Henry Street | East | 30.5 | 14.5 | 250 | 153.1 | A |
| Pike Street and Madison Street (East) | East | 50.0 | 15.0 | 199 | 151.2 | A |
| Rutgers Street and Madison Street | North | 29.5 | 14.0 | 644 | 51.7 | B |
| | East | 50.5 | 14.0 | 387 | 65.3 | A |
| | South (West of the Median) | 23.0 | 15.0 | 385 | 95.9 | A |
| | West | 50.0 | 15.0 | 389 | 72.6 | A |
| | South (East of the Median) | 23.0 | 15.0 | 476 | 74.9 | A |
| Pike Street and Cherry Street | East | 52.0 | 14.0 | 187 | 263.2 166.5 | A |
| Rutgers Street and Cherry Street | North | 71.0 | 16.0 | 76 | 465.7 | A |
| | East | 50.5 | 13.5 | 125 | 249.2 236.6 | A |
| | South | 21.5 | 14.5 | 128 | 175.7 | A |
| | West | 50.5 | 13.0 | 177 | 191.6 | A |
| Weekday PM Peak Hour | | | | | | |
| Pike Street and Henry Street | East | 30.5 | 14.5 | 382 | 82.6 | A |
| Pike Street and Madison Street (East) | East | 50.0 | 15.0 | 283 | 98.9 | A |
| Rutgers Street and Madison Street | North | 29.5 | 14.0 | 805 | 41.7 | B |
| | East | 50.5 | 14.0 | 527 | 49.3 | B |
| | South (West of the Median) | 23.0 | 15.0 | 537 | 71.7 | A |
| | West | 50.0 | 15.0 | 654 | 43.6 | B |
| | South (East of the Median) | 23.0 | 15.0 | 657 | 58.1 | B |
| Pike Street and Cherry Street | East | 52.0 | 14.0 | 63 | 786.0 350.3 | A |
| Rutgers Street and Cherry Street | North | 71.0 | 16.0 | 136 | 228.8 217.3 | A |
| | East | 50.5 | 13.5 | 191 | 182.3 | A |
| | South | 21.5 | 14.5 | 76 | 310.6 | A |
| | West | 50.5 | 13.0 | 219 | 150.6 | A |
| Note: SFP = square feet per pedestrian | | | | | | |

THE FUTURE WITHOUT THE PROPOSED PROJECTS

Future 2021 No Action condition pedestrian volumes were estimated by increasing existing pedestrian levels to reflect expected growth in overall travel through and within the study area. As per CEQR guidelines, an annual background growth rate of 0.25 percent was assumed for the proposed projects' anticipated build year of 2021. An additional three percent of pedestrian volume growth to account for small- to moderate-sized No Build projects within a ½ mile of the project sites, and trips generated by two discrete No Build projects in the area were also incorporated into the future No Action pedestrian volumes. The 2021 No Action pedestrian volumes for the weekday AM, midday, and PM peak hours are presented in **Figures 14-23 through 14-25**.

STREET-LEVEL PEDESTRIAN OPERATIONS

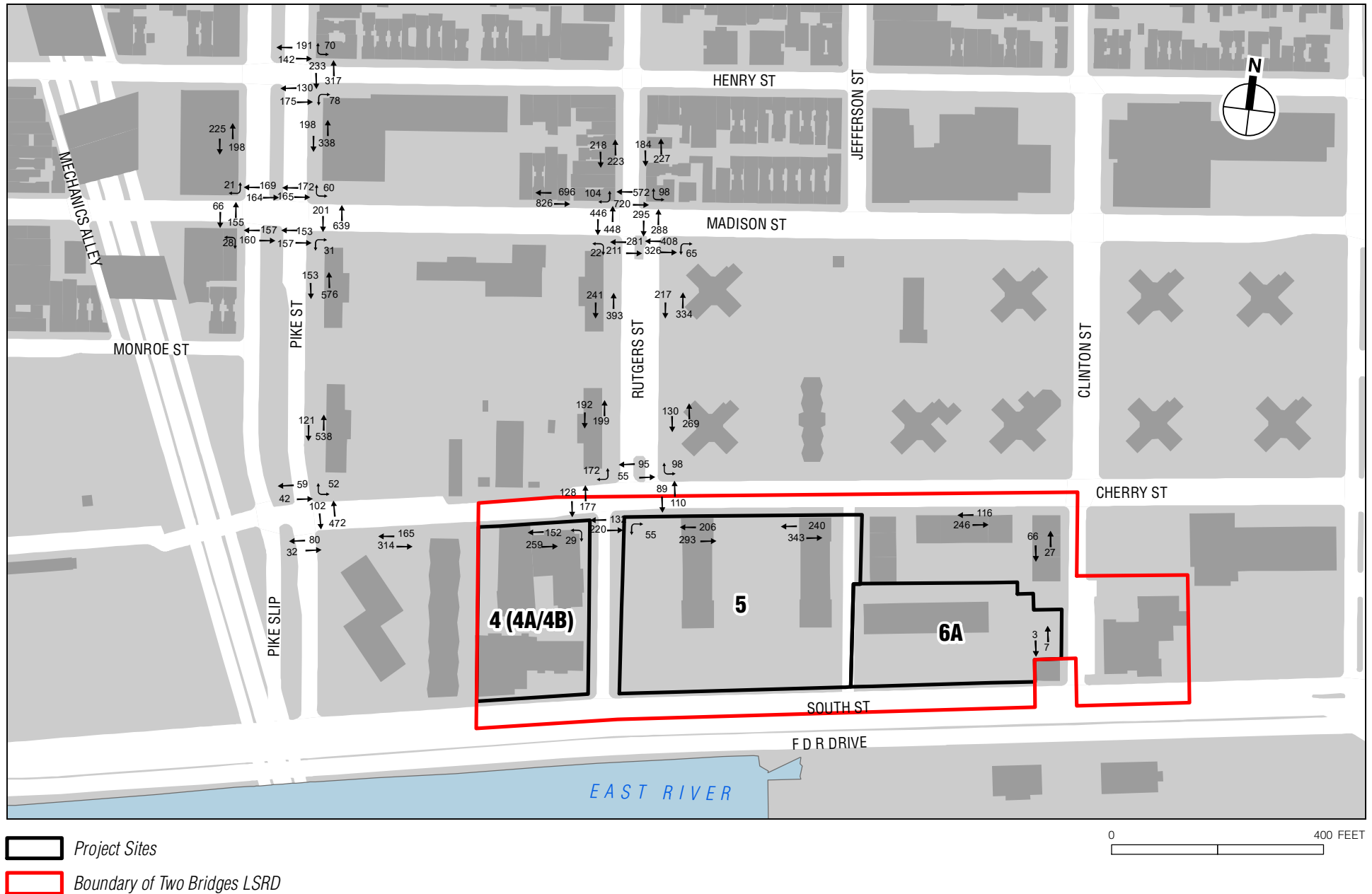
A summary of the 2021 No Action condition pedestrian analysis results is presented in **Table 14-38**.

Table 14-38
Summary of 2021 No Action Pedestrian Analysis Results

| Level of Service | Analysis Peak Hours | | |
|-------------------------|---------------------|----------------|------------|
| | Weekday AM | Weekday Midday | Weekday PM |
| Sidewalks | | | |
| Sidewalks at LOS A/B/C | 1817 | 18 | 17 |
| Sidewalks at LOS D | 01 | 0 | 1 |
| Sidewalks at LOS E | 0 | 0 | 0 |
| Sidewalks at LOS F | 0 | 0 | 0 |
| Total | 18 | 18 | 18 |
| Corners | | | |
| Crosswalks at LOS A/B/C | 16 | 16 | 16 |
| Crosswalks at LOS D | 0 | 0 | 0 |
| Crosswalks at LOS E | 0 | 0 | 0 |
| Crosswalks at LOS F | 0 | 0 | 0 |
| Total | 16 | 16 | 16 |
| Crosswalks | | | |
| Corners at LOS A/B/C | 11 | 11 | 12 |
| Corners at LOS D | 1 | 1 | 0 |
| Corners at LOS E | 0 | 0 | 0 |
| Corners at LOS F | 0 | 0 | 0 |
| Total | 12 | 12 | 12 |

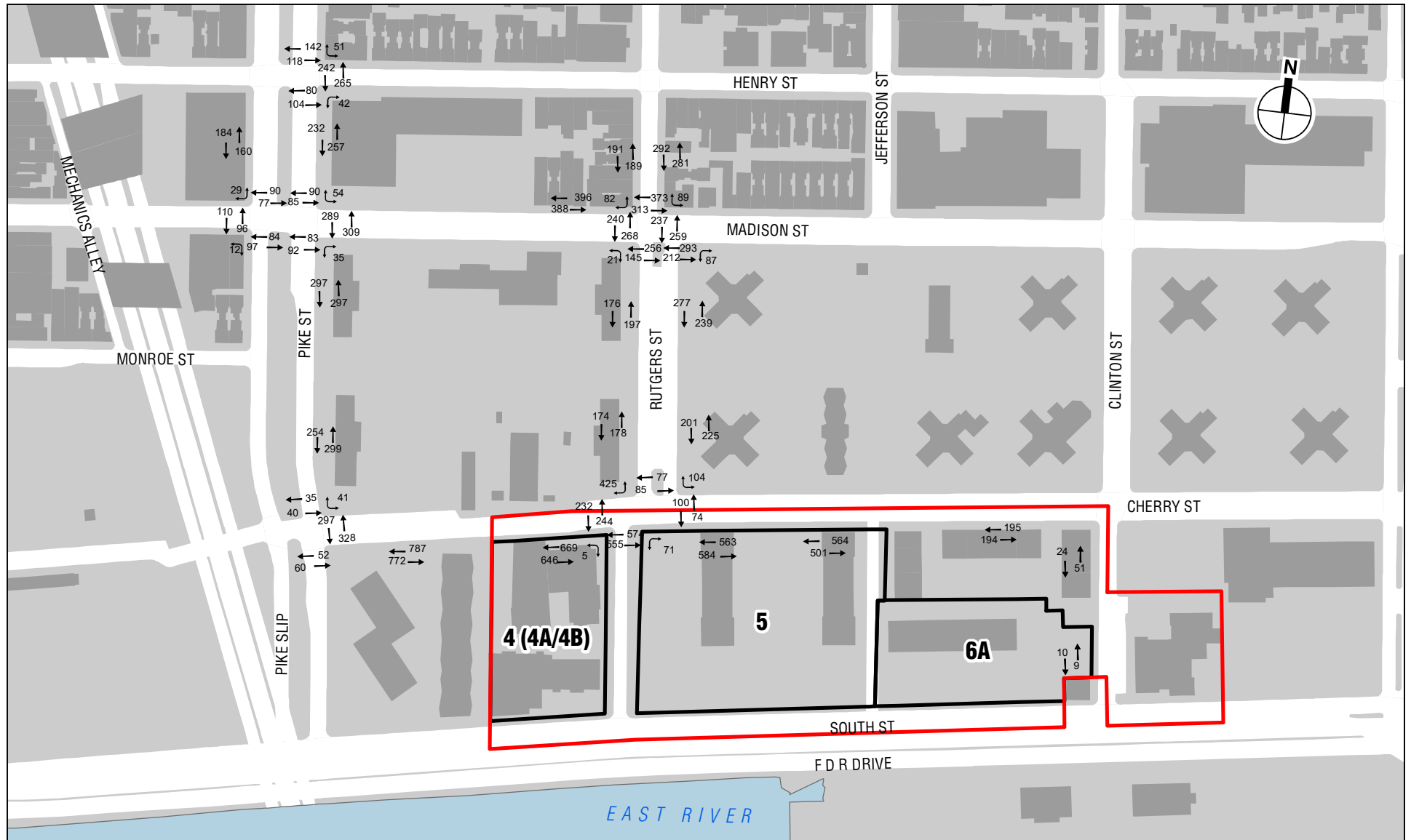
Note: LOS = Level-of-Service

As shown in **Tables 14-39 through 14-41**, all sidewalk, corner reservoir, and crosswalk analysis locations will operate at acceptable mid-LOS D or better service levels (31.5 SFP platoon flows for sidewalks; minimum of 19.5 SFP for corners and crosswalks) or will operate at the same LOS as under existing conditions, except for the south crosswalk at Cherry Street and Rutgers Street during the weekday midday peak hour.



2021 No Action Pedestrian Volumes
Weekday AM Peak Hour

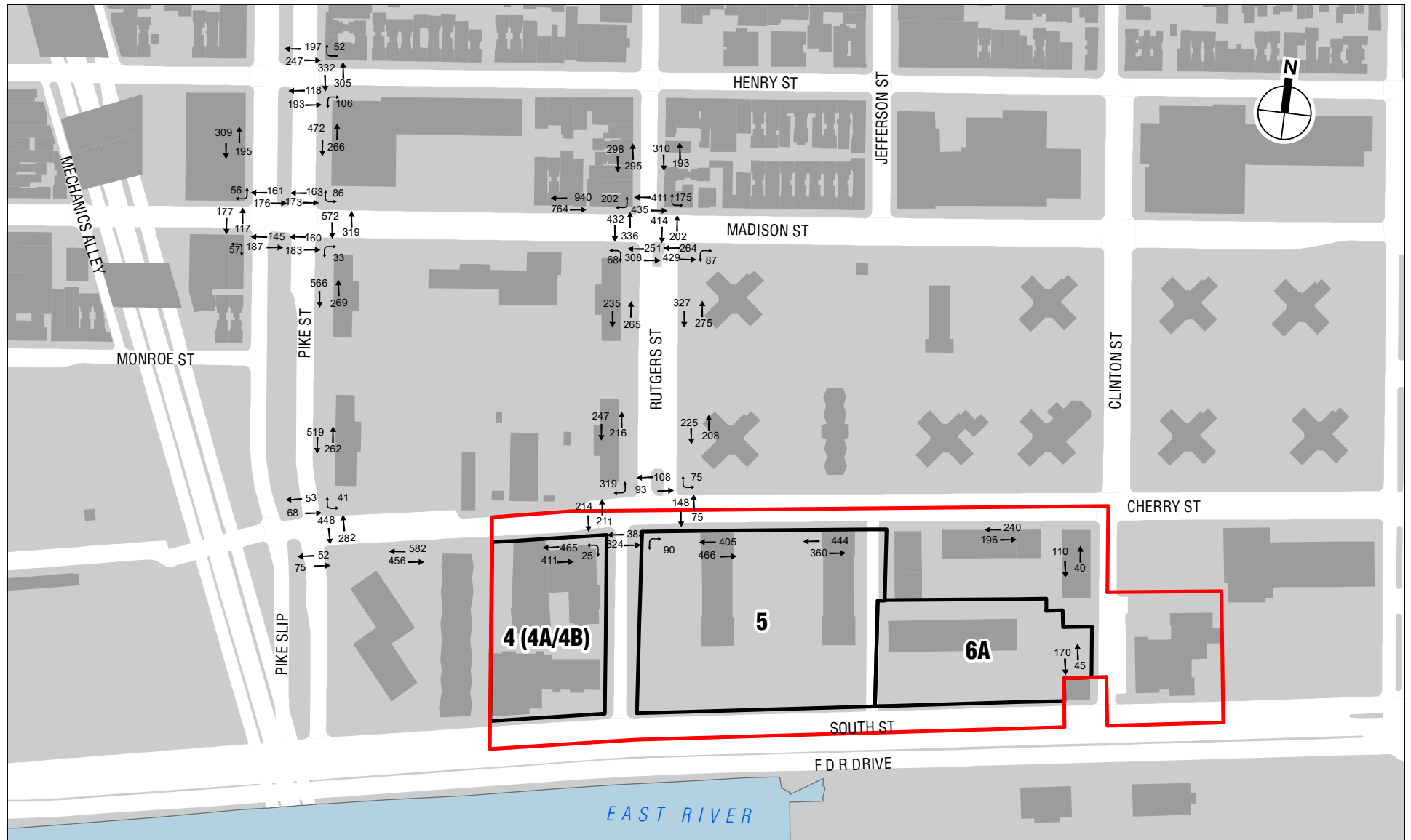
Figure 14-23



- Project Sites
- Boundary of Two Bridges LSRD

0 400 FEET

2021 No Action Pedestrian Volumes
Weekday Midday Peak Hour
Figure 14-24



- Project Sites
- Boundary of Two Bridges LSRD

Table 14-39

2021 No Action Condition: Sidewalk Analysis

| Location | Sidewalk | Effective Width (ft) | Two-way Peak Hour Volume | PHF | SFP | Platoon LOS |
|--|----------|----------------------|--------------------------|---------------------|-------------------------|-------------|
| Weekday AM Peak Hour | | | | | | |
| Pike Street between Henry Street and Madison Street | East | 5.5 | 536 | <u>0.80</u> 0.70 | <u>129.6</u> 113.3 | B |
| Pike Street between Henry Street and Madison Street | West | 4.5 | 423 | 0.86 | 144.5 | B |
| Rutgers Street between Madison Street and Henry Street | East | 3.5 | 411 | <u>0.80</u> 0.75 | <u>107.4</u> 100.6 | B |
| Rutgers Street between Madison Street and Henry Street | West | 2.5 | 441 | <u>0.80</u> 0.77 | <u>71.4</u> 68.4 | C |
| Pike Street between Madison Street and Monroe Street | East | 6.5 | 729 | 0.81 | 113.9 | B |
| Rutgers Street between Madison Street and Monroe Street | West | 6.5 | 634 | <u>0.80</u> 0.78 | <u>129.5</u> 126.2 | B |
| Madison Street between Rutgers Street and Pike Street | North | 5.0 | 1522 | <u>0.80</u> 0.71 | <u>40.3</u> 35.5 | CD |
| Rutgers Street between Madison Street and Monroe Street | East | 9.0 | 551 | 0.91 | 235.2 | B |
| Pike Street between Monroe Street and Cherry Street | East | 6.5 | 659 | 0.81 | 126.1 | B |
| Cherry Street between Pike Street and Site 4 (4A/4B) Residential Entrance | South | 6.5 | 479 | <u>0.80</u> 0.79 | <u>171.6</u> 169.5 | B |
| Rutgers Street between Monroe Street and Cherry Street | East | 8.5 | 399 | 0.85 | 286.6 | B |
| Cherry Street between Frank T. Modica Way (Rutgers Street) and Site 5 Entrance | South | 8.5 | 499 | <u>0.80</u> 0.71 | <u>215.6</u> 191.3 | B |
| Cherry Street between Frank T. Modica Way (Rutgers Street) and Site 4 (4A/4B) Residential Entrance | South | 6.5 | 411 | 0.83 | 207.7 | B |
| Rutgers Street between Cherry Street and Monroe Street | West | 6.5 | 391 | 0.85 | 223.6 | B |
| Cherry Street Between Site 5 Entrance and Jefferson Street | South | 10.0 | 583 | <u>0.80</u> 0.77 | <u>217.12</u> 108.9 | B |
| Clinton Street between Cherry Street and Plaza Entrance | West | 6.5 | 93 | <u>0.80</u> 0.72 | <u>885.6</u> 797.0 | A |
| Cherry Street between Jefferson Street and Clinton Street | South | 5.5 | 362 | <u>0.80</u> 0.68 | <u>192.2</u> 163.3 | B |
| Clinton Street between Plaza Entrance and South Street | West | 5.5 | 10 | <u>0.80</u> 0.63 | <u>6969.6</u> 5488.6 | A |
| Weekday Midday Peak Hour | | | | | | |
| Pike Street between Henry Street and Madison Street | East | 5.5 | 489 | 0.81 | 143.9 | B |
| Pike Street between Henry Street and Madison Street | West | 4.5 | 344 | 0.89 | 184.1 | B |
| Rutgers Street between Madison Street and Henry Street | East | 3.5 | 573 | 0.90 | 86.5 | C |
| Rutgers Street between Madison Street and Henry Street | West | 2.5 | 380 | 0.84 | 86.9 | C |
| Pike Street between Madison Street and Monroe Street | East | 6.5 | 594 | 0.87 | 150.4 | B |
| Rutgers Street between Madison Street and Monroe Street | West | 6.5 | 373 | 0.86 | 237.2 | B |
| Madison Street between Rutgers Street and Pike Street | North | 5.0 | 784 | 0.89 | 89.3 | C |
| Rutgers Street between Madison Street and Monroe Street | East | 9.0 | 516 | 0.88 | 242.9 | B |
| Pike Street between Monroe Street and Cherry Street | East | 6.5 | 553 | <u>0.80</u> 0.78 | <u>148.6</u> 144.8 | B |
| Cherry Street between Pike Street and Site 4 (4A/4B) Residential Entrance | South | 6.5 | 1559 | 0.80 | 51.8 | C |
| Rutgers Street between Monroe Street and Cherry Street | East | 8.5 | 426 | <u>0.80</u> 0.78 | <u>252.6</u> 246.3 | B |
| Cherry Street between Frank T. Modica Way (Rutgers Street) and Site 5 Entrance | South | 8.5 | 1147 | <u>0.80</u> 0.77 | <u>93.3</u> 89.8 | BC |
| Cherry Street between Frank T. Modica Way (Rutgers Street) and Site 4 (4A/4B) Residential Entrance | South | 6.5 | 1315 | 0.80 | 61.8 | C |
| Rutgers Street between Cherry Street and Monroe Street | West | 6.5 | 352 | 0.93 | 271.8 | B |
| Cherry Street Between Site 5 Entrance and Jefferson Street | South | 10.0 | 1065 | 0.94 | 139.4 | B |
| Clinton Street between Cherry Street and Plaza Entrance | West | 6.5 | 75 | <u>0.80</u> 0.67 | <u>1098.2</u> 919.7 | A |

Table 14-39 (cont'd)
2021 No Action Condition: Sidewalk Analysis

| Location | Sidewalk | Effective Width (ft) | Two-way Peak Hour Volume | PHF | SFP | Platoon LOS |
|--|----------|----------------------|--------------------------|--------------|------------------|-------------|
| Weekday PM Peak Hour | | | | | | |
| Cherry Street between Jefferson Street and Clinton Street | South | 5.5 | 389 | 0.80 0.77 | 178.9 172.1 | B |
| Clinton Street between Plaza Entrance and South Street | West | 5.5 | 19 | 0.80 0.59 | 3668.2 2705.3 | A |
| Pike Street between Henry Street and Madison Street | East | 5.5 | 738 | 0.80 0.78 | 93.9 91.5 | B |
| Pike Street between Henry Street and Madison Street | West | 4.5 | 504 | 0.80 0.75 | 112.7 105.6 | B |
| Rutgers Street between Madison Street and Henry Street | East | 3.5 | 503 | 0.93 | 102.0 | B |
| Rutgers Street between Madison Street and Henry Street | West | 2.5 | 593 | 0.83 | 54.4 | C |
| Pike Street between Madison Street and Monroe Street | East | 6.5 | 835 | 0.87 | 106.8 | B |
| Rutgers Street between Madison Street and Monroe Street | West | 6.5 | 500 | 0.93 | 191.2 | B |
| Madison Street between Rutgers Street and Pike Street | North | 5.0 | 1704 | 0.83 | 37.2 | D |
| Rutgers Street between Madison Street and Monroe Street | East | 9.0 | 602 | 0.88 | 208.1 | B |
| Pike Street between Monroe Street and Cherry Street | East | 6.5 | 781 | 0.92 | 120.8 | B |
| Cherry Street between Pike Street and Site 4 (4A/4B) Residential Entrance | South | 6.5 | 1038 | 0.80 0.78 | 78.7 76.7 | C |
| Rutgers Street between Monroe Street and Cherry Street | East | 8.5 | 433 | 0.83 | 257.9 | B |
| Cherry Street between Frank T. Modica Way (Rutgers Street) and Site 5 Entrance | South | 8.5 | 871 | 0.80 | 123.3 | B |
| Cherry Street between Frank T. Modica Way (Rutgers Street) and Site 4 (4A/4B) Residential Entrance | South | 6.5 | 876 | 0.80 0.79 | 93.4 92.3 | B |
| Rutgers Street between Cherry Street and Monroe Street | West | 6.5 | 463 | 0.94 | 208.8 | B |
| Cherry Street Between Site 5 Entrance and Jefferson Street | South | 10.0 | 804 | 0.83 | 163.2 | B |
| Clinton Street between Cherry Street and Plaza Entrance | West | 6.5 | 150 | 0.80 0.61 | 549.0 418.6 | AB |
| Cherry Street between Jefferson Street and Clinton Street | South | 5.5 | 436 | 0.80 0.75 | 159.5 149.5 | B |
| Clinton Street between Plaza Entrance and South Street | West | 5.5 | 215 | 0.80 0.55 | 324.0 222.6 | B |
| Note: SFP = square feet per pedestrian | | | | | | |

Table 14-40

2021 No Action Condition: Corner Analysis

| Location | Corner | Weekday AM Peak Hour | | Weekday Midday Peak Hour | | Weekday PM Peak Hour | |
|---|-----------|----------------------|-----|--------------------------|-----|----------------------|-----|
| | | SFP | LOS | SFP | LOS | SFP | LOS |
| Pike Street and Henry Street | Northeast | <u>431.2127.5</u> | A | <u>468.5168.1</u> | A | <u>404.8104.2</u> | A |
| | Southeast | <u>434.5121.7</u> | A | 206.6 | A | <u>418.8114.8</u> | A |
| Pike Street and Madison Street (West) | Northwest | <u>472.7164.0</u> | A | <u>252.6282.0</u> | A | <u>452.3152.3</u> | A |
| | Southwest | <u>478.4169.6</u> | A | <u>259.8277.4</u> | A | <u>446.4143.2</u> | A |
| Pike Street and Madison Street (East) | Northeast | <u>97.693.8</u> | A | 151.6 | A | 83.6 | A |
| | Southeast | <u>409.3107.4</u> | A | 177.1 | A | 104.5 | A |
| Rutgers Street and Madison Street | Northwest | <u>46.145.8</u> | B | 102.8 | A | 69.8 | A |
| | Northeast | <u>48.346.8</u> | B | 88.3 | A | 68.3 | A |
| | Southwest | <u>88.888.5</u> | A | <u>453.0152.0</u> | A | <u>402.2102.0</u> | A |
| | Southeast | <u>460.5158.5</u> | A | <u>235.5235.0</u> | A | 197.8 | A |
| Pike Street and Cherry Street | Northeast | <u>217.6214.3</u> | A | <u>207.0176.6</u> | A | <u>468.7142.3</u> | A |
| | Southeast | <u>465.8124.8</u> | A | <u>454.3116.2</u> | A | <u>433.595.6</u> | A |
| Cherry Street and Rutgers Street | Northeast | <u>318.7251.0</u> | A | <u>319.2304.5</u> | A | <u>279.8272.9</u> | A |
| | Southwest | 123.6 | A | <u>43.843.5</u> | B | <u>69.669.1</u> | A |
| | Northwest | 579.9 | A | <u>298.5292.9</u> | A | <u>325.6302.1</u> | A |
| | Southeast | 279.6 | A | 79.9 | A | <u>430.6130.2</u> | A |
| Note: SFP = square foot per pedestrian | | | | | | | |

Table 14-41
2021 No Action Condition: Crosswalk Analysis

| Location | Crosswalk | Crosswalk Length (ft) | Crosswalk Width (ft) | Two-way Peak Hour Volume | SFP | LOS |
|---|----------------------------|-----------------------|----------------------|--------------------------|------------------------|-----|
| Weekday AM Peak Hour | | | | | | |
| Pike Street and Henry Street | East | 30.5 | 14.5 | 550 | 57.8 | B |
| Pike Street and Madison Street (East) | East | 50.0 | 15.0 | 840 | 32.0 | C |
| Rutgers Street and Madison Street | North | 29.5 | 14.0 | 1292 | 22.1 | D |
| | East | 50.5 | 14.0 | 583 | 38.9 38.3 | C |
| | South (West of the Median) | 23.0 | 15.0 | 492 | 67.0 | A |
| | West | 50.0 | 15.0 | 894 | 28.2 | C |
| | South (East of the Median) | 23.0 | 15.0 | 734 | 43.3 | B |
| Pike Street and Cherry Street | East | 52.0 | 14.0 | 574 | 82.0 | A |
| Rutgers Street and Cherry Street | North | 71.0 | 16.0 | 150 | 220.6 | A |
| | East | 50.5 | 13.5 | 199 | 169.3 | A |
| | South | 21.5 | 14.5 | 352 | 63.4 | A |
| | West | 50.5 | 13.0 | 305 | 104.8 | A |
| Weekday Midday Peak Hour | | | | | | |
| Pike Street and Henry Street | East | 30.5 | 14.5 | 507 | 73.1 | A |
| Pike Street and Madison Street (East) | East | 50.0 | 15.0 | 598 | 48.4 | B |
| Rutgers Street and Madison Street | North | 29.5 | 14.0 | 686 | 48.1 | B |
| | East | 50.5 | 14.0 | 496 | 50.3 | B |
| | South (West of the Median) | 23.0 | 15.0 | 401 | 91.8 | A |
| | West | 50.0 | 15.0 | 508 | 55.0 | B |
| | South (East of the Median) | 23.0 | 15.0 | 505 | 70.3 | A |
| Pike Street and Cherry Street | East | 52.0 | 14.0 | 625 | 76.3 64.3 | A |
| Rutgers Street and Cherry Street | North | 71.0 | 16.0 | 162 | 217.0 | A |
| | East | 50.5 | 13.5 | 174 | 178.1 171.3 | A |
| | South | 21.5 | 14.5 | 1129 | 16.6 | D |
| | West | 50.5 | 13.0 | 476 | 69.3 | A |
| Weekday PM Peak Hour | | | | | | |
| Pike Street and Henry Street | East | 30.5 | 14.5 | 637 | 47.8 | B |
| Pike Street and Madison Street (East) | East | 50.0 | 15.0 | 891 | 29.5 | C |
| Rutgers Street and Madison Street | North | 29.5 | 14.0 | 846 | 39.3 | C |
| | East | 50.5 | 14.0 | 616 | 41.8 | B |
| | South (West of the Median) | 23.0 | 15.0 | 559 | 68.7 | A |
| | West | 50.0 | 15.0 | 768 | 36.8 | C |
| | South (East of the Median) | 23.0 | 15.0 | 693 | 54.9 | B |
| Pike Street and Cherry Street | East | 52.0 | 14.0 | 730 | 64.7 57.8 | AB |
| Rutgers Street and Cherry Street | North | 71.0 | 16.0 | 201 | 153.9 151.2 | A |
| | East | 50.5 | 13.5 | 223 | 155.7 | A |
| | South | 21.5 | 14.5 | 712 | 29.5 | C |
| | West | 50.5 | 13.0 | 425 | 76.1 | A |
| Note: SFP = square feet per pedestrian | | | | | | |

THE FUTURE WITH THE PROPOSED PROJECTS

Project-generated pedestrian volumes were assigned to the pedestrian network considering current land uses in the area, population distribution, nearby parking locations, available transit services, and surrounding pedestrian facilities. The hourly incremental pedestrian volumes presented above in **Figures 14-26 through 14-28**, were added to the projected 2021 No Action volumes to generate the 2021 With Action pedestrian volumes for analysis (see **Figures 14-26 through 14-28**).

STREET-LEVEL PEDESTRIAN OPERATIONS AND SIGNIFICANT ADVERSE IMPACTS

A summary of the 2021 With Action condition pedestrian analysis results is presented in **Table 14-42**. Details on SFP and level-of-service are presented in **Tables 14-43 to 14-45**. Based on the *CEQR Technical Manual* sliding scale impact thresholds, significant adverse pedestrian impacts, as detailed below, were identified for one sidewalk during the weekday PM peak hour, one crosswalk during the weekday AM and midday peak hours, and three crosswalks during the weekday PM peak hour. Potential measures that can be implemented to mitigate these significant adverse pedestrian impacts are discussed in Chapter 21, "Mitigation."

Sidewalks

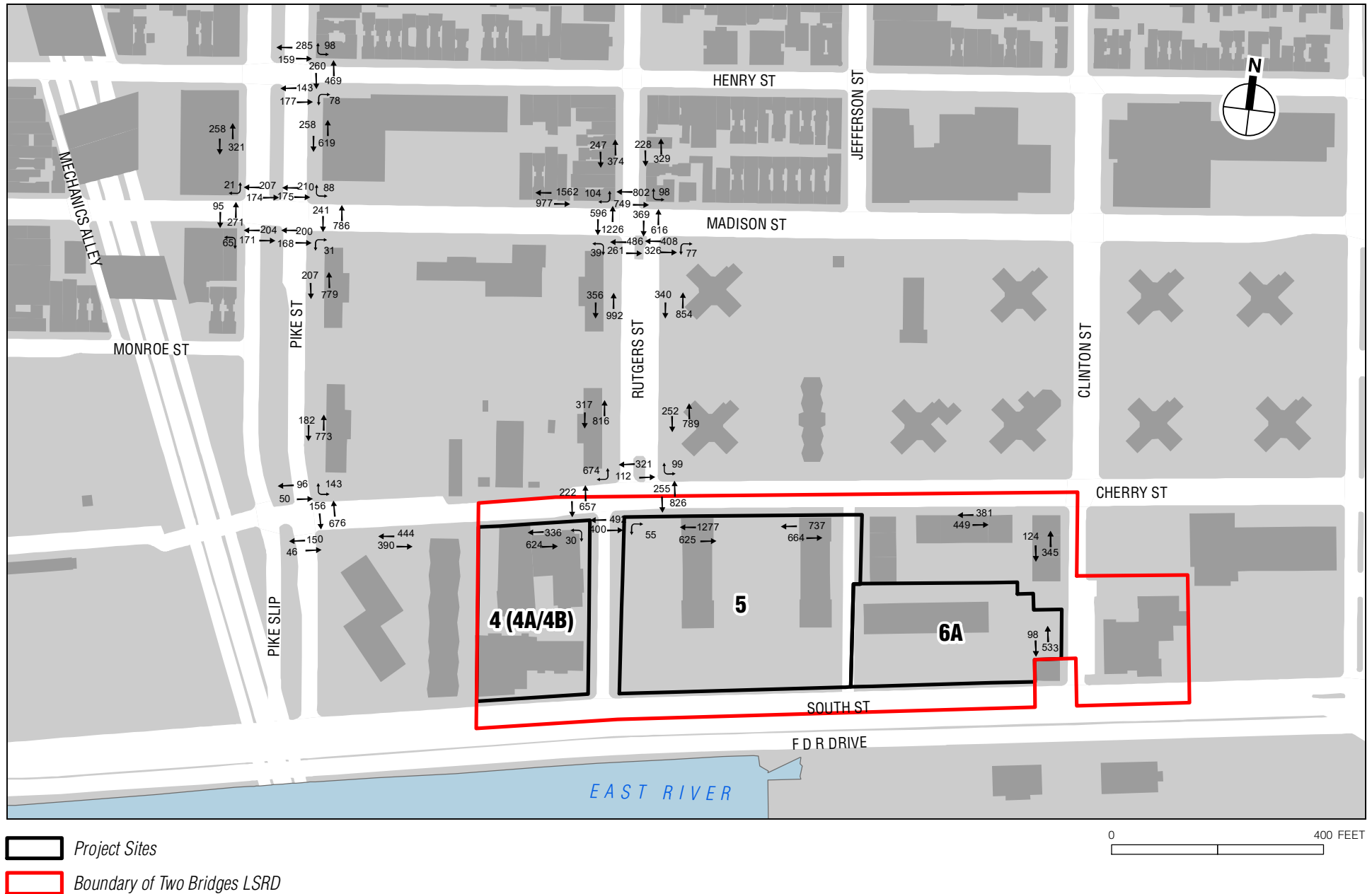
- The north sidewalk of Madison Street between Rutgers Street and Pike Street would deteriorate from LOS ~~C-D~~ with ~~40.335.5~~ SFP and ~~LOS D~~ with ~~37.2~~ SFP to LOS E with ~~22.822.1~~ SFP and 21.7 SFP during the weekday AM and PM peak hour, respectively. These degradations in pedestrian operations constitute significant adverse impacts.

Crosswalks

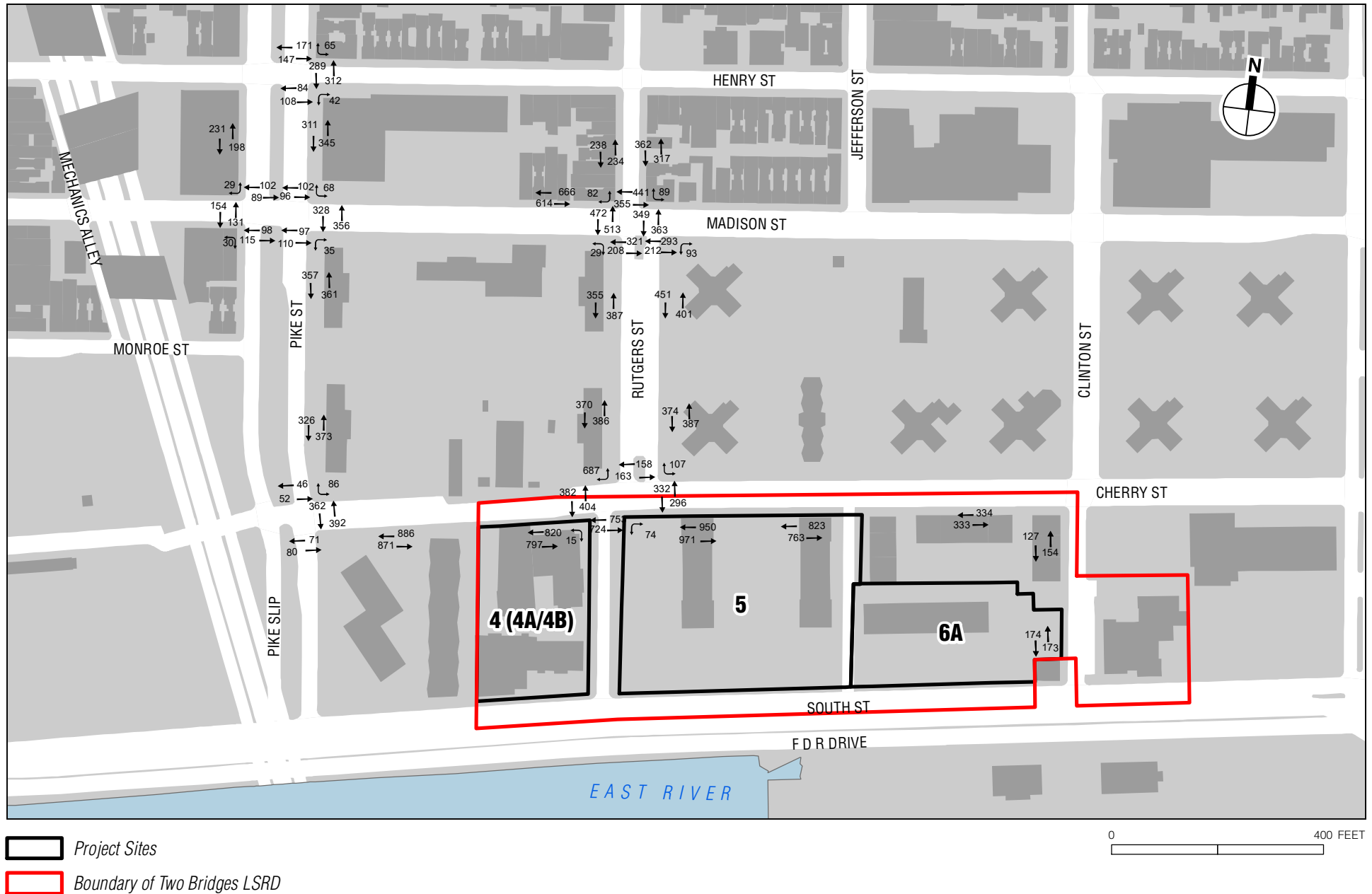
- The north crosswalk of Madison Street and Rutgers Street would deteriorate within LOS D from 22.1 SFP to 17.9 SFP during the weekday AM peak hour. This degradation in pedestrian operations constitutes a significant adverse impact.

Table 14-42
Summary of 2021 With Action Pedestrian Analysis Results

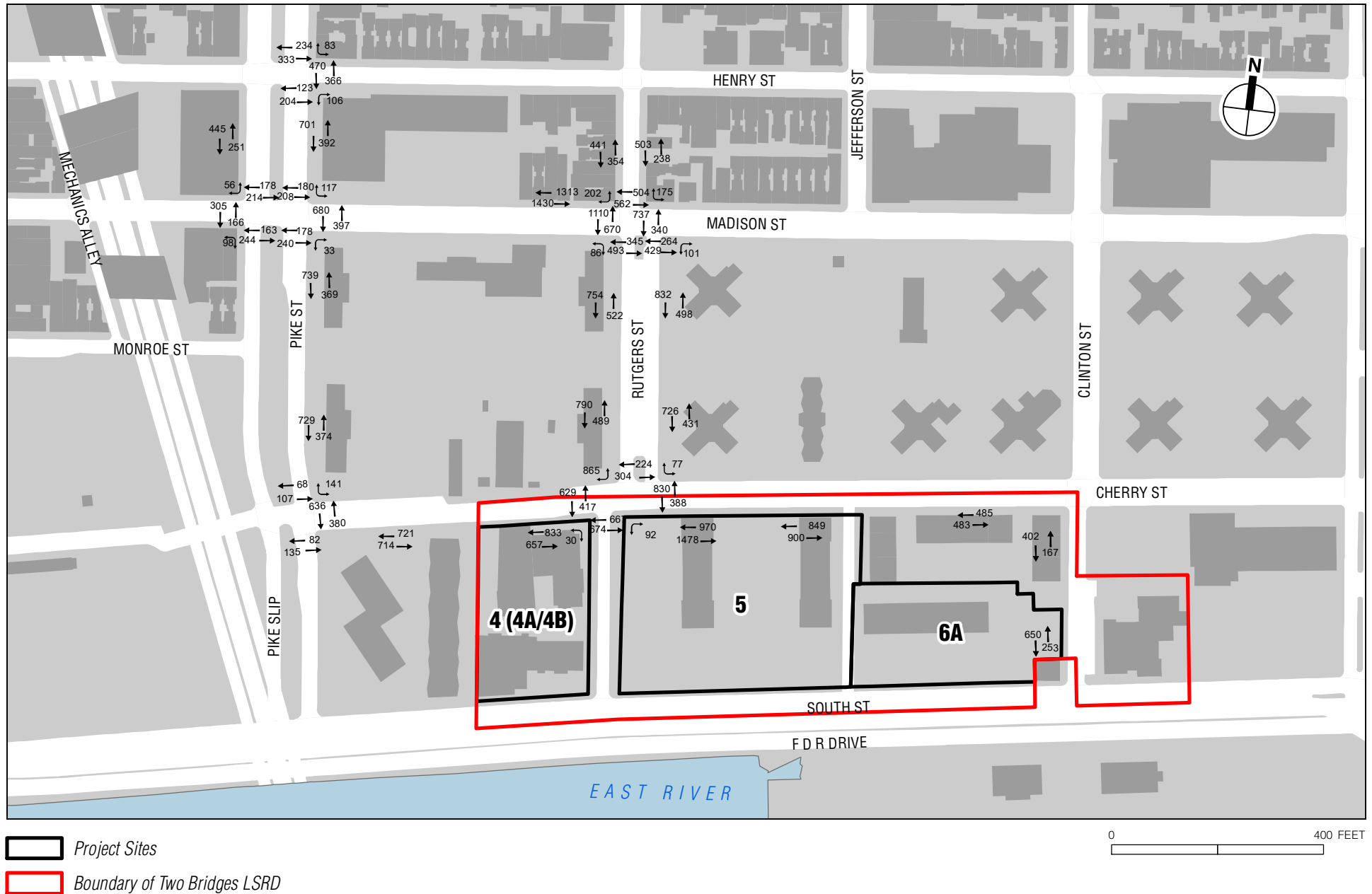
| Level of Service | Analysis Peak Hours | | |
|-------------------------------------|---------------------|----------------|------------|
| | Weekday AM | Weekday Midday | Weekday PM |
| Sidewalks | | | |
| Sidewalks at LOS A/B/C | 17 | 18 | 17 |
| Sidewalks at LOS D | 0 | 0 | 0 |
| Sidewalks at LOS E | 1 | 0 | 1 |
| Sidewalks at LOS F | 0 | 0 | 0 |
| Total | 18 | 18 | 18 |
| Corners | | | |
| Crosswalks at LOS A/B/C | 16 | 16 | 16 |
| Crosswalks at LOS D | 0 | 0 | 0 |
| Crosswalks at LOS E | 0 | 0 | 0 |
| Crosswalks at LOS F | 0 | 0 | 0 |
| Total | 16 | 16 | 16 |
| Crosswalks | | | |
| Corners at LOS A/B/C | 8 | 11 | 8 |
| Corners at LOS D | 3 | 0 | 2 |
| Corners at LOS E | 1 | 1 | 2 |
| Corners at LOS F | 0 | 0 | 0 |
| Total | 12 | 12 | 12 |
| Note: LOS = Level-of-Service | | | |



2021 With Action Pedestrian Volumes
Weekday AM Peak Hour
Figure 14-26



2021 With Action Pedestrian Volumes
Weekday Midday Peak Hour
Figure 14-27



2021 With Action Pedestrian Volumes
Weekday PM Peak Hour
Figure 14-28

Table 14-43

2021 With Action Condition: Sidewalk Analysis

| Location | Sidewalk | Effective Width (ft) | Two-way Peak Hour Volume | PHF | SFP | Platoon LOS |
|--|----------|----------------------|--------------------------|-----------------|-------------------|-------------|
| Weekday AM Peak Hour | | | | | | |
| Pike Street between Henry Street and Madison Street | East | 5.5 | 877 | <u>0.800.73</u> | <u>78.871.8</u> | C |
| Pike Street between Henry Street and Madison Street | West | 4.5 | 579 | 0.86 | 105.4 | B |
| Rutgers Street between Madison Street and Henry Street | East | 3.5 | 557 | <u>0.800.77</u> | <u>78.975.9</u> | C |
| Rutgers Street between Madison Street and Henry Street | West | 2.5 | 621 | <u>0.800.78</u> | <u>49.948.6</u> | C |
| Pike Street between Madison Street and Monroe Street | East | 6.5 | 986 | 0.81 | 83.9 | C |
| Rutgers Street between Madison Street and Monroe Street | West | 6.5 | 1194 | <u>0.800.79</u> | <u>68.259.4</u> | C |
| Madison Street between Rutgers Street and Pike Street | North | 5.0 | 2539 | <u>0.800.75</u> | <u>22.821.1</u> | E+ |
| Rutgers Street between Madison Street and Monroe Street | East | 9.0 | 1348 | 0.91 | 95.7 | B |
| Pike Street between Monroe Street and Cherry Street | East | 6.5 | 955 | 0.81 | 86.7 | C |
| Cherry Street between Pike Street and Site 4 (4A/4B) Residential Entrance | South | 6.5 | 834 | <u>0.800.79</u> | <u>98.297.0</u> | B |
| Rutgers Street between Monroe Street and Cherry Street | East | 8.5 | 1041 | 0.85 | 109.4 | B |
| Cherry Street between Frank T. Modica Way (Rutgers Street) and Site 5 Entrance | South | 8.5 | 1902 | <u>0.800.77</u> | <u>55.753.5</u> | C |
| Cherry Street between Frank T. Modica Way (Rutgers Street) and Site 4 (4A/4B) Residential Entrance | South | 6.5 | 960 | 0.83 | 88.4 | C |
| Rutgers Street between Cherry Street and Monroe Street | West | 6.5 | 1133 | 0.85 | 76.5 | C |
| Cherry Street Between Site 5 Entrance and Jefferson Street | South | 10.0 | 1401 | <u>0.800.79</u> | <u>89.888.7</u> | C |
| Clinton Street between Cherry Street and Plaza Entrance | West | 6.5 | 469 | <u>0.800.78</u> | <u>175.3170.9</u> | B |
| Cherry Street between Jefferson Street and Clinton Street | South | 5.5 | 830 | <u>0.800.74</u> | <u>83.377.0</u> | C |
| Clinton Street between Plaza Entrance and South Street | West | 5.5 | 631 | 0.80 | 110.0 | B |
| Weekday Midday Peak Hour | | | | | | |
| Pike Street between Henry Street and Madison Street | East | 5.5 | 656 | 0.81 | 107.1 | B |
| Pike Street between Henry Street and Madison Street | West | 4.5 | 429 | 0.89 | 147.5 | B |
| Rutgers Street between Madison Street and Henry Street | East | 3.5 | 679 | 0.90 | 72.7 | C |
| Rutgers Street between Madison Street and Henry Street | West | 2.5 | 472 | 0.84 | 69.7 | C |
| Pike Street between Madison Street and Monroe Street | East | 6.5 | 718 | 0.87 | 124.3 | B |
| Rutgers Street between Madison Street and Monroe Street | West | 6.5 | 742 | 0.86 | 118.9 | B |
| Madison Street between Rutgers Street and Pike Street | North | 5.0 | 1280 | 0.89 | 54.1 | C |
| Rutgers Street between Madison Street and Monroe Street | East | 9.0 | 852 | 0.88 | 146.9 | B |
| Pike Street between Monroe Street and Cherry Street | East | 6.5 | 699 | <u>0.800.79</u> | <u>117.4115.9</u> | B |
| Cherry Street between Pike Street and Site 4 (4A/4B) Residential Entrance | South | 6.5 | 1757 | 0.80 | 45.7 | C |
| Rutgers Street between Monroe Street and Cherry Street | East | 8.5 | 761 | <u>0.800.79</u> | <u>141.2139.4</u> | B |
| Cherry Street between Frank T. Modica Way (Rutgers Street) and Site 5 Entrance | South | 8.5 | 1921 | <u>0.800.78</u> | <u>55.453.7</u> | C |
| Cherry Street between Frank T. Modica Way (Rutgers Street) and Site 4 (4A/4B) Residential Entrance | South | 6.5 | 1617 | 0.80 | 49.9 | C |
| Rutgers Street between Cherry Street and Monroe Street | West | 6.5 | 756 | 0.93 | 126.2 | B |
| Cherry Street Between Site 5 Entrance and Jefferson Street | South | 10.0 | 1586 | 0.94 | 93.3 | B |
| Clinton Street between Cherry Street and Plaza Entrance | West | 6.5 | 281 | <u>0.800.76</u> | <u>292.9278.3</u> | B |
| Cherry Street between Jefferson Street and Clinton Street | South | 5.5 | 667 | <u>0.800.78</u> | <u>104.0101.3</u> | B |
| Clinton Street between Plaza Entrance and South Street | West | 5.5 | 347 | <u>0.800.78</u> | <u>200.6195.6</u> | B |

Table 14-43 (cont'd)
2021 With Action Condition: Sidewalk Analysis

| Location | Sidewalk | Effective Width (ft) | Two-way Peak Hour Volume | PHF | SFP | Platoon LOS |
|--|----------|----------------------|--------------------------|---------------------|-----------------------|-------------|
| Weekday PM Peak Hour | | | | | | |
| Pike Street between Henry Street and Madison Street | East | 5.5 | 1093 | <u>0.80</u> 0.78 | <u>62.9</u> 61.3 | C |
| Pike Street between Henry Street and Madison Street | West | 4.5 | 696 | <u>0.80</u> 0.75 | <u>81.3</u> 76.1 | C |
| Rutgers Street between Madison Street and Henry Street | East | 3.5 | 741 | 0.93 | 68.8 | C |
| Rutgers Street between Madison Street and Henry Street | West | 2.5 | 795 | 0.83 | 40.0 | C |
| Pike Street between Madison Street and Monroe Street | East | 6.5 | 1108 | 0.87 | 80.2 | C |
| Rutgers Street between Madison Street and Monroe Street | West | 6.5 | 1276 | 0.93 | 74.3 | C |
| Madison Street between Rutgers Street and Pike Street | North | 5.0 | 2743 | 0.83 | 21.7 | E+ |
| Rutgers Street between Madison Street and Monroe Street | East | 9.0 | 1330 | 0.88 | 93.7 | B |
| Pike Street between Monroe Street and Cherry Street | East | 6.5 | 1103 | 0.92 | 85.2 | C |
| Cherry Street between Pike Street and Site 4 (4A/4B) Residential Entrance | South | 6.5 | 1435 | <u>0.80</u> 0.79 | <u>56.5</u> 55.7 | C |
| Rutgers Street between Monroe Street and Cherry Street | East | 8.5 | 1157 | 0.83 | 96.0 | B |
| Cherry Street between Frank T. Modica Way (Rutgers Street) and Site 5 Entrance | South | 8.5 | 2448 | 0.80 | 42.8 | C |
| Cherry Street between Frank T. Modica Way (Rutgers Street) and Site 4 (4A/4B) Residential Entrance | South | 6.5 | 1490 | <u>0.80</u> 0.79 | <u>54.3</u> 53.6 | C |
| Rutgers Street between Cherry Street and Monroe Street | West | 6.5 | 1279 | 0.94 | 75.0 | C |
| Cherry Street Between Site 5 Entrance and Jefferson Street | South | 10.0 | 1749 | 0.83 | 74.4 | C |
| Clinton Street between Cherry Street and Plaza Entrance | West | 6.5 | 569 | <u>0.80</u> 0.74 | <u>144.4</u> 133.5 | B |
| Cherry Street between Jefferson Street and Clinton Street | South | 5.5 | 968 | <u>0.80</u> 0.78 | <u>71.2</u> 69.4 | C |
| Clinton Street between Plaza Entrance and South Street | West | 5.5 | 903 | <u>0.80</u> 0.72 | <u>76.5</u> 68.7 | C |
| Note: SFP = square feet per pedestrian + Denotes a significant adverse pedestrian impact | | | | | | |

Table 14-44
2021 With Action Condition: Corner Analysis

| Location | Corner | Weekday AM Peak Hour | | Weekday Midday Peak Hour | | Weekday PM Peak Hour | |
|---|-----------|----------------------|-----|--------------------------|-----|----------------------|-----|
| | | SFP | LOS | SFP | LOS | SFP | LOS |
| Pike Street and Henry Street | Northeast | <u>95.093.0</u> | A | <u>137.7137.4</u> | A | <u>76.976.4</u> | A |
| | Southeast | <u>107.999.3</u> | A | 179.7 | A | <u>97.494.5</u> | A |
| Pike Street and Madison Street (West) | Northwest | <u>127.7122.7</u> | A | <u>197.8221.6</u> | A | 107.2 | A |
| | Southwest | <u>119.1114.8</u> | A | <u>192.2207.0</u> | A | <u>98.196.7</u> | A |
| Pike Street and Madison Street (East) | Northeast | <u>78.776.1</u> | A | 130.2 | A | 66.8 | A |
| | Southeast | <u>86.285.0</u> | A | 152.5 | A | 84.7 | A |
| Rutgers Street and Madison Street | Northwest | <u>29.028.9</u> | C | 66.1 | A | 33.9 | C |
| | Northeast | <u>33.432.5</u> | C | 67.0 | A | 42.9 | B |
| | Southwest | <u>38.238.1</u> | C | <u>86.486.1</u> | A | <u>47.547.4</u> | B |
| | Southeast | <u>158.1156.0</u> | A | <u>233.0232.5</u> | A | 194.1 | A |
| Pike Street and Cherry Street | Northeast | <u>139.1137.6</u> | A | <u>162.0142.9</u> | A | <u>110.497.9</u> | A |
| | Southeast | <u>105.786.6</u> | A | <u>123.897.8</u> | A | <u>90.670.9</u> | A |
| Cherry Street and Rutgers Street | Northeast | <u>82.776.8</u> | A | <u>124.0121.3</u> | A | <u>67.366.6</u> | A |
| | Southwest | 37.3 | C | <u>27.127.0</u> | C | <u>27.026.9</u> | C |
| | Northwest | 167.8 | A | <u>172.5171.0</u> | A | <u>117.0112.6</u> | A |
| | Southeast | 108.1 | A | 58.3 | B | <u>67.467.2</u> | A |
| Note: SFP = square foot per pedestrian | | | | | | | |

Table 14-45
2021 With Action Condition: Crosswalk Analysis

| Location | Crosswalk | Crosswalk Length (ft) | Crosswalk Width (ft) | Two-way Peak Hour Volume | SFP | LOS |
|--|----------------------------|-----------------------|----------------------|--------------------------|----------|-----|
| Weekday AM Peak Hour | | | | | | |
| Pike Street and Henry Street | East | 30.5 | 14.5 | 729 | 42.2 | B |
| Pike Street and Madison Street (East) | East | 50.0 | 15.0 | 1027 | 25.4 | C |
| Rutgers Street and Madison Street | North | 29.5 | 14.0 | 1551 | 17.9 | D+ |
| | East | 50.5 | 14.0 | 985 | 21.421.1 | D |
| | South (West of the Median) | 23.0 | 15.0 | 747 | 42.2 | B |
| | West | 50.0 | 15.0 | 1822 | 12.4 | E+ |
| | South (East of the Median) | 23.0 | 15.0 | 734 | 43.3 | B |
| Pike Street and Cherry Street | East | 52.0 | 14.0 | 832 | 53.255.2 | B |
| Rutgers Street and Cherry Street | North | 71.0 | 16.0 | 433 | 73.6 | A |
| | East | 50.5 | 13.5 | 1081 | 28.0 | C |
| | South | 21.5 | 14.5 | 892 | 22.8 | D |
| | West | 50.5 | 13.0 | 879 | 33.8 | C |
| Weekday Midday Peak Hour | | | | | | |
| Pike Street and Henry Street | East | 30.5 | 14.5 | 601 | 60.9 | A |
| Pike Street and Madison Street (East) | East | 50.0 | 15.0 | 684 | 41.8 | B |
| Rutgers Street and Madison Street | North | 29.5 | 14.0 | 796 | 40.9 | B |
| | East | 50.5 | 14.0 | 712 | 34.0 | C |
| | South (West of the Median) | 23.0 | 15.0 | 529 | 68.5 | A |
| | West | 50.0 | 15.0 | 985 | 27.1 | C |
| | South (East of the Median) | 23.0 | 15.0 | 505 | 70.3 | A |
| Pike Street and Cherry Street | East | 52.0 | 14.0 | 754 | 62.754.4 | AB |
| Rutgers Street and Cherry Street | North | 71.0 | 16.0 | 321 | 107.7 | A |
| | East | 50.5 | 13.5 | 628 | 47.146.5 | B |
| | South | 21.5 | 14.5 | 1477 | 12.0 | E+ |
| | West | 50.5 | 13.0 | 786 | 40.7 | B |
| Weekday PM Peak Hour | | | | | | |
| Pike Street and Henry Street | East | 30.5 | 14.5 | 836 | 35.4 | C |
| Pike Street and Madison Street (East) | East | 50.0 | 15.0 | 1077 | 23.8 | D |
| Rutgers Street and Madison Street | North | 29.5 | 14.0 | 1066 | 30.5 | C |
| | East | 50.5 | 14.0 | 1077 | 22.3 | D |
| | South (West of the Median) | 23.0 | 15.0 | 838 | 44.1 | B |
| | West | 50.0 | 15.0 | 1780 | 14.4 | E+ |
| | South (East of the Median) | 23.0 | 15.0 | 693 | 54.9 | B |
| Pike Street and Cherry Street | East | 52.0 | 14.0 | 1016 | 45.541.8 | B |
| Rutgers Street and Cherry Street | North | 71.0 | 16.0 | 528 | 56.655.8 | B |
| | East | 50.5 | 13.5 | 1218 | 25.8 | C |
| | South | 21.5 | 14.5 | 1341 | 14.1 | E+ |
| | West | 50.5 | 13.0 | 1046 | 29.0 | C |
| Note: SFP = square feet per pedestrian + Denotes a significant adverse pedestrian impact | | | | | | |

- The west crosswalk of Madison Street and Rutgers Street would deteriorate from LOS C with 28.2 SFP and LOS C with 36.8 SFP to LOS E with 12.3 and 14.4 SFP during the weekday AM and PM peak hours, respectively. These degradations in pedestrian operations constitute significant adverse impacts.
- The south crosswalk of Cherry Street and Rutgers Street would deteriorate from LOS D with 16.6 SFP and LOS C with 29.5 SFP to LOS E with 12.0 and 14.1 SFP during the weekday midday and PM peak hours, respectively. These degradations in pedestrian operations constitute significant adverse impacts.

G. VEHICULAR AND PEDESTRIAN SAFETY EVALUATION

Crash data for the study area intersections were obtained from the NYSDOT for the time period between November 1, 2013 and October 31, 2016. The data obtained quantify the total number of reportable crashes (involving fatality, injury, or more than \$1,000 in property damage), fatalities, and injuries during the study period, as well as a yearly breakdown of vehicular crashes with pedestrians and bicycles at each location. During the November 1, 2013 and October 31, 2016 three-year period, a total of 278 injuries, and 96 pedestrian/bicyclist-related crashes occurred at the study area intersections. A rolling total of crash data identified three high crash locations in the 2013 to 2016 period, Allen Street and Canal Street, the Bowery and Canal Street at the Manhattan Bridge, and Chatham Square/Park Row at Worth Street/Mott Street. **Table 14-46** depicts total crash characteristics by intersection during the study period, as well as a breakdown of pedestrian and bicycle crashes by year and location.

Table 14-46
Accident Summary

| Intersection | | Study Period | | | | | | Accidents by Year | | | | | | | |
|--------------------------------|----------------------------------|-----------------------|------|------|------|------------------|----------------|-------------------|------|------|------|---------|------|------|------|
| North-South Roadway | East-West Roadway | All Accidents by Year | | | | Total Fatalities | Total Injuries | Pedestrian | | | | Bicycle | | | |
| | | 2013 | 2014 | 2015 | 2016 | | | 2013 | 2014 | 2015 | 2016 | 2013 | 2014 | 2015 | 2016 |
| Allen Street | Canal Street | 3 | 8 | 2 | 7 | 0 | 16 | 1 | 1 | 0 | 2 | 1 | 0 | 0 | 3 |
| Allen Street | Delancey Street | 4 | 9 | 12 | 6 | 0 | 37 | 0 | 0 | 2 | 2 | 1 | 0 | 1 | 1 |
| Allen Street | Division Street | 0 | 5 | 3 | 3 | 1 | 10 | 0 | 1 | 2 | 2 | 0 | 0 | 0 | 0 |
| Allen Street | Grand Street | 0 | 7 | 2 | 3 | 0 | 5 | 0 | 1 | 1 | 0 | 0 | 0 | 1 | 0 |
| The Bowery | Bayard Street | 0 | 7 | 3 | 4 | 0 | 6 | 0 | 1 | 2 | 0 | 0 | 0 | 0 | 1 |
| The Bowery | Canal Street/Manhattan Bridge | 5 | 31 | 21 | 14 | 0 | 81 | 0 | 1 | 4 | 2 | 0 | 0 | 1 | 1 |
| The Bowery | Division/Doyers/Catherine Street | 0 | 3 | 6 | 3 | 0 | 7 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 1 |
| Broadway | Worth Street | 1 | 3 | 3 | 2 | 0 | 7 | 1 | 1 | 0 | 1 | 0 | 0 | 3 | 0 |
| Catherine Street | East Broadway | 1 | 1 | 2 | 0 | 0 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Centre Street | Worth Street | 0 | 1 | 1 | 1 | 0 | 4 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 |
| Chatham Square | East Broadway | 0 | 3 | 1 | 1 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 |
| Chatham Square/Park Row | Worth Street/Mott Street | 0 | 1 | 8 | 5 | 0 | 10 | 0 | 0 | 2 | 1 | 0 | 1 | 3 | 0 |
| Clinton Street | Cherry Street | 0 | 1 | 1 | 1 | 0 | 3 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 0 |
| Clinton Street | South Street | 0 | 0 | 1 | 3 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 |
| Lafayette Street | Worth Street | 0 | 3 | 2 | 2 | 0 | 7 | 0 | 1 | 2 | 1 | 0 | 0 | 0 | 1 |
| Market Slip | South Street | 0 | 1 | 1 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Market Street | Division Street | 2 | 5 | 0 | 1 | 0 | 6 | 1 | 2 | 0 | 1 | 0 | 0 | 0 | 0 |
| Market Street | East Broadway | 0 | 2 | 1 | 2 | 0 | 6 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 |
| Market Street | Henry Street | 0 | 2 | 1 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 |
| Montgomery Street | Cherry Street | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 |
| Montgomery Street | South Street | 0 | 1 | 1 | 3 | 0 | 2 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 |
| Montgomery Street | Madison Street | 0 | 2 | 2 | 2 | 0 | 4 | 0 | 1 | 1 | 1 | 0 | 0 | 0 | 0 |
| Pike Slip | South Street | 0 | 1 | 3 | 2 | 0 | 4 | 0 | 1 | 1 | 0 | 0 | 0 | 1 | 0 |
| Pike Street | Cherry Street | 0 | 1 | 0 | 1 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 |
| Pike Street | East Broadway | 0 | 2 | 4 | 7 | 0 | 13 | 0 | 0 | 2 | 3 | 0 | 1 | 0 | 1 |
| Pike Street | Henry Street | 0 | 1 | 2 | 0 | 0 | 5 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 |
| Pike Street | Madison Street | 0 | 4 | 3 | 6 | 0 | 12 | 0 | 1 | 2 | 2 | 0 | 0 | 0 | 1 |
| Rutgers Street | Cherry Street | 0 | 0 | 1 | 2 | 0 | 3 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 |
| Rutgers Slip | South Street | 2 | 2 | 5 | 0 | 1 | 11 | 0 | 1 | 1 | 0 | 0 | 0 | 1 | 0 |
| Rutgers Street | Madison Street | 0 | 2 | 1 | 1 | 0 | 3 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 |
| Pike Slip | Monroe Street | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |

Source: NYSDOT November 1, 2013 through October 31, 2016 accident data

Note: Bold intersections are high accident locations.

Table 14-47 shows a detailed description of each pedestrian/bicyclist-related crash at the high crash locations listed above during the three-year period.

Table 14-47
Vehicle and Pedestrian Crash Details

| Intersection | Year | Date | Time | Crash Class | | Action of Vehicle | Action of Pedestrian | Cause of Crash | | | |
|--|------|-------|---------|-------------|--------|-------------------------------|------------------------------|------------------|----------------------------|--------------------|----------------------------------|
| | | | | Injured | Killed | | | Left/Right Turns | Pedestrian Error/Confusion | Driver Inattention | Other |
| Allen Street and Canal Street | 2013 | 11/21 | 2:00PM | X | | Making right turn – East | Going straight – East | X | | | |
| | | 11/26 | 6:00PM | X | | Going straight – West | Crossing with signal | | | | Unknown |
| | 2014 | 11/20 | 1:56PM | X | | Making left turn – Northeast | Crossing with signal | X | | X | |
| | | 4/15 | 5:56AM | X | | Unknown – North | Unknown | | | | Unknown |
| | 2016 | 5/31 | 8:25AM | X | | Unknown | Unknown | | | | Unknown |
| | | 8/11 | 6:30PM | X | | Making right turn – Southwest | Unknown – South | X | | | |
| | | 10/5 | 4:58PM | X | | Merging – East | Going straight – East | | | X | |
| | | 10/17 | 11:45AM | X | | Making right turn – East | Crossing/No signal or Xwalk | X | | X | |
| The Bowery and Canal Street/Manhattan Bridge | 2014 | 7/31 | 10:00PM | X | | Making left turn – Southeast | Crossing with signal | X | | X | |
| | | 5/4 | 12:30PM | X | | Slowed or stopping – East | Crossing/No signal or Xwalk | | X | | |
| | 2015 | 10/31 | 9:47AM | X | | Going straight – West | Crossing/No signal or Xwalk | | X | | |
| | | 11/1 | 10:30AM | X | | Making right turn – Southwest | Crossing with signal | X | | X | |
| | | 12/9 | 8:55PM | X | | Going straight – Southwest | Not in roadway | | | | Alcohol involvement |
| | | 12/19 | 9:09PM | X | | Changing lanes – West | Changing lanes – West | | | | Unknown |
| | 2016 | 3/30 | 11:25PM | X | | Making left turn – East | Crossing with signal | X | | | |
| | | 8/20 | 12:11PM | X | | Making left turn – East | Going straight – East | X | X | X | |
| | | 10/10 | 5:20AM | X | | Making left turn – East | Crossing with signal | X | | X | |
| Chatham Square/Park Row and Worth Street/Mott Street | 2014 | 12/31 | 12:15PM | X | | Going straight – East | Going straight – East | | X | X | |
| | | 3/04 | 10:30AM | X | | Other – South | Going straight – South | | X | | |
| | 2015 | 4/15 | 12:15PM | X | | Making right turn – North | Crossing against signal | X | X | | |
| | | 5/5 | 9:15PM | X | | Going straight – South | Going straight – West | | | | Failure to yield R.o.W. |
| | | 7/14 | 7:54PM | X | | Going straight – North | Making left turn – Southeast | X | | | Passing or lane usage improperly |
| | | 11/10 | 5:00PM | X | | Going straight – East | Crossing against signal | | | X | |
| | 2016 | 5/16 | 4:15PM | X | | Going straight – East | Crossing/No signal or Xwalk | | X | | |

ALLEN STREET AND CANAL STREET

Based on the review of the crash history at the intersection of Allen Street and Canal Street, no prevailing trends with regard to geometric deficiencies were identified as the primary causes of recorded crashes. With respect to geometric deficiencies that could potentially cause safety hazards, the intersection of Allen Street and Canal Street is signalized and provides five high visibility crosswalks, one of which allows pedestrians to cross Canal Street via the interior median. Standard pedestrian signals are present on all crosswalks. In terms of project-generated activity, this intersection would experience incremental peak hour volume increases of approximately 78 or fewer vehicle trips and negligible pedestrian trips at any crosswalk during

each of the three analysis peak hours. As described in Chapter 21, “Mitigation,” the predicted impact at this intersection could be fully mitigated with standard traffic engineering measures. Therefore, the proposed projects are not anticipated to exacerbate any of the current causes of pedestrian-related crashes. Additional safety measures, such as installing countdown timers on all crosswalks, can be implemented to further improve pedestrian and bicycle safety at this intersection.

THE BOWERY AND CANAL STREET/MANHATTAN BRIDGE

Based on the review of the crash history at the intersection of the Bowery and Canal Street/Manhattan Bridge, no prevailing trends with regard to geometric deficiencies were identified as the primary causes of recorded crashes. With respect to geometric deficiencies that could potentially cause safety hazards, the intersection of the Bowery and Canal Street/Manhattan Bridge is signalized and provides four high visibility crosswalks. In addition, countdown timers are present on the all crosswalks; there is no signal at the stop controlled, northbound right turn from the Bowery to Manhattan Bridge eastbound upper level. In terms of project-generated activity, this intersection would experience incremental peak hour volume increases of approximately 82 or fewer vehicle trips and negligible pedestrian trips at any crosswalk during each of the three analysis peak hours. Additional safety measures, such as installing a countdown timer on the crosswalk serving the northbound, bridge access lane of the Bowery, can be implemented to further improve pedestrian and bicycle safety at this intersection.

CHATHAM SQUARE/PARK ROW AND WORTH STREET/MOTT STREET

Based on the review of the crash history at the intersection of Chatham Square/Park Row and Worth Street/Mott Street, no prevailing trends with regard to geometric deficiencies were identified as the primary causes of recorded crashes. With respect to geometric deficiencies that could potentially cause safety hazards, the intersection of Chatham Square/Park Row and Worth Street/Mott Street is signalized and provides five high visibility crosswalks. In addition, countdown timers are present on all crosswalks. In terms of project-generated activity, this intersection would experience incremental peak hour volume increases of approximately 78 or fewer vehicle trips and negligible pedestrian trips at any crosswalk during each of the three analysis peak hours. As this intersection shows no failings in safety features, and only just trips the upper limits of allowable crashes, no additional safety measures are recommended to further improve pedestrian and bicycle safety at this intersection. However, NYPD traffic enforcement agents are present at this intersection during peak periods to enhance traffic flow and facilitate pedestrian safety.

H. PARKING ASSESSMENT

EXISTING CONDITIONS

Inventories of on-street parking within a ¼-mile and off-street parking within a ½-mile of the project sites were conducted in May 2016 and March 2017. The on-street survey involved recording curbside regulations and performing general observations of daytime utilization. The off-street survey provided an inventory of the area’s public parking facilities and their legal capacities and daytime utilization.

ON-STREET PARKING

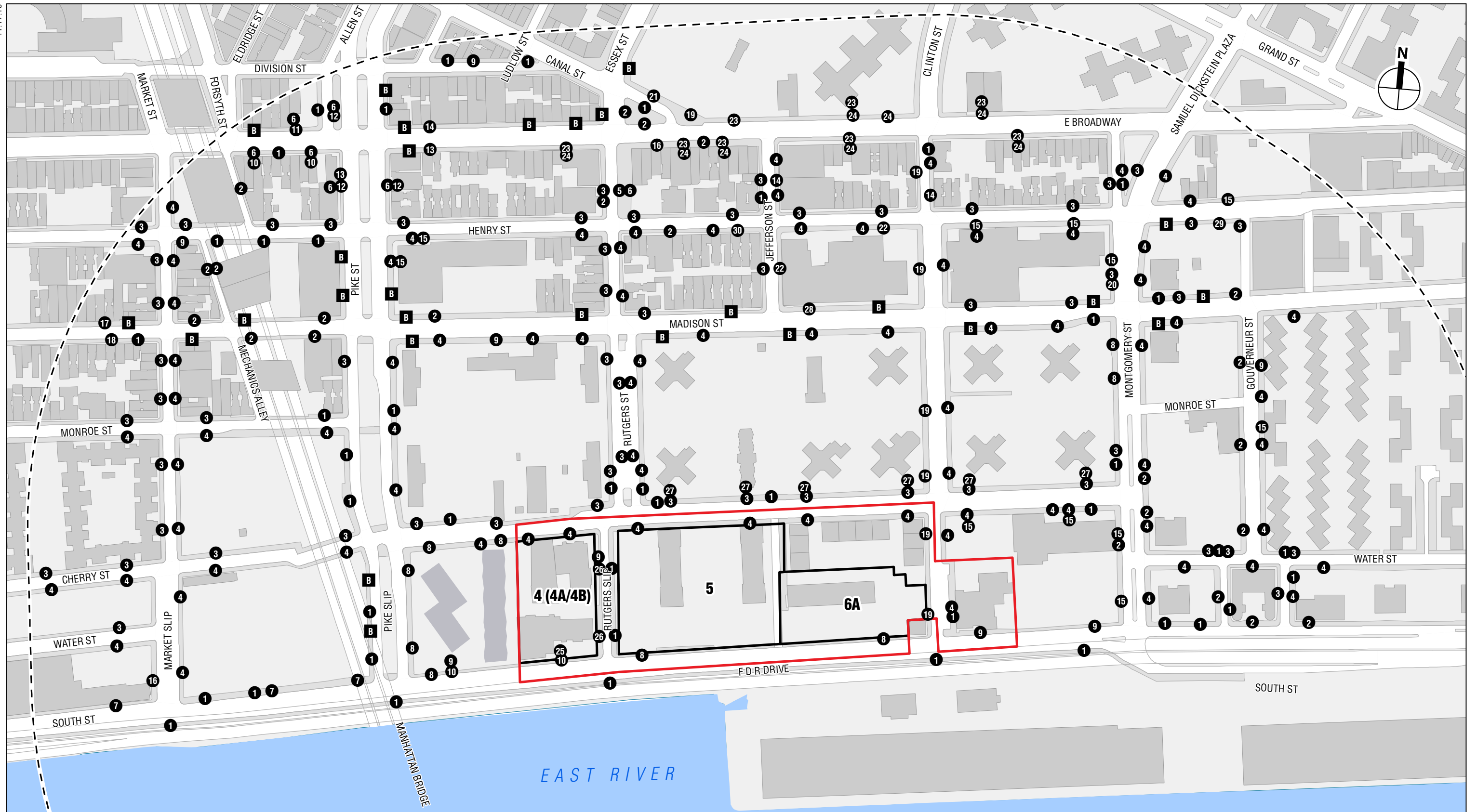
Curbside parking regulations within a ¼-mile of the project sites are illustrated in **Figure 14-29** and summarized in **Table 14-48**. The curbside regulations in the area generally include limited one-hour metered parking, no standing or no parking anytime except authorized vehicles, and alternate-side parking to accommodate street-cleaning. Based on field observations, on-street parking in the area is generally at or near full utilization during weekday daytime hours.

Table 14-48
On-Street Parking Regulations

| No. | Regulation | No. | Regulation |
|---|--|-----|---|
| 1 | NS Anytime | 17 | NS 7AM–10AM Except Sun. |
| 2 | NP Anytime | 18 | NS 4PM–7PM Except Sun. |
| 3 | NP 11:00–12:30AM Mon. and Thu. | 19 | No Stopping Anytime |
| 4 | NP 11:00–12:30AM Tue. and Fri. | 20 | NP 8AM–4PM School Days |
| 5 | NP 7:30–8:00AM Except Sun. | 21 | NS Except Authorized Vehicles (Taxi) |
| 6 | 2-Hr Metered Parking 8AM–7PM Except Sun. | 22 | Doctor License Plates Only |
| 7 | 3-Hr Metered Parking, Buses Only 8AM–6PM Except Sun. | 23 | 1-Hr Metered Parking 8:30AM–7PM Except Sun. |
| 8 | NS Anytime (Temporary Construction Regulation) | 24 | NP 8:00–8:30AM Except Sun. |
| 9 | NP 8AM–6PM Mon.–Fri. | 25 | Ambulette Only Mon.–Fri. 8AM–6PM |
| 10 | NP 3:00–6:00AM Tue., Thu., Sat. | 26 | NS 8AM–6PM Mon.–Fri. |
| 11 | NP 3:00–6:00AM Mon., Wed., Fri. | 27 | Back-in 60-degree Parking Only |
| 12 | NP 7:30AM–8AM Except Sun. | 28 | Ambulette Only |
| 13 | NS Except Trucks Loading and Unloading 7AM–7PM Except Sun. | 29 | Truck Loading Only 9AM–4PM Except Sun. |
| 14 | NS Except Trucks Loading and Unloading 8AM–6PM Except Sun. | 30 | Truck Loading Only 7AM–4PM Except Sun. |
| 15 | NP 7AM–4PM School Days | B | Bus Stop |
| 16 | NS Except Trucks Loading and Unloading | | |
| Notes: NP = No Parking; NS = No Standing; Sun. = Sunday; Mon. = Monday; Tue. = Tuesday; Wed. = Wednesday; Thu. = Thursday; Fri. = Friday; Sat. = Saturday Source: Surveys conducted by AKRF, Inc.; June 2017 | | | |

OFF-STREET PARKING

Off-street publicly accessible parking lots and garages (see **Figure 14-30**) within ½-mile of the project sites were surveyed in February and September 2016. Each facility's operating license and legal capacity were noted. Based on responses given by parking attendants and visual inspections, where possible, estimates were made on the parking occupancy or utilization at each facility for the weekday morning, midday, evening, and overnight time periods. A summary of the recorded information and the area's overall off-street public parking supply and utilization is presented in **Table 14-49**.

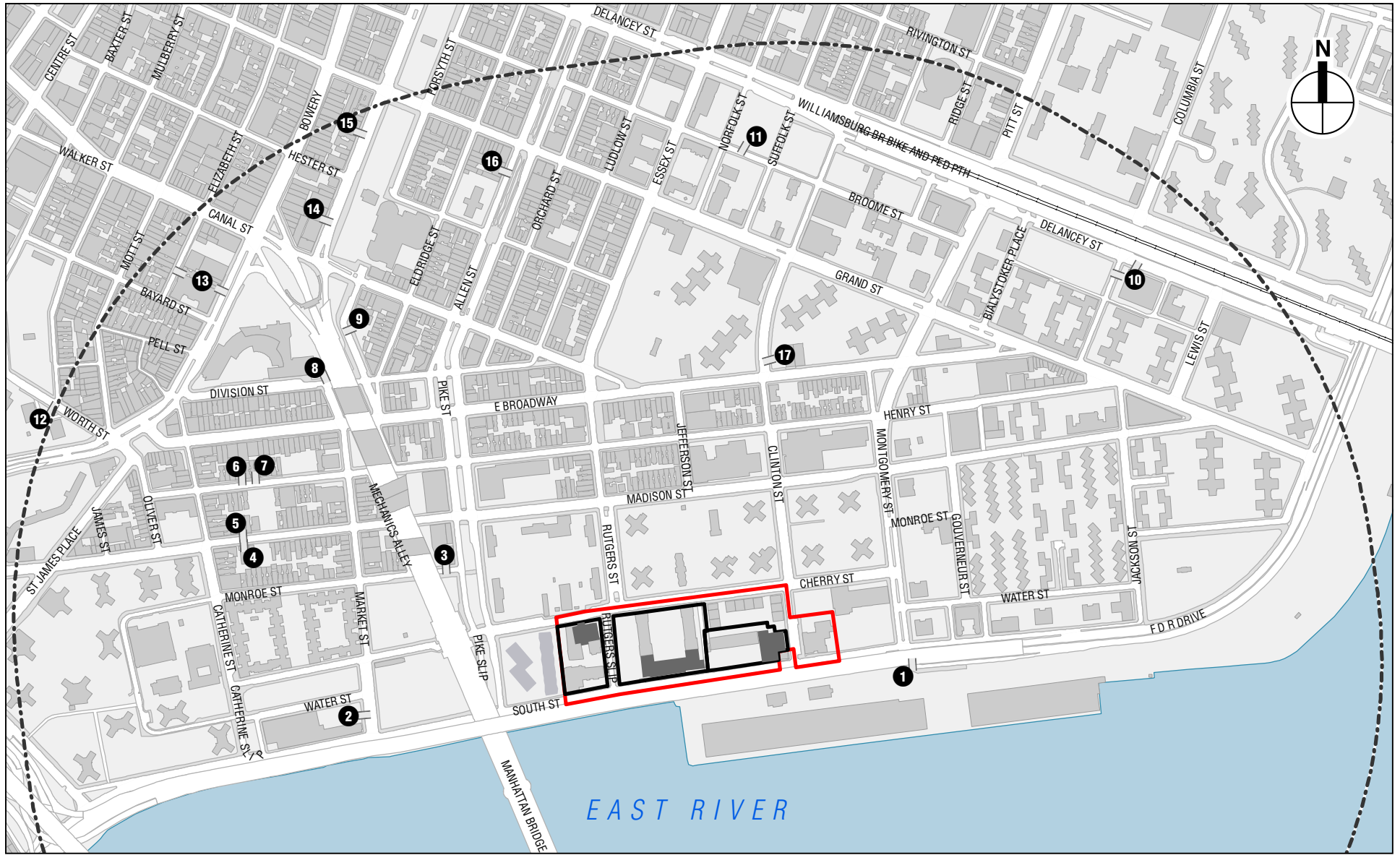


- Project Site
- Boundary of Two Bridges LSRD
- 1/4-mile Radius of Project Sites
- Parking Regulations

TWO BRIDGES LSRD

0 400 FEET

On-Street Parking Regulations
Figure 14-29



Project Sites

Proposed Buildings

Boundary of Two Bridges LSRD

Off-Street Parking

Study Area (1/2-mile boundary)

TWO BRIDGES LSRD

Off-Street Parking Facilities

Figure 14-30

Table 14-49

Existing Weekday Off-Street Parking Supply and Utilization
Approximately ½-Mile Study Area

| Map No. | Name/Operator and Address/Location | License Number | Licensed Capacity | Utilization Rate | | | | Utilized Spaces | | | | Available Spaces | | | |
|--|---|----------------|-------------------|------------------|------------|------------|------------|-----------------|--------------|--------------|--------------|------------------|------------|------------|--------------|
| | | | | AM | MD | PM | ON | AM | MD | PM | ON | AM | MD | PM | ON |
| 1 | Imperial Parking LLC: Pier 42, South FDR | 1446819 | 400 | 85% | 85% | 85% | 85% | 340 | 340 | 340 | 340 | 60 | 60 | 60 | 60 |
| 2 | Edison NY Parking LLC: 220 South Street | 1134501 | 63 | 80% | 85% | 50% | 50% | 50 | 54 | 32 | 32 | 13 | 9 | 31 | 31 |
| 3 | Kaylee Operating LLC: 148 Madison Street | 1155046 | 66 | 80% | 85% | 50% | 50% | 53 | 56 | 33 | 33 | 13 | 10 | 33 | 33 |
| 4 | Madison Street Operating Corp: 88 Madison Street | 908352 | 50 | 80% | 80% | 50% | CLD | 40 | 40 | 25 | CLD | 10 | 10 | 25 | CLD |
| 5 | 10 Street Parking Corp: 38 Henry Street | 925245 | 150 | 75% | 75% | 80% | 80% | 113 | 113 | 120 | 120 | 37 | 37 | 30 | 30 |
| 6 | Henry Operating Corp: 47 Henry Street | 1057433 | 8 | 100% | 100% | 100% | CLD | 8 | 8 | 8 | CLD | 0 | 0 | 0 | CLD |
| 7 | Henry Operating Corp: 49-59 Henry Street | 1039024 | 114 | 40% | 70% | 40% | 40% | 46 | 80 | 46 | 46 | 68 | 34 | 68 | 68 |
| 8 | Champion Confucius: 2-68 Division Street | 1146910 | 300 | 70% | 85% | 85% | 50% | 210 | 255 | 255 | 150 | 90 | 45 | 45 | 150 |
| 9 | Bridge View Auto Service Center: 26 Forsyth Street | 954225 | 42 | 90% | 90% | 90% | 90% | 38 | 38 | 38 | 38 | 4 | 4 | 4 | 4 |
| ½-Mile Area Only Totals | | | 1,193 | 75% | 82% | 75% | 64% | 898 | 984 | 897 | 759 | 295 | 209 | 296 | 376 |
| 10 | Area Garage LLC: (unlisted) | 429851 | 457 | 40% | 88% | 60% | 25% | 183 | 402 | 274 | 114 | 274 | 55 | 183 | 343 |
| 11 | Lower East Side District Mgmt. Assoc. – 135-163 Delancey Street | 2008327 | 294 | 70% | 90% | 75% | 55% | 206 | 265 | 221 | 162 | 88 | 29 | 73 | 132 |
| 12 | Chatham Parking Systems Inc. – 180 Park Row | 368910 | 130 | 65% | 85% | 85% | 65% | 85 | 111 | 111 | 85 | 45 | 19 | 19 | 45 |
| 13 | Quik Park Garage Inc. – 2-8 Elizabeth Street | 1461597 | 140 | 60% | 85% | 60% | 30% | 84 | 119 | 84 | 42 | 56 | 21 | 56 | 98 |
| 14 | T&K Park Inc. – 61 Christie Street | 1344945 | 50 | 20% | 90% | 55% | 25% | 10 | 45 | 28 | 13 | 40 | 5 | 22 | 37 |
| 15 | MTP Operating Corp. – 89-93 Christie Street | 977117 | 116 | 80% | 80% | 60% | 60% | 93 | 93 | 70 | 70 | 23 | 23 | 46 | 46 |
| 16 | 59 Allen Street Garage Corp. – 59-63 Allen Street | 1192853 | 200 | 65% | 85% | 75% | 55% | 130 | 170 | 150 | 110 | 70 | 30 | 50 | 90 |
| 17 | Clinton Grand Parking LLC – 240 E. Broadway | 2034514 | 505 | 60% | 90% | 60% | 55% | 303 | 455 | 303 | 278 | 202 | 50 | 202 | 227 |
| Total ½-Mile Area | | | 3,085 | 65% | 86% | 69% | 53% | 1,992 | 2,644 | 2,138 | 1,633 | 1,093 | 441 | 947 | 1,394 |
| Notes: MD = Midday; ON = Overnight; CLD = Closed Source: Survey conducted by AKRF Inc. in February and September 2016 | | | | | | | | | | | | | | | |

Within the ½-mile parking study area, a total of 17 public parking facilities were inventoried. The combined capacity of these facilities totals 3,085 parking spaces. Overall, they were 65, 86, 69, and 53-percent utilized, with 1,093, 441, 947, and 1,394 parking spaces available during the weekday morning, midday, evening, and overnight time periods, respectively.

THE FUTURE WITHOUT THE PROPOSED PROJECTS

Overall public parking utilization is expected to experience the same growth as projected for traffic. In the No Action condition, No Build projects are expected to displace two public parking facilities and one facility was closed subsequent to data collection, for a total displacement of approximately -757 spaces. As presented in **Table 14-50**, accounting for the parking demand generated from background growth, an additional three percent of background growth to address increases in parking demand from small- to moderate-sized projects in the study area, and parking demand from discrete No Build projects that would advance independent

of the proposed projects, the No Action condition public parking utilization is expected to increase to 100, 128, 105, and 89-percent during the weekday morning, midday, evening, and overnight time periods, respectively, in the ½-mile off-street parking study area. This represents a parking shortfall of up to 646 during the weekday midday peak period.

Table 14-50
Existing and 2021 No Action Parking Supply and Utilization (½-Mile)

| | Weekday AM | Weekday Midday | Weekday PM | Weekday Overnight |
|---|---------------|-------------------|---------------|----------------------|
| Existing Public Parking Supply | 3,085 | 3,085 | 3,085 | 3,027 |
| Existing Public Parking Demand | 1,992 | 2,644 | 2,138 | 1,633 |
| Existing Public Parking Utilization | 65% | 86% | 69% | 54% |
| Displaced Public Parking Supply Total | -757 | -757 | -757 | -757 |
| 2021 No Action Public Parking Supply Total | 2,328 | 2,328 | 2,327 | 2,270 |
| 2021 No Action Background Incremental Demand | 25 | 33 | 27 | 20 |
| Additional Three Percent Background Growth Incremental Demand | 60 | 79 | 64 | 49 |
| Discrete No Build Projects Total Parking Demand | 281 | 258 | 229 | 315 |
| Discrete No Build Projects Accessory Parking Spaces | 60 | 60 | 60 | 60 |
| Discrete No Build Projects Demand Accommodated by Public Parking | 258 | 218 | 220 | 315 |
| No Action Incremental Public Parking Demand | 343 | 330 | 311 | 384 |
| 2021 No Action Public Parking Demand Total | 2,335 | 2,974 | 2,449 | 2,017 |
| 2021 No Action Public Parking Utilization | 100% | 128% | 105% | 89% |
| 2021 No Action Available Spaces (Shortfall) | (7) | (646) | (121) | 253 |
| Samples Calculations: No Action Incremental Public Parking Demand = 2021 No Action Background Incremental Demand + Additional Three Percent Background Growth Incremental Demand + Discrete No Build Projects Demand Accommodated by Public Parking No Action Incremental Public Parking Demand for Weekday AM = 25 + 60 + 258 = 343 2021 No Action Public Parking Demand Total = Existing Public Parking Demand + No Action Incremental Public Parking Demand 2021 No Action Public Parking Demand Total for Weekday AM = 1,992 + 343 = 2,335 | | | | |

THE FUTURE WITH THE PROPOSED PROJECTS

The weekday parking demand generated by the proposed projects is presented in **Table 14-51**. As presented in **Table 14-52**, accounting for the No Action parking supply and demand utilization, and the parking demand generated by the proposed projects, the With Action public parking utilization is expected to increase to 113, 132, 116, and 112 percent of the ½-mile off-street parking capacity during the weekday morning, midday, evening, and overnight time periods, respectively. These utilization levels represent parking shortfalls of 293, 755, 373, and 274 spaces during the corresponding weekday peak periods.

Table 14-51
Parking Demand from Proposed Projects—Weekday

| Hour | Residential | Local Retail | School Staff | Total |
|-------------|-------------|--------------|--------------|-------|
| 12 AM–01 AM | 527 | 0 | 0 | 527 |
| 01 AM–02 AM | 527 | 0 | 0 | 527 |
| 02 AM–03 AM | 527 | 0 | 0 | 527 |
| 03 AM–04 AM | 527 | 0 | 0 | 527 |
| 04 AM–05 AM | 527 | 0 | 0 | 527 |
| 05 AM–06 AM | 527 | 0 | 0 | 527 |
| 06 AM–07 AM | 527 | 0 | 0 | 527 |
| 07 AM–08 AM | 453 | 0 | 0 | 453 |
| 08 AM–09 AM | 284 | 0 | 2 | 286 |
| 09 AM–10 AM | 189 | 0 | 2 | 191 |
| 10 AM–11 AM | 128 | 0 | 2 | 130 |
| 11 AM–12 PM | 107 | 0 | 2 | 109 |
| 12 PM–01 PM | 107 | 0 | 2 | 109 |
| 01 PM–02 PM | 107 | 0 | 2 | 109 |
| 02 PM–03 PM | 107 | 0 | 2 | 109 |
| 03 PM–04 PM | 109 | 0 | 2 | 111 |
| 04 PM–05 PM | 144 | 0 | 2 | 146 |
| 05 PM–06 PM | 252 | 0 | 0 | 252 |
| 06 PM–07 PM | 343 | 0 | 0 | 343 |
| 07 PM–08 PM | 424 | 0 | 0 | 424 |
| 08 PM–09 PM | 459 | 0 | 0 | 459 |
| 09 PM–10 PM | 487 | 0 | 0 | 487 |
| 10 PM–11 PM | 510 | 0 | 0 | 510 |
| 11 PM–12 AM | 527 | 0 | 0 | 527 |

Table 14-52
2021 No Action and With Action Parking Supply and Utilization (½-Mile)

| | Weekday AM | Weekday Midday | Weekday PM | Weekday Overnight |
|---|------------|----------------|------------|-------------------|
| 2021 No Action Public Parking Supply | 2,328 | 2,328 | 2,328 | 2,270 |
| 2021 No Action Public Parking Demand | 2,335 | 2,974 | 2,449 | 2,017 |
| 2021 No Action Public Parking Utilization | 100% | 132% | 116% | 112% |
| Proposed Projects Parking Demand | 286 | 109 | 252 | 527 |
| Proposed Projects Accessory Parking Spaces | 0 | 0 | 0 | 0 |
| Proposed Projects Parking Demand Accommodated by Accessory Parking | 0 | 0 | 0 | 0 |
| Proposed Projects Parking Demand Accommodated by Public Parking | 286 | 109 | 252 | 527 |
| 2021 With Action Public Parking Demand Total | 2,621 | 3,083 | 2,701 | 2,544 |
| 2021 With Action Public Parking Utilization | 113% | 132% | 116% | 112% |
| 2021 With Action Available Spaces (Shortfall) | (293) | (755) | (373) | (274) |
| Sample Calculation: | | | | |
| 2021 With Action Public Parking Demand Total = 2021 No Action Public Parking Demand + Proposed Projects Demand Accommodated by Public Parking | | | | |
| 2021 With Action Public Parking Demand Total for Weekday Overnight = 2,270 + 527 = 2,544 | | | | |

It is expected that excess parking demands resulting from the proposed projects during the weekday peak periods would need to be accommodated by on-street parking or off-street parking beyond ½-mile walk from the project sites. Alternatively, motorists could choose alternate modes of transportation. As stated in the *CEQR Technical Manual* and discussed in the above parking analysis methodology, a parking shortfall resulting from a project located in Manhattan does not constitute a significant adverse parking impact, due to the magnitude of available alternative modes of transportation. *