## **CHAPTER 21: MITIGATION**

#### A. INTRODUCTION

According to the *CEQR Technical Manual*, where significant adverse impacts are identified, mitigation to reduce or eliminate the impacts to the fullest extent practicable is developed and evaluated. In addition, in the absence of a commitment to mitigation or when no feasible mitigation measures can be identified, a reasoned elaboration as to why mitigation is not practicable should be put forth, and the potential for unmitigated or unmitigated significant adverse impacts must be disclosed.

Measures to mitigate adverse impacts <u>have been</u> evaluated <u>by the lead agency in consultation with expert and involved agencies</u> between the Draft Environmental Impact Statement (DEIS) and Final Environmental Impact Statement (FEIS). Therefore, the FEIS includes more complete information and commitments on all practicable mitigation measures to be implemented with the Proposed Actions.

#### B. PRINCIPAL CONCLUSIONS

#### **COMMUNITY FACILITIES**

CHILD CARE FACILITIES

To avoid the significant adverse impact on child care, the Proposed Actions would need to create a total of 72 new publicly funded child care slots. Alternatively, the number of affordable dwelling units that could be developed on the identified Projected Developed Sites would have to be reduced to 210 affordable units from 1,061 affordable units—an approximately 80 percent reduction (851 fewer affordable units).

Potential mitigation measures for significant adverse impacts to child care centers <u>were</u> developed in consultation with the New York City Administration for Children's Services (ACS), <u>DOE and SCA</u>. The projected increase in demand for child care slots in the With-Action Condition could be offset by private day care facilities and day care centers outside of the Child Care Study Area, which are not included in this analysis; some parents may choose day care providers that are closer to their workplace rather than their home. While the CEQR analysis is limited to ACS-contracted child care facilities per the 2014 *CEQR Technical Manual*, DOE also contracts with childcare providers to provide additional publicly-funded early education opportunities that are available to all residents, regardless of family income. Since 2014, the City has made significant investments to provide free, full-day, high-quality early childhood education through Pre-K for All and 3-K for All, as part of a broader effort to create a continuum of high-quality early care and education programs for New York City children from birth to five years old. Furthermore, all programs previously managed by ACS will shift to management by DOE, enabling consistent high-quality standards under a single agency by the second half of 2019.

There are an additional ten DOE-operated or DOE-contracted sites in the study area that are available to all residents, regardless of family income, that are not included in the CEQR analysis.

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In addition, the SCA plans to construct eight new 3K centers on Staten Island that would add an additional 965 slots childcare capacity, at least two of which would be located within the study area, anticipated to open by 2020. ACS will also monitor the demand and need for additional publicly funded day care services in the area and identify the appropriate measures to meet demand for additional slots.

While these measures could offset or would serve to at least partially mitigate the identified impact, in the event that the significant adverse impact on publicly funded child care facilities is not completely eliminated, an unavoidable significant impact would result.

# PUBLIC SCHOOLS

To avoid the identified significant adverse elementary school impact in Sub-district 4 of Community School District (CSD) 31, the number of incremental dwelling units that could be developed in the sub-district would have to be reduced to 1,720, generating 482 elementary school students, as compared to No-Action conditions. This would represent a decrease of 837 DU (33 percent) in CSD 31, Sub-district 4. An increase of 482 elementary school students within Sub-district 1 of CSD 31, would increase the No-Action utilization rates in the sub-district by less than five percentage points and would be below the CEQR Technical Manual threshold and, thus, not a significant adverse impact.

To avoid the potential for a significant adverse impact on elementary schools in CSD 31, Sub-district 4, the Proposed Actions would need to add approximately 175 new elementary school seats increasing capacity. If additional school construction is warranted, and funding is available, it will be identified in the Five-Year Capital Plan that covers the period in which the capacity need would occur. If the Bay Street Corridor Rezoning application is approved, a parcel within the Stapleton Waterfront Phase III development, which has been identified, will serve as the site for a new primary or prekindergarten through 8th grade school construction by the SCA. This action would take place in a future Five-Year Capital Plan, as the development associated with the Proposed Actions proceeds and should the need arise. This mitigation would be supplemented through administrative actions that the DOE would undertake to mitigate the shortfall in school seats, such as adjusting catchment areas and/or reorganizing grade levels within schools. DOE would continue to monitor trends in demand for school seats in the area. The DOE responses to identified demand could take place in stages an include administrative actions and/or enlargement of existing schools, followed by the later construction or lease of new school facilities at an appropriate time. In the current 2020-2024 Five Year Capital Plan, 1,776 elementary/intermediate school seats have been funded to address exiting school seat needs in CSD 31, Sub-district 4. SCA is in the process of identifying appropriate sites to locate and construct these funded school seats.

New York City Department of City Planning (DCP), as lead agency, will <u>continue to explore these</u> mitigation measures with the SCA/\_DOE. If <u>these</u> mitigation measures cannot be <u>implemented</u>, the impact will be identified as unavoidable.

## **OPEN SPACE**

To avoid the significant adverse indirect impacts on total and active open space resources in the 0.5-mile Residential Study Area, the total amount of open space created in the With-Action Condition

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would need to increase by approximately  $6.\underline{15}$  acres ( $1.\underline{55}$  acres more than the  $\underline{4.6}$  acres provided in the With-Action), including  $2.\underline{37}$  acres of active open space. Alternatively, the number of dwelling units that could be developed on the Projected Development Sites would have to be *reduced* to  $1,\underline{601}$  dwelling units from 2,569 dwelling units—an approximately  $\underline{38}$  percent decrease ( $\underline{968}$  fewer dwelling units).

Measures considered to mitigate the Proposed Actions' significant adverse open space impact include: developing a new recreation center at the Lyons Pool site; making improvements to existing parks to allow for expanded programming and enhanced usability; making New York City public school playgrounds accessible to the community after school hours through the Schoolyards to Playgrounds program; and public realm improvements in the vicinity of the intersection of Victory Boulevard and Bay Street. These potential mitigation measures were explored in coordination with the lead agency, DPR, DOE, DOT and EDC between the DEIS and the FEIS.

Based on these discussions, the following mitigation measure has been identified for implementation:

Public realm and pedestrian improvements at underutilized street space located at the intersection of Victory Boulevard and Bay Street: These improvements will provide an enhanced pedestrian realm at a critical gateway to the Bay Street Corridor. They will consist of amenities such as benches, lighting, trees and planting to encourage pedestrian activity, support access to public transit, and improve the streetscape. The proposed public realm improvements are anticipated to total at least 0.13 acres.

Other measures have been identified that could substantially enhance and/or increase the amount of open space resources for the additional population introduced by the Proposed Actions. If funded and implemented, these measures could further mitigate the significant adverse open space impact.

Although these additional measures could substantially enhance and increase the usability of open space resources and partially mitigate the significant adverse open space impact in the With-Action Condition, capital and expense of funding to build and maintain additional open space or park facilities has not been identified at this point in time. Consequently, the Proposed Actions' significant adverse indirect open space impact would not be completely eliminated and, as a result, an unavoidable significant adverse open space impacts would occur. However, the City will continue to explore avenues to implement the measures identified along with other opportunities to create new publicly-accessible open space resources, improve existing open spaces, and/or provide additional programming within existing open spaces.

# HISTORIC AND CULTURAL RESOURCES

As discussed in Chapter 7, "Historic and Cultural Resources," the construction activity at Projected Development Site 5 under the With-Action Condition has the potential to result in significant adverse archaeological impacts associated with prehistoric resources and nineteenth- to early twentieth-century waterfront features.

A Phase 1A study of Projected Development Site 5 was completed in May 2017 (Appendix E). The Phase 1A study concluded that the archaeological area of potential effects (APE) has a moderate to

high sensitivity for prehistoric resources on the western margin in the limited area of fast land, and a moderate to high sensitivity for nineteenth- to early-twentieth-century waterfront features (docks or piers) in the remainder of the southern archaeological-APE. The northern, narrow portion of the archaeological-APE was identified as having no to low sensitivity for shoreline features. The Phase IA recommended archaeological testing in advance of any future ground disturbing developments within the two areas of archaeological sensitivity to determine the absence or presence of potential buried resources. However, as Projected Development Site 5 is owned by a private entity, there is no mechanism in place to require a developer to conduct archaeological testing or require the preservation or documentation of archaeological resources, should they exist. Therefore, a significant adverse effect related to archaeological resources may occur on Projected Development Site 5. Because there is no mechanism to avoid or mitigate potential impacts to archaeological resources at the privately-owned Projected Development Site 5, the significant adverse impact would be unavoidable.

# **TRANSPORTATION**

#### **TRAFFIC**

As described in Chapter 14, "Transportation," the Proposed Actions would result in significant adverse traffic impacts at 31 study area intersections during one or more analyzed peak hours; specifically, 36 lane groups at 24 intersections during the Weekday AM peak hour, 43 lane groups at 21 intersections during the Weekday MD peak hour, 59 lane groups at 26 intersections during the Weekday PM peak hour, and 37 lane groups at 20 intersections during the Saturday MD peak hour. Implementation of traffic engineering improvements such as signal timing changes or modifications to curbside parking regulations would provide mitigation for several of the anticipated traffic impacts. Implementation of the recommended traffic engineering improvements is subject to review and approval by New York City Department of Transportation (DOT) and will be based on the findings of a traffic monitoring program (TMP) developed by DCP in collaboration with DOT. If, prior to implementation, DOT determines that an identified mitigation measure is infeasible, an alternative and equivalent mitigation measure will be considered. However, if no other alternative mitigation measures can be identified, those impacts would be unmitigated.

Table 21-1 shows that significant adverse impacts would be fully mitigated at all but 10 lane groups at 6 intersections during the Weekday AM peak hour, 24 lane groups at 11 intersections during the Weekday MD peak hour, 46 lane groups at 21 intersections during the Weekday PM peak hour, and 14 lane groups at 9 intersections during the Saturday MD peak hour.

Table 21-1: Summary of Lane Groups/Intersections with Partially Mitigated and/or Unmitigated Significant Adverse Traffic Impacts

	Weekday AM	Weekday Midday	Weekday PM	Saturday Midday
Impacted Lane Groups	10	24	46	14
Impacted Intersections	6	11	21	9

Tables 21-2 and 21-3 provide a more detailed summary of the intersections that would have significant adverse traffic impacts and indicates whether the impacts would be fully mitigated for the

signalized and unsignalized intersections, respectively. In total, impacts to one or more approach movements would remain unmitigated in one or more peak hours at 21 intersections.

Table 21-2: Signalized Intersections with Partially Mitigated and/or Unmitigated Significant Adverse Traffic Impacts

Adverse Traffic Impacts Signalized Intersection	Weekday AM	Weekday Midday	Weekday PM	Saturday Midday
Richmond Terrace and Franklin Avenue				
Richmond Terrace and Jersey Street			X	
Richmond Terrace and Westervelt Avenue				
Hamilton Avenue and Richmond Terrace				
Wall Street and Richmond Terrace				
Richmond Terrace and Ferry Terminal (bus)		X	X	X
Richmond Terrace and Ferry Terminal (parking lot)		X	X	X
Bay Street and Slosson Terrace				
Victory Boulevard and Bay Street/St. Marks Place			X	
Victory Boulevard and Bay Street		X	X	X
Bay Street and Hannah Street	X			
Front Street and Hannah Street				
Bay Street and Swan Street/Van Duzer Street			X	
Bay Street and Grant Street	X	X	X	X
Van Duzer Street and Clinton Street				
Bay Street and Clinton Street				
Bay Street and Baltic Street		X	X	X
Bay Street and Wave Street			X	
Front Street and Wave Street				
Front Street and Prospect Street				
Van Duzer Street and Beach Street				
Bay Street and Water Street		X	X	X
Bay Street and Canal Street			X	
Front Street and Canal Street				
Bay Street and Broad Street			X	
Richmond Terrace and Clove Road				
Victory Boulevard and Cebra Avenue	X	X	X	
Victory Boulevard and Jersey Street		X	X	X
Victory Boulevard and Forest Avenue			X	
Broad Street and Canal Street				
Broad Street and Van Duzer Street				
Broad Street and Targee Street				
Vanderbilt Avenue and Tompkins Avenue	X	X	X	
Bay Street and Vanderbilt Avenue			X	
Bay Street and Edgewater Drive				
Bay Street and Hylan Boulevard	X	X	X	X
Bay Street and School Road			X	

Table 21-3: Unsignalized Intersections with Partially Mitigated and/or Unmitigated Significant Adverse Traffic Impacts

Unsignalized Intersection	Weekday AM	Weekday Midday	Weekday PM	Saturday Midday
Hamilton Avenue and Stuyvesant Place				
Wall Street and Stuyvesant Place				
Front Street and Hannah Street <sup>1</sup>				
Van Duzer Street and St Julian Place				
Bay Street and St Julian Place				
Bay Street and Grant Street <sup>2</sup>				
Bay Street and Baltic Street <sup>2</sup>				
Bay Street and William Street	X	X	X	X
Bay Street and Congress Street			X	
Bay Street and Wave Street <sup>1</sup>				
Front Street and Wave Street <sup>1</sup>				
Front Street and Prospect Street <sup>1</sup>				
Bay Street and Water Street <sup>1</sup>				
Front Street and Canal Street <sup>1</sup>				
Jersey Street and Brook Street				
Pike Street and Brook Street				
Pike Street and Victory Boulevard				
Hudson Street and Cedar Street				
Broad Street and Cedar Street				

**Notes:** 1 - Intersection becomes signalized in No-Action Condition. 2 - Intersection becomes signalized with mitigation.

## TRANSIT (BUS)

The Proposed Actions would result in a capacity shortfall on all bus routes serving the study area during the Weekday AM and PM peak hours. These significant adverse bus transit impacts could be fully mitigated by the addition of two to six additional standard buses to each direction of each route during both peak hours. The general policy of NYCT is to provide additional bus service where demand warrants, taking into account financial and operational constraints.

#### **PEDESTRIAN**

Incremental demand from the Proposed Actions would result in significant adverse pedestrian impacts at a total of 11 sidewalks and <u>5</u> crosswalks during one or more peak hours. Mitigation measures recommended to address significant adverse traffic impacts would result in significant adverse pedestrian impacts at an additional <u>two</u> crosswalks in one or more peak hours.

Recommended mitigation measures to address the pedestrian impacts are discussed below. Implementation of these measures would be subject to review and approval by DOT. If, prior to implementation, DOT determines that an identified mitigation measure is infeasible, an alternative

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and equivalent mitigation measure will be identified. <u>However, if no other alternative mitigation</u> measures can be identified, those impacts would be unmitigated.

#### Sidewalks

Eleven of the 28 analyzed sidewalks are expected to be significantly adversely impacted by the Proposed Actions. Due to constrained right-of-way, mitigation measures to address the potential significant adverse pedestrian impacts for all significantly impacted sidewalks are not feasible. Therefore, these sidewalks could not be mitigated and the impacts are considered significant and unavoidable.

# Crosswalks

With the implementation of mitigation measures recommended to address significant adverse traffic impacts, a total of seven of the 20 analyzed crosswalks would be significantly adversely impacted by the Proposed Actions. Crosswalk widening between 0.6 feet and 10.3 feet would fully mitigate all seven impacted crosswalks.

#### CONSTRUCTION

#### HISTORIC AND CULTURAL RESOURCES

As described in Chapter 7, "Historic and Cultural Resources," development under the Proposed Actions— specifically, on Projected Development Site 20 and Potential Development Site Q—could result in inadvertent construction-related damage to two NYCL- and/or S/NR-eligible historic resources, as they are located within 90 feet of one or more of the aforementioned projected and potential development sites. The two eligible resources – S/NR-eligible 292 Van Duzer Street and the S/NR-eligible and NYCL-eligible Stapleton Branch of the New York City Public Library – would not be redeveloped under the No-Action condition. If these eligible resources are designated in the future prior to the initiation of construction, the protective measures of New York City Department of Buildings (DOB) Technical Policy and Procedure Notice (TPPN) #10/88 would apply and indirect significant adverse impact from construction would be avoided. Should they remain undesignated, however, the additional protective measures of TPPN #10/88 would not apply, and the potential for significant adverse construction-related impacts would not be mitigated.

#### NOISE

As described in Chapter 20, "Construction," the Proposed Actions would have the potential to result in significant adverse construction noise impacts throughout the Project Area and at sensitive receptors in the vicinity of the Project Area. Because the analysis is based on a conceptual site plan and construction schedule, it is possible that the actual construction may be of less magnitude, or that construction on multiple Projected Development Sites might not overlap, in which case construction noise would be less intense than the analysis predicts.

Between the DEIS and FEIS, possible mitigation measures to address the identified potential construction noise impacts <u>were</u> explored. <u>It was found that there are no reasonable means to ensure measures be employed that would mitigate, partially or fully, the significant adverse construction</u>

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noise impacts; therefore, the significant adverse construction noise impacts identified in Chapter 20, "Construction," would be unavoidable.

#### C. COMMUNITY FACILITIES

#### CHILD CARE SERVICES

Under the Proposed Actions, approximately 1,061 new low- to moderate-income units would be developed by 2030, which would generate approximately 95 children under the age of six who would be eligible for publicly funded child care programs based on the *CEQR Technical Manual* child care multipliers. With the additional children, in the With-Action Condition, there would be a deficit of 98 slots in the 1.5-mile Child Care Study Area by 2030 (125.59 percent utilization), and the utilization rate of the existing child care facilities would increase by approximately 24.80 percentage points over the No-Action Condition (100.78 percent utilization).

To avoid the significant adverse impact on child care, the Proposed Actions would need to create a total of 72 new publicly funded child care slots. Alternatively, the number of affordable dwelling units that could be developed on the identified Projected Developed Sites would have to be reduced to 210 affordable units from 1,061 affordable units—an approximately 80 percent reduction (851 fewer affordable units).

The projected increase in demand for child care slots in the With-Action Condition could be offset by private day care facilities and day care centers outside of the Child Care Study Area, which are not included in this analysis; some parents may choose day care providers that are closer to their workplace rather than their home. While the CEQR analysis is limited to ACS-contracted child care facilities per the 2014 CEQR Technical Manual, DOE also contracts with childcare providers to provide additional publicly-funded early education opportunities that are available to all residents, regardless of family income. Since 2014, the City has made significant investments to provide free, full-day, high-quality early childhood education through Pre-K for All and 3-K for All, as part of a broader effort to create a continuum of high-quality early care and education programs for New York City children from birth to five years old. Furthermore, all programs previously managed by ACS will shift to management by DOE, enabling consistent high-quality standards under a single agency by the second half of 2019.

As shown in Table 21-4. there are an additional ten DOE-operated or DOE-contracted sites in the study area that are available to all residents, regardless of family income, that are not included in the CEQR analysis.

In addition, the SCA plans to construct eight new 3K centers on Staten Island that would add an additional 965 slots childcare capacity, at least two of which would be located within the study area, anticipated to open by 2020.

Table 21-4: Additional DOE-Operated and Contracted Child Care Facilities in Study Area

<u>Name</u>	Address	Borough	Zip	3K seats in	Pre-K seats	Included in
<u></u>	LARRA VOU	<u> </u>		2019-20	in 2019-20	CEQR?
The Richmond Pre-K Center at	120 Stuyvesant Pl.	Staten Island	10301	<u>45</u>	<u>54</u>	<u>No</u>
120 Stuyvesant Place						
Alwayz1.2.3 Early Learning	<u>80 Bay St</u> .	Staten Island	<u>10301</u>	<u>15</u>	<u>0</u>	<u>No</u>
<u>Center</u>						
Saint Peter - Saint Paul School	129 Clinton Ave.	Staten Island	<u>10301</u>	<u>30</u>	<u>60</u>	<u>No</u>
Children's Harbor Montessori	1000 Richmond Ter.	Staten Island	10301	<u>0</u>	<u>27</u>	<u>No</u>
<u>School</u>						
<u>Jewish Community Center of</u>	485 Victory Blvd.	Staten Island	<u>10301</u>	<u>30</u>	<u>54</u>	<u>No</u>
<u>Staten Island</u>						
Yeled V'Yalda Silver Lake I	<u>10 Gregg Pl</u> .	Staten Island	<u>10301</u>	<u>23</u>	<u>36</u>	<u>No</u>
<u>Head Start</u>						
Sacred Heart School	301 North Burgher Ave.	Staten Island	<u>10310</u>	<u>0</u>	<u>54</u>	<u>No</u>
<b>Hugs &amp; Kiddies of Staten</b>	140 Harvest Ave.	Staten Island	10310	<u>12</u>	<u>16</u>	<u>No</u>
<u>Island</u>						
Yeled V'Yalda Silver Lake	20 Park Hill Cir.	Staten Island	<u>10304</u>	<u>45</u>	<u>58</u>	<u>No</u>
<u>Head Start II</u>						
Most Terrific Child	555 Tompkins Ave.	Staten Island	<u>10305</u>	<u>15</u>	<u>15</u>	<u>No</u>
		<u>I</u>	<u>'otal</u>	<u>429</u>	<u>592</u>	

ACS <u>will</u> monitor the demand and need for additional publicly funded day care services in the area and identify the appropriate measures to meet demand for additional slots. While these measures <u>and the factors described above</u> could offset or would serve to at least partially mitigate the identified impact, in the event that the significant adverse impact on publicly funded child care facilities is not completely eliminated, an unavoidable significant adverse impact would result.

#### **PUBLIC SCHOOLS**

The Proposed Actions are anticipated to result in a significant adverse impact to public elementary schools. The Project Area falls within the boundaries of CSD 31, Sub-district 4. The Proposed Actions would introduce approximately 1,331 total students, including approximately 716 elementary school students over the No-Action Condition. The elementary school utilization rate would increase from 129 percent in the No-Action Condition to 136 percent in the With-Action Condition (a 7.0-percentage-point increase), with a deficit of 3,911 elementary school seats. According to CEQR Technical Manual guidance, a significant adverse impact may result if a proposed action would result in (i) a utilization rate equal to or greater than 100 percent, and (ii) an increase in the collective utilization rate of equal to or greater than 5 percentage points between the No-Action and With-Action conditions. Therefore, the Proposed Actions are anticipated to result in a significant adverse impact to elementary schools in CSD 31, Sub-district 4, when the 838 residential unit is constructed which is expected to occur in 2024.

While the <u>DEIS did not identify a significant adverse impact related to public schools, it was noted that new data was anticipated, which could potentially change the DEIS conclusions. As mentioned in Chapter 4 of the FEIS, "Community Facilities," shortly before the issuance of the DEIS, new data from the School Construction Authority (SCA) was released related to projected public school ratios, enrollment projections, and projected new housing starts. Based on the re-analyzed indirect effects</u>

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on public elementary schools, the Proposed Actions would potentially result in a significant adverse impact to public elementary schools in CSD 31, Sub-district 4.

To avoid the identified significant adverse elementary school impact in Sub-district 4 of CSD 31, the number of incremental dwelling units that could be developed in the sub-district would have to be reduced to 1,720, generating 482 elementary school students, as compared to No-Action conditions. This would represent a decrease of 837 DU (33 percent) in CSD 31, Sub-district 4. An increase of 482 elementary school students within Sub-district 1 of CSD 31, would increase the No-Action utilization rates in the sub-district by less than five percentage points and would be below the *CEQR Technical Manual* threshold and, thus, not a significant adverse impact.

To avoid the potential for a significant adverse impact on elementary schools in CSD 31, Sub-district 4, the Proposed Actions would need to add approximately 175 new elementary school seats increasing capacity. If additional school construction is warranted, and funding is available, it will be identified in the Five-Year Capital Plan that covers the period in which the capacity need would occur. If the Bay Street Corridor Rezoning application is approved, a parcel within the Stapleton Waterfront Phase III development, which has been identified, will serve as the site for a new primary or pre-kindergarten through 8th grade school construction by the SCA. This action would take place in a future Five-Year Capital Plan, as the development associated with the Proposed Actions proceeds and should the need arise.

The Proposed A-Text Application (N190114(A) ZRR, and C190179(A) HAR), provides a waiver of community facility floor area in the Special Stapleton Waterfront District on Sites A or B1 for 100,000 sf of school use, which could facilitate this mitigation. This mitigation would be supplemented through administrative actions that the DOE would undertake to mitigate the shortfall in school seats, such as adjusting catchment areas and/or reorganizing grade levels within schools. DOE would continue to monitor trends in demand for school seats in the area. The DOE responses to identified demand could take place in stages an include administrative actions and/or enlargement of existing schools, followed by the later construction or lease of new school facilities at an appropriate time. In the current 2020-2024 Five Year Capital Plan, 1,776 elementary/intermediate school seats have been funded to address exiting school seat needs in CSD 31, Sub-district 4. SCA is in the process of identifying appropriate sites to locate and construct these funded school seats.

To mitigate the identified elementary school impacts resulting from the Proposed Actions, enrollment in CSD 31, Sub-district 4 will be monitored. If a need for additional capacity is identified, DOE will evaluate the appropriate timing and mix of measures, identified above, to address increased school enrollment. In coordination with the New York City School Construction Authority (SCA), if additional school construction is warranted, and if funding is available, it will be identified in the Five-Year Capital Plan that covers the period in which the capacity need would occur (refer to the SCA's letter to the City Planning Commission Chair dated April 9, 2019, provided in Appendix K, "Agency Correspondence"). If feasible mitigation measures cannot be identified to fully mitigate the impact, the impact will be identified as unavoidable.

# Chapter 21: Mitigation

#### D. OPEN SPACE

As discussed in Chapter 5, "Open Space," <u>the Proposed Actions would result in a significant adverse indirect impact to the total and active open space resources in the 0.5-mile Residential Study Area. The Proposed Actions would lead to a reduction in total and active open space ratios and exacerbate the extent to which the current active and total open space ratios in the Residential Study Area fall below City guidelines.</u>

To avoid this significant adverse indirect impact, the total amount of open space created in the With-Action Condition would need to increase by approximately 6.15 acres, including 2.37 acres of active open space. Alternatively, the number of dwelling units that could be developed on the Projected Development Sites would have to be *reduced* to 1,601 dwelling units from 2,569 dwelling units—an approximately 38 percent decrease (968 fewer dwelling units).

Measures considered to mitigate the Proposed Actions' significant adverse open space impact include: developing a new recreation center at the Lyons Pool site; making improvements to existing parks to allow for expanded programming and enhanced usability; making New York City public school playgrounds accessible to the community after school hours through the Schoolyards to Playgrounds program; and public realm improvements in the vicinity of the intersection of Victory Boulevard and Bay Street. These potential mitigation measures were explored in coordination with the lead agency, DPR, DOE, DOT and EDC between the DEIS and the FEIS.

Based on these discussions, the following mitigation measure has been identified for implementation:

• Public realm and pedestrian improvements at underutilized street space located at the intersection of Victory Boulevard and Bay Street: These improvements will provide an enhanced pedestrian realm at a critical gateway to the Bay Street Corridor. They will consist of amenities such as benches, lighting, trees and planting to encourage pedestrian activity, support access to public transit, and improve the streetscape. The proposed public realm improvements are anticipated to total at least 0.13 acres.

Other measures have been identified that could substantially enhance and/or increase the amount of open space resources for the additional population introduced by the Proposed Actions. If funded and implemented, these measures could further mitigate the significant adverse open space impact.

- Development of a new recreation center at the Lyons Pool site, as identified by NYC Parks in the recently completed North Shore Staten Island Recreation Center Feasibility Study: If implemented, this facility would provide a significant complement of active recreational amenities and could add approximately 1 acre of new active recreation.
- Creating a publicly accessible playground at a school proposed to be located at the Stapleton Waterfront site: As described in Chapter 22 of this FEIS, an Alternative to the Proposed Actions has been submitted which would waive from floor area calculations up to 100,000 sf for a school use at Stapleton Waterfront Phase III. If this Alternative is adopted, construction of a new school on Site A is anticipated to include an at-grade playground that would be open to the public during non-school hours. This would provide new active open space to the community in close proximity to an area where significant residential development is projected at Stapleton Waterfront.

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• Improvements to study area open space resources: Improvements to sites, such as converting Village Hall at Tappen Park to park use and/or enhancing park components at existing parks, could help to qualitatively improve open space for current and future residents. The scope of improvements to study area open space resources would be contingent upon available funds and the deficiencies or needs specific to the open space resource.

Although these additional measures could substantially enhance and increase the usability of open space resources and partially mitigate the significant adverse open space impact in the With-Action Condition, capital and expense of funding to build and maintain additional open space or park facilities has not been identified at this point in time. Consequently, the Proposed Actions' significant adverse indirect open space impact would not be completely eliminated and, as a result, an unavoidable significant adverse open space impacts would occur avenues to implement the measures identified along with other opportunities to create new publicly-accessible open space resources, improve existing open spaces, and/or provide additional programming within existing open spaces.

# E. HISTORIC AND CULTURAL RESOURCES

As discussed in Chapter 7, "Historic and Cultural Resources," the construction activity at Projected Development Site 5 under the With-Action Condition has the potential to result in significant adverse archaeological impacts associated with prehistoric resources and nineteenth- to early twentieth-century waterfront features.

A Phase 1A study of Potential Development Site 5 was completed in May 2017 (Appendix E). The Phase 1A study concluded that the archaeological area of potential effects (APE) has a moderate to high sensitivity for prehistoric resources on the western margin in the limited area of fast land, and a moderate to high sensitivity for nineteenth- to early-twentieth-century waterfront features (docks or piers) in the remainder of the southern archaeological-APE. The northern, narrow portion of the archaeological-APE was identified as having no to low sensitivity for shoreline features. The Phase IA recommended archaeological testing in advance of any future ground disturbing developments within the two areas of archaeological sensitivity to determine the absence or presence of potential buried resources.

However, as Projected Development Site 5 is owned by a private entity, there is no mechanism in place to require a developer to conduct archaeological testing or require the preservation or documentation of archaeological resources, should they exist. Therefore, a significant adverse effect related to archaeological resources may occur on Projected Development Site 5. Because there is no mechanism to avoid or mitigate potential impacts to archaeological resources at the privately-owned Projected Development Site 5, the significant adverse impact would be unavoidable.

# F. TRANSPORTATION

As described in Chapter 14, "Transportation," a number of elements in the study area would experience significant adverse traffic, transit, and pedestrian impacts as a result of the Proposed Actions under the reasonable worst-case development scenario. The transportation analyses provide a conservative assessment of the With-Action condition. The discussion below outlines readily implementable mitigation measures that would fully or partially mitigate the identified impacts. The

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implementation of these measures would be conducted in coordination with the DOT as development proceeds.

As detailed in the "Operational Analysis Methodology" section of Chapter 14, the operation of an intersection is defined in terms of control delay per vehicle and the corresponding level-of-service (LOS) and volume-to-capacity (v/c) ratio. The criteria used for defining significant adverse impacts are based on a sliding scale for various LOS and delay measures. A significant adverse impact is considered to be fully mitigated when the projected delay for an intersection lane group or movement under the With-Action condition is brought back to within an acceptable range of its No-Action condition level or to marginally acceptable mid-LOS D (45.0 seconds for signalized intersections and 30.0 seconds for unsignalized intersections). In some cases, viable mitigation measures for a particular movement could result in additional delay or LOS deterioration for other movements. Such increases in delay and deterioration in LOS do not constitute a significant adverse impact as long as the mid-LOS D threshold is not exceeded, or the increase in delay does not exceed the limits of the sliding scale mentioned above.

#### PROPOSED SCHEDULE FOR TRAFFIC AND PEDESTRIAN MITIGATION MEASURES

Subject to the approval of DOT, the mitigation measures summarized in Table 21-5 and Table 21-20 would be implemented to mitigate the significant adverse traffic and pedestrian impacts resulting from full build-out of the Proposed Actions in 2030. However, as the development of the Proposed Actions would be expected to occur over an approximately 11-year period, it is possible that some of the significant adverse traffic and pedestrian impacts could occur prior to full build-out. In collaboration, DCP as lead agency and DOT have developed a Traffic Monitoring Program (TMP) that would be implemented if the Proposed Actions are approved, to verify the need and effectiveness of the proposed mitigation measures.

## **Construction and Operation**

As new development under the Proposed Actions would be expected to take place over an approximate 11-year timeframe (through the year 2030), transportation monitoring will be performed as a multi-tiered process. The TMP's construction monitoring phase would begin before the construction of the first three sites projected as a result of the Proposed Actions, i.e., Projected Development Sites 3, 9 and 22. These sites were chosen because they are anticipated to begin construction soon after the Proposed Actions are approved. The data collection and analyses of the construction phase of the TMP will focus on construction peak hours and whether portions of the mitigation proposed for the full project build out would be warranted for installation during the construction of these three sites.

The City will begin to implement the operational portion of the TMP once either (1) buildings on Projected Development Sites 3, 9 and 22 are built and occupied; or (2) a net increase of approximately 500,000 square feet (sf) of total new development on projected or potential development sites is reached within the proposed rezoning area, whichever occurs first. DCP would track when new developments come online and would be responsible for identifying when the need to begin the operational TMP will be triggered. This phase of the TMP would begin with travel demand surveys, which would provide the most up-to-date representation of site-generated trips and travel behavior within the proposed rezoning area and to compare these findings with the assumptions studied in

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<u>Chapter 14, "Transportation" of the FEIS, to determine the extent to which future volume projections presented in the FEIS may occur.</u>

If the new travel demand surveys indicate that the FEIS projections of trip generation rates and modal splits are accurate or greater than projected in the FEIS, a Level 1 and Level 2 CEQR screening assessment would be conducted, detailing the trip generation resulting from the developed projected/potential sites, as well as vehicular and pedestrian network assignments. This analysis would also incorporate an updated vehicular and pedestrian safety assessment. DOT will then determine whether subsequent steps should involve field data collection (traffic and pedestrian counts, field inventories and observations, etc.) and analysis focusing on traffic and pedestrian conditions at affected locations/elements, as well as signal warrant studies, to determine whether proposed mitigation measures (including any new traffic signals) are warranted and/or whether additional or new measures should be considered. If the results of the analysis confirm the mitigation measures identified in the FEIS (or identify alternative mitigation measures that may be more appropriate), these mitigation measures would be discussed by DOT and DCP.

If new travel demand surveys indicate that the FEIS projections are overestimated (i.e., the projected traffic and pedestrian volumes are less than the FEIS projections), the next verification would take place after another 500,000 sf of total new development on projected or potential development sites is reached within the proposed rezoning area. The scope of subsequent monitoring phases would be determined by DCP and DOT based on the results of previous phases. Upon mutual agreement by DOT and DCP, it may be determined that a different threshold for determining future monitoring may be more appropriate.

## **TRAFFIC**

As described in Chapter 14, "Transportation," the Proposed Actions would result in significant adverse traffic impacts at 31 study area intersections during one or more analyzed peak hours, with 24, 21, 26, and 20 impacted intersections during the Weekday AM, MD, PM, and Saturday MD peak hours, respectively.

As demonstrated below, some of these impacts could be mitigated through the implementation of traffic engineering improvements, including:

- Installation of new traffic signals:
- Modification of traffic signal phasing, timing, and/or offsets;
- Elimination of on-street parking within 100 feet of intersections to add a limited travel lane, known as "daylighting";
- Channelization, changes to lane markings, and the addition of new turn bays to make more efficient use of available street widths; and
- Implementing turn restrictions.

The types of mitigation measures proposed herein are standard measures that are routinely identified by the City and considered feasible for implementation. Table 21-<u>5</u> summarizes the recommended mitigation measures for each of the intersections with significant adverse traffic impacts during the Weekday AM, MD, PM, and Saturday MD peak hours. Implementation of the recommended traffic engineering improvements is subject to review and approval by DOT and will

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be based on the results of a traffic monitoring program (TMP), developed by DCP, in coordination with DOT. DCP, as lead agency, <u>has explored</u> further mitigation measures and developed the <u>initial</u> scope of work for the TMP. If, prior to implementation, DOT determines that an identified mitigation measure is infeasible, an alternative and equivalent mitigation measure will be considered. <u>However</u>, if no other alternative mitigation measures can be identified, those impacts would be unmitigated.

#### FULLY MITIGATED SIGNIFICANT ADVERSE TRAFFIC IMPACTS

The potential significant adverse traffic impacts at the following study locations would be fully mitigated through the reallocation of green time. The specific signal timing changes for each study intersection are outlined in Table 21-5.

- Richmond Terrace and Hamilton Avenue (Intersection 5 on Figure 14-6)
- Front Street and Hannah Street (Intersection 14 on Figure 14-6)
- Van Duzer Street and Beach Street (Intersection 27 on Figure 14-6)
- Bay Street and Edgewater Drive (Intersection 47 on Figure 14-6)

The potential significant adverse traffic impacts at the following study locations would be fully mitigated through the reallocation of green time and modified offsets. Changing intersection offsets affects how traffic flows between adjacent intersections along a corridor and can be effective at reducing queue delay. The specific signal timing and offset changes for each study intersection are outlined in Table 21-5.

- Richmond Terrace and Franklin Avenue (Intersection 1 on Figure 14-6)
  - A potential significant adverse traffic impact is not expected at this intersection during the Weekday MD peak hour; however, due to proposed signal timing changes at Richmond Terrace and Jersey Street, it is recommended that the offset and signal timing at this intersection be modified to avoid the potential for a new significant adverse impact.
- Richmond Terrace and Westervelt Avenue (Intersection 3 on Figure 14-6)
  - o Proposed signal timing changes at Richmond Terrace and Jersey Street would resolve the potential significant adverse traffic impact expected at this intersection during the Weekday AM and MD peak hours; therefore, no additional mitigation measures are recommended.
- Bay Street and Slosson Terrace (Intersection 10 on Figure 14-6)
- Bay Street and Clinton Street (Intersection 20 on Figure 14-6)
- Broad Street and Targee Street (Intersection 43 on Figure 14-6)

Table 21-<u>5</u>: Proposed Traffic Mitigation Table

	Intersection		Week	day AM	Peak Hour			Week	day MI	O Peak Hour			<u>Weekday F</u>	M Peak Hour			<u>Saturd</u>	ay MD Peak Hour	
		Impacts	Movement No-Action WB LT 37.3 D	80.3	th-Action	Mitigated 42.5 D	Movement WB LT	No-Action 11.8 B	35.5	Vith-Action D	Mitigated 37.5 D	Movement WB LT	No-Action 81.4 F 253.0	With-Action F + 73	Mitigated 3.8 E	Movement	No-Action	With-Action	Mitigated
		Mitigation Description	Shift 2 seconds from NB phase to seconds.										om NB phase to EB / WB	L					
	Disharand Tanasa and		No-Action/With-Action		Mit	tigated	No-Acti	on/With-Action		M	litigated	No-Act	ion/With-Action	Mitiga	ated				
1	Richmond Terrace and Franklin Avenue		G A	R		G A R		G A	R		G A R		G A R		G A R				
		0	<b>EB / WB</b> 79.0 3.0	2.0	EB / WB	81.0 3.0 2.0	EB/WB	79.0 3.0	2.0	EB / WB	80.0 3.0 2.0	WB/EB	79.0 3.0 2.0	EB / WB 86	3.0 2.0				
		Signal Timing Mitigation	<b>NB</b> 31.0 3.0	2.0	NB	29.0 3.0 2.0	NB	31.0 3.0	2.0	NB	30.0 3.0 2.0	NB	31.0 3.0 2.0	NB 24	1.0 3.0 2.0				
			Offset 56	sec	Offset	28 sec	Offset	60	sec	Offset	51 sec	Offset	60 sec	Offset	60 sec				
			Cycle Length 120	sec	Cycle Length	n 120 sec	Cycle Leng	th 120	sec	Cycle Leng	th 120 sec	Cycle Len	gth 120 sec	Cycle Length	120 sec				
-																			
			Movement No-Action  EB L 87.4 F	208.5	th-Action F +	Mitigated 68.7 E	Movement	No-Action	V	Vith-Action	Mitigated	Movement EB L	No-Action 39.2 D 48.3	With-Action D + 33	Mitigated 3.9 C	Movement	No-Action	With-Action	Mitigated
			WB LT 68.6 E	110.7	F +	08.7 L	WB LT	227.7 F	337.5	F +		WB LT	163.2 F 353.4		5.9 C	WB LT	78.1 E	113.9 F +	
		Impacts	WB R 7.7 A	9.0	Α		WBR	8.5 A	8.3	A +		WBR	11.1 B 9.8			WBR	9.9 A	12.4 B	
			WB L	0.0		9.9 A	WB L	0.0 7.	0.0	,,	17.8 B	WBL	5 0.0		3.6 B	WBL	0.0 /1	12.1	13.8 B
			WB TR			37.9 D	WB TR				42.8 D	WB TR		77	7.6 E +	WB TR			44.4 D
2	Richmond Terrace and Jersey Street	Mitigation Description	Re-stripe WB approach as one 10' from NB / SB phase to EB / WB ph Change offset from 97 seconds to	ase. Shift 1				e to EB / WB ph	ase. Shift	1 second from EBL	or 100'. Shift 6 seconds lead phase to EB / WB		re-stripe WB approach as om NB / SB phase to EB			Re-stripe WB app	oach as one 10' L	lane and one 11' TR lane f	or 100'.
	bersey officer		No-Action/With-Action		Mit	tigated	No-Acti	on/With-Action		M	litigated	No-Act	ion/With-Action	Mitiga	ated	No-Acti	on/With-Action	N	Mitigated
			G A	R	_	G A R		G A	R		G A R		G A R		G A R		G A	R	G A R
			EBL 10.0 3.0	2.0	EBL	11.0 3.0 2.0	EBL	9.0 3.0	2.0	EBL	8.0 3.0 2.0	EBL	8.0 3.0 2.0	EBL 8	.0 3.0 2.0	EBL	10.0 3.0	2.0 <b>EBL</b>	10.0 3.0 2.0
		Signal Timing Mitigation	<b>EB / WB</b> 65.0 3.0	2.0	EB / WB	69.0 3.0 2.0	EB/WB	64.0 3.0	2.0	EB / WB		EB / WB		-	9.0 3.0 2.0	EB / WB	40.0 3.0	2.0 <b>EB / WB</b>	
			<b>NB / SB</b> 30.0 3.0	2.0	NB / SB	25.0 3.0 2.0	NB/SB	32.0 3.0	2.0	NB / SB	26.0 3.0 2.0	NB / SB	30.0 3.0 2.0	NB / SB 28	3.0 3.0 2.0	NB / SB	25.0 3.0	2.0 <b>NB/SB</b>	25.0 3.0 2.0
			Offset 97		Offset	83 sec	Offset	34		Offset	113 sec	Offset	34 sec	Offset	31 sec	Offset	60	sec Offset	60 sec
L			Cycle Length 120	sec	Cycle Length	n 120 sec	Cycle Leng	th 120	sec	Cycle Leng	th 120 sec	Cycle Len	gth 120 sec	Cycle Length	120 sec	Cycle Leng	th 90	sec Cycle Leng	gth 90 sec
Г			Movement No-Action	Wi	th-Action	Mitigated	Movement	No-Action	Ιν	Vith-Action	Mitigated	Movement	No-Action	With-Action	Mitigated	Movement	No-Action	With-Action	Mitigated
		Impacts	Movement No Action		ui Addon	mingated	movement	NO AUGION		THE ACTION	mingatea	EB TR	25.8 C 47.9		2.2 C	Movement	TO ACTOR	Willi Addon	imingatea
		·	<b>WB LT</b> 47.0 D	88.8	F +	43.2 D	WB LT	71.4 E	80.8	F +	31.1 C	WB LT	78.1 E 101.3	F + 80	).5 F				
		Mitigation Description	Mitigation measures at nearby inte	rsections res	solved the potential	l impact.	Mitigation measure	es at nearby inte	rsections r	esolved the potentia	al impact.	Shift 2 seconds fr seconds.	om NB phase to EB / WB	phase. Change offset fro	m 23 seconds to 51				
3	Richmond Terrace and Westervelt Avenue		No-Action/With-Action		Mit	tigated	No-Acti	on/With-Action		M	litigated	No-Act	ion/With-Action	Mitiga	ated				
			G A	R	_	G A R		G A	R		G A R	_	G A R		3 A R				
		Signal Timing Mitigation	EB / WB 73.0 3.0	2.0	EB / WB	73.0 3.0 2.0	EB/WB	73.0 3.0	2.0	EB / WB		EB / WB		_	5.0 3.0 2.0				
		g a gamen	NB 37.0 3.0	2.0	NB	37.0 3.0 2.0	NB	37.0 3.0	2.0	NB	37.0 3.0 2.0	NB	37.0 3.0 2.0	NB 35					
			Offset 93		Offset	93 sec	Offset	23		Offset	23 sec	Offset	23 sec	Offset	51 sec				
			Cycle Length 120	sec	Cycle Length	n 120 sec	Cycle Leng	th 120	sec	Cycle Leng	th 120 sec	Cycle Len	gth 120 sec	Cycle Length	120 sec				

Table 21-5: Proposed Traffic Mitigation Table (con't)

	Intersection		Weekday All	// Peak Hour	Weekday MI	O Peak Hour	Weekday P	M Peak Hour	Saturday ME	O Peak Hour
		Impacts	Movement No-Action V	Vith-Action Mitigated	Movement No-Action V	Vith-Action Mitigated	Movement No-Action	With-Action Mitigated	Movement         No-Action         W           NB LT         31.4         C         53.2	Vith-Action Mitigated D + 43.6 D
		Mitigation Description							Shift 1 second from the pedestrian phase to N	NB / SB phase.
_	Hamilton Avenue and								No-Action/With-Action	Mitigated
5	Richmond Terrace								G A R	G A R
		Signal Timing Mitigation							NB / SB 45.0 3.0 2.0	NB / SB 46.0 3.0 2.0
									All Peds   35.0   3.0   2.0   Offset   60   sec	All Peds 34.0 3.0 2.0  Offset 60 sec
									Offset 60 sec  Cycle Length 90 sec	Offset 60 sec  Cycle Length 90 sec
L									, ,	, ,
Ī			Movement No-Action V	Vith-Action Mitigated		Vith-Action Mitigated	Movement No-Action	With-Action Mitigated	Movement No-Action V	Vith-Action Mitigated
		Impacts			<b>WB L</b> 134.0 F 139.4	F + 139.4 F +	<b>NB T</b> 75.4 E 80.1	F + 80.1 F +		
					<b>SBT</b> 65.2 E 82.4	F + 82.4 F +	SBT 80.1 F 87.1	F + 80.1 F + F + 87.1 F +	<b>SBT</b> 27.3 C 46.0	D + 46.1 D +
					-			1 -	-	<u> </u>
		Mitigation Description	Shift 1 second from WB phase to NB / SB ph	ase to mitigate impact at intersection #9.	Unmiti	igable	Unmi	tigable	Unmiti	gable
8	Richmond Terrace and Ferry Terminal (bus)		No-Action/With-Action	Mitigated	No-Action/With-Action	Mitigated	No-Action/With-Action	Mitigated	No-Action/With-Action	Mitigated
			G A R	G A R	G A R	G A R	G A R	G A R	G A R	G A R
		0	WB 27.0 3.0 2.0  All Peds 23.0 3.0 2.0	WB 26.0 3.0 2.0  All Peds 23.0 3.0 2.0	WB 10.0 3.0 2.0  All Peds 23.0 3.0 2.0	WB         10.0         3.0         2.0           All Peds         23.0         3.0         2.0	WB 27.0 3.0 2.0  All Peds 23.0 3.0 2.0	WB         27.0         3.0         2.0           All Peds         23.0         3.0         2.0	WB 10.0 3.0 2.0  All Peds 23.0 3.0 2.0	WB 10.0 3.0 2.0  All Peds 23.0 3.0 2.0
		Signal Timing Mitigation	NB / SB 55.0 3.0 2.0	NB / SB 56.0 3.0 2.0	NB/SB 42.0 3.0 2.0	NB/SB 42.0 3.0 2.0	NB / SB 55.0 3.0 2.0	NB / SB 55.0 3.0 2.0	NB / SB 42.0 3.0 2.0	NB / SB
			Offset 21 sec	Offset 21 sec	Offset 45 sec	Offset 45 sec	Offset 95 sec	Offset 95 sec	Offset 45 sec	Offset 45 sec
			Cycle Length 120 sec	Cycle Length 120 sec	Cycle Length 90 sec	Cycle Length 90 sec	Cycle Length 120 sec	Cycle Length 120 sec	Cycle Length 90 sec	Cycle Length 90 sec
r										
		Impacts	Movement         No-Action         V           NB T         39.0         D         51.5	Vith-Action Mitigated D + 34.2 C	Movement         No-Action         V           NB T         64.6         E         91.1	Vith-Action Mitigated F + 92.2 F +	Movement         No-Action           NB T         208.0 F         260.0	With-Action Mitigated F + 261.1 F +	Movement         No-Action         V           NB T         70.9         E         77.3	Vith-Action Mitigated E + 77.3 E +
		impacts			<b>SB TR</b> 69.4 E 93.8	F + 93.8 F +	<b>SB TR</b> 55.7 E 64.5	E + 64.5 E +	<b>SB TR</b> 130.3 F 158.4	F + 158.4 F +
	,	Mitigation Description	Shift 1 second from SB / WB R phase and 1 to NB / SB R phase.	second from WB / NB R phase	Unmiti	igable	Unmi	tigable	Unmiti	igable
	Richmond Terrace and		No-Action/With-Action	Mitigated	No-Action/With-Action	Mitigated	No-Action/With-Action	Mitigated	No-Action/With-Action	Mitigated
9	Ferry Terminal (parking lot)		G A R	G A R	G A R	G A R	G A R	G A R	G A R	G A R
			WB / NB R 27.0 3.0 2.0	WB / NB R 26.0 3.0 2.0  All Peds 23.0 3.0 2.0	WB / NB R         10.0         3.0         2.0           All Peds         23.0         3.0         2.0	WB / NB R 10.0 3.0 2.0  All Peds 23.0 3.0 2.0	WB / NB R 27.0 3.0 2.0	WB / NB R 27.0 3.0 2.0	WB/NBR 10.0 3.0 2.0	WB / NB R 10.0 3.0 2.0  All Peds 23.0 3.0 2.0
		Signal Timing Mitigation	All Peds         23.0         3.0         2.0           SB / WB R         24.0         3.0         2.0	All Peds 23.0 3.0 2.0 SB / WB R 23.0 3.0 2.0	All Peds 23.0 3.0 2.0 SB / WB R 8.0 3.0 2.0	All Peds 23.0 3.0 2.0 SB / WB R 8.0 3.0 2.0	All Peds         23.0         3.0         2.0           SB / WB R         21.0         3.0         2.0	All Peds 23.0 3.0 2.0 SB/WB R 21.0 3.0 2.0	All Peds         23.0         3.0         2.0           SB/WB R         9.0         3.0         2.0	All Peds         23.0         3.0         2.0           SB / WB R         9.0         3.0         2.0
			NB/SBR 26.0 3.0 2.0	NB/SBR 28.0 3.0 2.0	NB / SB R 29.0 3.0 2.0	NB / SB R 29.0 3.0 2.0	NB/SBR 29.0 3.0 2.0	NB / SB R 29.0 3.0 2.0	NB / SB R 28.0 3.0 2.0	NB / SB R 28.0 3.0 2.0
			Offset 21 sec	Offset 21 sec	Offset 45 sec	Offset 45 sec	Offset 95 sec	Offset 95 sec	Offset 45 sec	Offset 45 sec
			Cycle Length 120 sec	Cycle Length 120 sec	Cycle Length 90 sec	Cycle Length 90 sec	Cycle Length 120 sec	Cycle Length 120 sec	Cycle Length 90 sec	Cycle Length 90 sec

Table 21-5: Proposed Traffic Mitigation Table (con't)

	Intersection		Weekday AM Peak Hour	Weekday MD Peak Hour	Weekday PM Peak Hour	Saturday MD Peak Hour
		Impacts	Movement         No-Action         With-Action         Mitigated           NB L         30.0 C         89.9 F + 42.2 D	Movement         No-Action         With-Action         Mitigated           NB L         31.2         C         50.0         D         +         32.4         C	Movement         No-Action         With-Action         Mitigated           NB T         46.1         D         64.1         E         +         33.0         C	Movement No-Action With-Action Mitigated
		Mitigation Description	Shift 11 seconds from NB / SB phase to the NB L lead phase.	SB TR 103.1 F 122.1 F + 95.2 F  Shift 2 seconds from EB phase to NB / SB phase. Shift 1 second from EB phase to NB L lead phase.	SB TR 95.5 F 125.6 F + 97.9 F  Shift 3 seconds from the NB L lead phase to NB / SB phase. Change offset from 48 to 52 seconds.	SB TR         142.3         F         162.7         F         +         135.3         F           Shift 2 seconds from EB phase to NB / SB phase.
10	Bay Street and Slosson Terrace	Signal Timing Mitigation	No-Action/With-Action	No-Action/With-Action	No-Action/With-Action	No-Action/With-Action
	,	Impacts	Movement No-Action With-Action Mitigated	Movement No-Action With-Action Mitigated	Movement         No-Action         With-Action         Mitigated           WB T         37.6         D         62.5         E         +         59.7         E         +           SB R         84.4         F         98.1         F         +         98.1         F         +	Movement No-Action With-Action Mitigated
11	Victory Boulevard and Bay Street/St. Marks Place	Mitigation Description  Signal Timing Mitigation	No-Action/With-Action   G A R   EB / WB   74.0   3.0   2.0   LPI   5.0   2.0   0.0   SB   29.0   3.0   2.0   Offset   13   sec   Cycle Length   120   sec   Cycle Length   120   sec   Cycle Length   120   sec   Sec		No-Action/With-Action	
		Impacts	Movement         No-Action         With-Action         Mitigated           EB L         31.3         C         49.9         D         +         41.3         D           NB L         32.8         C         97.3         F         +         44.6         D	Movement         No-Action         With-Action         Mitigated           EB L         31.5         C         60.2         E         +         104.3         F         +           EB LT         30.6         C         41.1         D         67.0         E         +           WB LTR         26.7         C         228.6         F         +         381.3         F         +           NB L         829.5         F         1204.3         F         +         323.1         F           SB LT         41.9         D         126.2         F         +         143.9         F         +           SB R         93.8         F         90.4         F         159.3         F         +	Movement         No-Action         With-Action         Mitigated           EB L         72.0         E         83.1         F         +         85.0         F         +           EB LT         72.9         E         95.2         F         +         91.3         F         +           WB LTR         57.8         E         756.6         F         +         573.1         F         +           NB L         577.1         F         1255.3         F         +         522.7         F           SB LT         14.1         B         55.4         E         +         183.6         F         +	Movement         No-Action         With-Action         Mitigated           WB LTR         24.2         C         49.2         D         +         37.3         D           NB L         1,171.5         F         1,549.4         F         +         377.0         F           SB LT         43.6         D         72.4         E         +         231.9         F         +
12	Victory Boulevard and Bay Street	Mitigation Description	to 0 seconds.  No-Action/With-Action Mitigated	WB phase to create a leading NB left-turn phase. Change the offset from 45 seconds to 4 seconds.  No-Action/With-Action  Mitigated	from 48 seconds to 80 seconds.  No-Action/With-Action Mitigated	turn phase and shift 2 seconds from NB / SB phase to EB / WB phase. Change the offset from 45 seconds to 0 second.  No-Action/With-Action Mitigated
		Signal Timing Mitigation	G         A         R         G         A         R           EB/WB         35.0         3.0         2.0         EB/WB         37.0         3.0         2.0           LPI         5.0         2.0         0.0         LPI         5.0         2.0         0           NB L         NB L         18.0         3.0         2.0           NB/SB         68.0         3.0         2.0         NB/SB         43.0         3.0         2.0           Offset         100         sec         Offset         0         sec	LPI         5.0         2.0         0         LPI         5.0         2.0         0           NB L         NB L         6.0         3.0         2.0           NB/SB         44.0         3.0         2.0         NB/SB         37.0         3.0         2.0	G         A         R         G         A         R           EB/WB         35.0         3.0         2.0         EB/WB         39.0         3.0         2.0           LPI         5.0         2.0         0         LPI         5.0         2.0         0           NB L         NB L         6.0         3.0         2.0           NB/SB         68.0         3.0         2.0         NB/SB         53.0         3.0         2.0           Offset         48         sec         Offset         80         sec	G         A         R         G         A         R           EB / WB         29.0         3.0         2.0         EB / WB         31.0         3.0         2.0           LPI         5.0         2.0         0         LPI         5.0         2.0         0           NB L         NB L         6.0         3.0         2.0           NB / SB         31.0         3.0         2.0           Offset         45         sec         Offset         0         sec
			Cycle Length 120 sec Cycle Length 120 sec	1 111	Cycle Length 120 sec Cycle Length 120 sec	Cycle Length 90 sec Cycle Length 90 sec

Table 21-5: Proposed Traffic Mitigation Table (con't)

	Intersection			Week	day AM	l Peak Hour				<u>Week</u>	day MD	Peak Hour			<u>Week</u>	day PM	l Peak Hour			<u>Satur</u>	day MD	Peak Hour	
Г			Movement	No-Action	W	ith-Action	Mitiga	ted	Movement	No-Action	W	ith-Action	Mitigated	Movement	No-Action	W	ith-Action	Mitigated	Movement	No-Action	Wit	h-Action	Mitigated
			WB LTR	56.7 E	117.1	F +	58.7 E							WB LTR	58.9 E	122.3	F +	55.5 E					
			NB LTR	82.4 F	158.2	F +			NB LTR	394.1 F	488.8	F +		NB LTR	118.7 F	208.7	F +		NB LTR	217.9 F	290.2	F +	
		Impacts	NB L				41.8 D		NB L				66.8 E	NB L				42.8 D	NB L				28.4 C
			NB TR				98.5 F		NB TR				92.9 F	NB TR		+		89.5 F	NB TR		<del>                                     </del>		58.7 E
			SB L	284.4 F	798.1		255.8 F	•	SB L	1,675.8 F	2255.1	Е.	653.3 F	SB L	711.6 F	1,404.1	F +	667.8 F	SBL	1,064.7 F	1,760.5		529.8 F
13	Bay Street and Hannah Street	Mitigation Description	Partial mitigation: permanent curb ex bay) and eliminate direction: modify I extension. Re-allo	Reconfigure soutly tension, one 5' be parking to Swan DOT proposed parcate 15 seconds is second from NB	h leg of the ike lane, tv Street (12 vement ma from NB / S	e intersection - NB ap wo 11' TR lanes, one 5', approximately 6 p arkings and create pe SB phase to create a e to EB / WB phase.	proach: add 11' L lane (7 arking space rmanent curl lagging NB	5' turn es) - SB b / SB left-	Reconfigure south extension, one 5' parking to Swan S proposed pavements	n leg of the interse bike lane, two 11' Street (125', appro ent markings and / SB phase and 1	ection - NB TR lanes, eximately 6 create pern	parking spaces) - S nanent curb extens	ermanent curb turn bay) and eliminate SB direction: modify DOT on. Re-allocate 10 to create a lagging NB /	Reconfigure soutl extension, one 5' parking to Swan S proposed paveme seconds from NB	h leg of the interse bike lane, two 11' Street (125', appro ent markings and / SB phase to cre	ection - NB TR lanes, eximately 6 create permeate a laggin	parking spaces) - nanent curb extens ng NB / SB left-tur	<u> </u>	Reconfigure soutl extension, one 5' parking to Swan S proposed paveme seconds from NB	n leg of the interse bike lane, two 11' Street (125', appro ent markings and / SB phase and 2	ection - NB a TR lanes, o oximately 6 p create perma	pproach: add a per ne 11' L lane (75' tu arking spaces) - SE anent curb extensio	manent curb rn bay) and eliminate direction: modify DOT n. Re-allocate 9 o create a lagging NB
			No-Acti	ion/With-Action		Miti	gated		No-Act	ion/With-Action		М	tigated	No-Act	tion/With-Action		N	litigated	No-Act	ion/With-Action		Miti	gated
				G A	R		G A	R		G A	R		G A R		G A	R		G A R		G A	R		G A R
			EB / WB	37.0 3.0	2.0	EB / WB	45.0 3.0	2.0	EB/WB	35.0 3.0	2.0	EB / WB	34.0 3.0 2.0	EB/WB	37.0 3.0	2.0	EB/WB	45.0 3.0 2.0	EB/WB	35.0 3.0	2.0	EB/WB	33.0 3.0 2.0
		Signal Timing Mitigation	NB/SB	73.0 3.0	2.0	NB/SB	50.0 3.0	2.0	NB/SB	45.0 3.0	2.0	NB / SB	35.0 3.0 2.0	NB/SB	73.0 3.0	2.0	NB / SB	48.0 3.0 2.0	NB/SB	45.0 3.0	2.0	NB/SB	36.0 3.0 2.0
			NB L / SB L			NB L / SB L	10.0 3.0	2.0	NBL/SBL			NB L / SB L	6.0 3.0 2.0	NBL/SBL			NB L / SB L	12.0 3.0 2.0	NBL/SBL			NB L / SB L	6.0 3.0 2.0
			Offset	101	sec	Offset	10		Offset	53	sec	Offset	50 sec	Offset	15	sec	Offset	23 sec	Offset	53	sec	Offset	45 sec
			Cycle Leng			Cycle Length	120		Cycle Leng		sec	Cycle Lengt		Cycle Len			Cycle Leng		Cycle Len		sec	Cycle Length	90 sec
L						.,				,		.,					.,			,			
Г			Movement	No-Action	W	ith-Action	Mitiga	ted	Movement	No-Action	W	ith-Action	Mitigated	Movement	No-Action	W	ith-Action	Mitigated	Movement	No-Action	Wit	h-Action	Mitigated
		Impacts							NB LR	23.1 C	45.8	D +	40.8 D										
		Mitigation Description							Shift 1 second fro	m EB / WB phase	e to NB pha	ise.											
14	Front Street and Hannah Street								No-Act	ion/With-Action		M	tigated										
	Haillan Steet	Signal Timing Mitigation				F		Η	EB/WB NB	G     A       43.0     3.0       37.0     3.0		EB/WB	G         A         R           42.0         3.0         2.0           38.0         3.0         2.0									F	
									Offset	0	sec	Offset	0 sec										
L									Cycle Len	jth 90	sec	Cycle Lengt	h 90 sec										
г			Movement	No-Action	l w	lith-Action	Mitiga	tod	Movement	No-Action	100	ith-Action	Mitigated	Movement	No-Action		lith-Action	Mitigated	Movement	No-Action	NA/S	h-Action	Mitigated
			EB L	125.1 F	128.3		119.2 F	leu	Wovement	NO-ACTION	**	IIII-ACTIOII	Miligated	EB L	70.6 E	114.9	F +	115.7 F +	Wovement	NO-ACTION	VVI	II-Action	Witigated
		Impacts	ED E	120.1	120.5	1	119.2 1							EB LTR	65.9 E	115.4	F +	116.1 F +					
	Bay Street and	Mitigation Description	Shift 6 seconds fro to 80 seconds.	om NB / SB phase	e to EB / W	/B phase. Change of	set from 95	seconds						EBEIK	00.9	Unmitig		110.1					
15	Swan Street/Van Duzer Street		No-Acti	ion/With-Action		Miti	gated							No-Act	tion/With-Action		N	litigated					
	Silver	Signal Timing Mitigation	EB / WB NB / SB Offset	G A 37.0 3.0 73.0 3.0 95	2.0 2.0 sec	-	G A 43.0 3.0 67.0 3.0	2.0						EB / WB NB / SB Offset		2.0	EB / WB NB / SB Offset	G         A         R           37.0         3.0         2.0           73.0         3.0         2.0           21         sec				F	
			Cycle Leng	jth 120.0	sec	Cycle Length	120.	0 sec						Cycle Len	gth 120.0	sec	Cycle Leng	th 120.0 sec					
															-								

Table 21-5: Proposed Traffic Mitigation Table (con't)

	Intersection			Weekda	ay AM Peak Ho	<u>our</u>			Weekda	y MD Peak Ho	<u>ır</u>			Weekd	ay PM Pea	ak Hour			Saturda	ay MD Peak	<u>Hour</u>	
18	Bay Street and Grant Street	Impacts  Mitigation Description		No-Action  Signalize intersection	With-Action  n. Signal warrant #4	42.8 36.4 7.2 76.8	D D A E +		No-Action  ignalize intersection	With-Action  . Signal warrant #4 is	Mitigated   28.5   C   28.6   C     5.7   A     272.7   F     met.   Mitigated	+	Movement  EB LTR  WB R  NB TR  SB T  Partial mitigation: Si	No-Action  ignalize intersecti	With-Ad	ant #4 is met.	Mitigated  40.8 D  38.1 D  6.1 A  231.6 F +	-	No-Action  Signalize intersection  No-Action	With-Actio	29.8 29.1 10.8 233.0	C B F +
		Signal Timing Mitigation		nsignalized		G WB 28.0	A R 3.0 2.0 3.0 2.0 99 sec 120 sec		ignalized	EB / W NB / S Offs Cycle Le	G A B 22.0 3.0 B 58.0 3.0 et 88	R 2.0 2.0 sec sec		ignalized		EB/WB	G A R 29.0 3.0 2.0 81.0 3.0 2.0 23 sec 120 sec		signalized		G 22.0 B / SB 58.0 Offset	A R 3.0 2.0 3.0 2.0 65 sec 90 sec
		Impacts	Movement SB TR	No-Action 33.8 C	With-Action  66.1 E	+ 31.2	litigated C	Movement SB TR	No-Action 188.1 F 2	With-Action 42.5 F +	Mitigated			No-Action 117.0 F 89.3 F	With-Ac 710.4 F 193.5 F	+	Mitigated 84.3 F 79.3 E	Movement SB TR	No-Action 222.8 F	With-Actio	+ 218.2	Mitigated F
		Mitigation Description	Change offset from SB phase.	m 76 seconds to 117	seconds. Shift 4 sec	conds from WE	phase to NB /	Shift 5 seconds from	n WB phase to NB /	SB phase.			Change offset from SB phase.	40 seconds to 17	seconds. Shift	15 seconds fro	om WB phase to NB /	Shift 4 seconds fro	om WB phase to NB	3 / SB phase.		
20	Bay Street and Clinton Street	Signal Timing Mitigation	No-Acti  WB  NB / SB  Offset  Cycle Leng	73.0 3.0 <b>76</b>	2.0 NB /	Mitigated G WB 33.0 / SB 77.0 fset Length	A R 3.0 2.0 3.0 2.0 117 sec 120 sec	No-Actio  WB  NB / SB  Offset  Cycle Lengt	31.0 3.0 3.0 49.0 3.0 5	R 2.0 W 2.0 NB / S sec Offs cec Cycle L	et 0	R 2.0 2.0 sec sec	wв	m/With-Action  G A  37.0 3.0  73.0 3.0  40  120	R 2.0 2.0 sec sec	wв	G         A         R           222.0         3.0         2.0           88.0         3.0         2.0           17         sec           120         sec	No-Acti  WB  NB / SB  Offset  Cycle Leng	49.0 3.0 <b>0</b>	sec	Mitigated     G	A R 3.0 2.0 3.0 2.0 0 sec 90 sec
		Impacts	Movement EB LTR WB LTR NB TR SB LT	No-Action	With-Action	38.7 35.0 16.5 30.2	D C B C	Movement EB LTR WB LTR NB TR SB LT	No-Action	With-Action	39.6 D 35.2 D 12.9 B 142.5 F	+	Movement EB LTR WB LTR NB TR SB LT	No-Action	With-Ac		Mitigated  44.2 D  39.5 D  37.4 D  36.5 F +	Movement EB LTR WB LTR NB TR SB LT	No-Action	With-Actio	38.7 33.8 7.9 96.4	C A
21	Bay Street and Baltic Street	Mitigation Description	Signalize intersect	tion. Signal warrant	#4 is met.			Signalize intersecti	on. Signal warrant #	4 is met.		Ş	Signalize intersectio	on. Signal warrant	#4 is met.			Signalize intersect	tion. Signal warrant	#4 is met.		
	Z I Baltic Street	Signal Timing Mitigation		ion/With-Action	Of	Mitigated   G   WB   29.0   81.0	A R 3.0 2.0 3.0 2.0 113 sec 120 sec		n/With-Action	EB / W NB / S Offs Cycle Lo	B 66.0 3.0 et 3	2.0 2.0 sec sec		n/With-Action		EB/WB	gated         R           Q A R         23.0           23.0         3.0         2.0           87.0         3.0         2.0           19 sec         120 sec		ion/With-Action		Mitigated G B / WB 14.0 B / SB 66.0 Offset	A R 3.0 2.0 3.0 2.0 3.0 sec 90 sec

# Table 21-5: Proposed Traffic Mitigation Table (con't)

	Intersection			Week	day AM	Peak Hour			Week	day MD	Peak Hour			Week	day PM	Peak Hour			Sature	day MD Pea	ak Hour	
			Movement	No-Action	Wi	th-Action	Mitigated	Movement	No-Action	Wi	ith-Action	Mitigated	Movement	No-Action	W	ith-Action	Mitigated	Movement	No-Action	With-Ac	ction	Mitigated
		Impacts	EB LR	48.6 E	138.8	F +	353.7 F +	EB LR	Err F	Err	F	Err F	EB LR	Err F	Err	F +	Err F +	EB LR	568.0 F	1,110.4 F		Err F
								NB LT	25.8 D	24.0	С	166.6 F +	NB LT	13.8 B	91.8	F +	298.8 F +	NB LT	6.5 A	11.6 B	6	9.8 F +
		Mitigation Description	Unmitigable. Inters				easures applied at	Unmitigable. Inter adjacent intersect				neasures applied at		rsection operations tions. Resulting imp			easures applied at		section operations ions. Resulting im			sures applied at
22	Bay Street and William Street		No-Acti	on/With-Action		Mi	tigated	No-Act	ion/With-Action		М	litigated	No-Ad	tion/With-Action		Mi	tigated	No-Act	ion/With-Action		Mitig	ated
		Signal Timing Mitigation	Un	signalized		Unsi	ignalized	Ui	nsignalized		Uns	signalized	U	Insignalized		Uns	ignalized	Ui	nsignalized		Unsign	alized
		Impacts	Movement	No-Action	Wi	th-Action	Mitigated	Movement	No-Action	Wi	ith-Action	Mitigated	Movement	No-Action	W	ith-Action	Mitigated	Movement	No-Action	With-Ac	ction	Mitigated
		impacts	Movement	NO ACCOL		III Addion	imagatea	Movement	NO ACTOR		ill Addon	imilgatea	NB LT	2.1 A	11.9	В	43.5 E +	Movement	NO AUTON	THE PA	J. I.	initigated
		Mitigation Description												rsection operations ctions. Resulting imp	s degrade o							
													No-Ad	tion/With-Action		Mi	tigated					
23	Bay Street and Congress Street	Signal Timing Mitigation											u	insignalized		Uns	ignalized					
			Movement	No-Action	Wi	th-Action	Mitigated	Movement	No-Action	Wi	ith-Action	Mitigated	Movement	No-Action	W	ith-Action	Mitigated	Movement	No-Action	With-Ad	etion	Mitigated
			Wovement	NO-ACTION	·	III-ACTION	Mitigated	Wovement	NO-ACTION	VVI	in-Action	witigated	WB LTR	37.1 D	35.2		Willigated	Wovement	No-Action	With-At	LIOH	Witigated
													WBL	07.1	00.2	J	51.0 D +					
													WB TR									
		Impacts						NB LT	204.3 F	279.3	F +	104.1 F	NB LT	84.0 F	215.9	F +	59.3 E +	NB LT	141.6 F	214.7 F		5.8 E
								NBLI	204.3	219.3	, <del>,</del>	104.1	SB L	17.7 B	99.4		10.8 B	NBLI	141.0	214.7	Ť /	5.6 L
			0D TD	00.5	77.0	_	47.0	0D TD	045.4	000.0	_	107.4						00 TD	200.0	000.0	. 4	74.0
			SB TR	23.5 C	77.8	E +	17.2 B	SB TR	215.4 F	268.9	F +	107.4 F	SB TR	110.2 F	207.1	F +	132.8 F +	SB TR	268.3 F	323.9 F	+ 1	71.8 F
24	Bay Street and Wave Street	Mitigation Description	parking regulation	on WB approach	to "No Star hange offse	nding Anytime" for	10' TR lane. Modify 95' from the stop bar (4 9 seconds. Shift 11	parking regulation	on WB approach	h to "No Star	nding Anytime" for	10' TR lane. Modify r 95' from the stop bar (4 se to NB / SB phase.	lane. Modify parl	ing regulation on W	NB approac	ch to "No Standing	urn bay) and one 10' TR Anytime" for 95' from from WB phase to NB /	parking regulation	oroach as one 10' l n on WB approach ill be removed). Si	to "No Standing	Anytime" for 95	from the stop bar (4
			No-Acti	on/With-Action		Mi	tigated	No-Act	ion/With-Action		М	litigated	No-Ac	tion/With-Action		Mi	tigated	No-Act	ion/With-Action		Mitig	ated
			] .	G A	R	_	G A R		G A	R		G A R		G A	R		G A R	_	G A	R		G A R
		Cianal Timir - Military	WB	37.0 3.0	2.0	WB	26.0 3.0 2.0	WB	31.0 3.0	2.0	WB	17.0 3.0 2.0	WB	30.0 3.0	2.0	WB	21.0 3.0 2.0	WB	31.0 3.0	2.0	<b>WB</b> 1	9.0 3.0 2.0
		Signal Timing Mitigation	NB / SB	73.0 3.0	2.0	NB/SB	84.0 3.0 2.0	NB / SB	49.0 3.0	2.0	NB / SB	63.0 3.0 2.0	NB / SB	80.0 3.0	2.0	NB / SB	89.0 3.0 2.0	NB/SB	49.0 3.0	2.0	NB/SB 6	1.0 3.0 2.0
			Offset	0	sec	Offset	9 sec	Offset	0	sec	Offset	0 sec	Offset	0	sec	Offset	0 sec	Offset	0	sec	Offset	0 sec
			Cycle Leng	jth 120	sec	Cycle Lengt	h 120 sec	Cycle Len	gth 90	sec	Cycle Lengt	th 90 sec	Cycle Ler	gth 120	sec	Cycle Lengt	h 120 sec	Cycle Len	gth 90	sec	Cycle Length	90 sec
					(			-					-									

# Table 21-<u>5</u>: Proposed Traffic Mitigation Table(con't)

	Intersection		Weekday A	M Peak Hour	<u>Weekday Mi</u>	D Peak Hour	Weekday PM	Peak Hour	Saturday MD	Peak Hour
Г			Movement No-Action	With-Action Mitigated	Movement No-Action V	Vith-Action Mitigated	Movement No-Action W	ith-Action Mitigated	Movement No-Action W	ith-Action Mitigated
		Impacts					<b>NB LT</b> 7.3 A 59.5	E + 13.0 B		
		Mitigation Description	Increased proposed cycle length from 60 s proposed mitigation at adjacent intersectio		Increased proposed cycle length from 60 sec proposed mitigation at adjacent intersections		Increased proposed cycle length from 60 seco proposed mitigation at adjacent intersections of		Increased proposed cycle length from 60 secc proposed mitigation at adjacent intersections	
25	Front Street and Wave Street		No-Action/With-Action	Mitigated	No-Action/With-Action	Mitigated	No-Action/With-Action	Mitigated	No-Action/With-Action	Mitigated
			G A R	G A R	G A R	G A R	G A R	G A R	G A R	G A R
		Signal Timing Mitigation	<b>EB</b> 19.0 3.0 2.0	<b>EB</b> 29.0 3.0 2.0	<b>EB</b> 19.0 3.0 2.0	<b>EB</b> 28.0 3.0 2.0	<b>EB</b> 19.0 3.0 2.0	<b>EB</b> 21.0 3.0 2.0	<b>EB</b> 19.0 3.0 2.0	<b>EB</b> 26.0 3.0 2.0
		Signal Tilling Willgation	<b>NB/SB</b> 31.0 3.0 2.0	<b>NB/SB</b> 51.0 3.0 2.0	<b>NB / SB</b> 31.0 3.0 2.0	<b>NB / SB</b> 52.0 3.0 2.0	<b>NB/SB</b> 31.0 3.0 2.0	<b>NB/SB</b> 59.0 3.0 2.0	<b>NB/SB</b> 31.0 3.0 2.0	<b>NB/SB</b> 54.0 3.0 2.0
			Offset 0 sec	Offset 0 sec	Offset 0 sec	Offset 0 sec	Offset 0 sec	Offset 0 sec	Offset 0 sec	Offset 0 sec
			Cycle Length 60 sec	Cycle Length 90 sec	Cycle Length 60 sec	Cycle Length 90 sec	Cycle Length 60 sec	Cycle Length 90 sec	Cycle Length 60 sec	Cycle Length 90 sec
			Movement No-Action	With-Action Mitigated		Vith-Action Mitigated		ith-Action Mitigated		lith-Action Mitigated
		Impacts	<b>NB TR</b> 41.6 D 70.6		<b>NB TR</b> 72.5 E 141.8	F + 23.5 C	NB TR 194.0 F 322.2	F + 92.4 F	NB TR 80.4 F 150.2	F + 45.2 D
			<b>SB LT</b> 31.7 C 152.:	F + 29.9 C	<b>SB LT</b> 231.4 F 731.1	F + 35.1 D	<b>SB LT</b> 2,797.4 F 3902.7	F + 1,277.9 F	<b>SB LT</b> 410.8 F 1119.2	F + 271.8 F
		Mitigation Description	Increased proposed cycle length from 60 s proposed mitigation at adjacent intersectio	econds to 90 seconds for consistency with as on Front Street.	Increased proposed cycle length from 60 sec proposed mitigation at adjacent intersections		Increased proposed cycle length from 60 seco proposed mitigation at adjacent intersections of		Increased proposed cycle length from 60 secon proposed mitigation at adjacent intersections of	
26	Front Street and		No-Action/With-Action	Mitigated	No-Action/With-Action	Mitigated	No-Action/With-Action	Mitigated	No-Action/With-Action	Mitigated
20	Prospect Street		G A R	G A R	G A R	G A R	G A R	G A R	G A R	G A R
			EB 13.0 3.0 2.0	EB 16.0 3.0 2.0	<b>EB</b> 13.0 3.0 2.0	<b>EB</b> 15.0 3.0 2.0	EB 13.0 3.0 2.0	<b>EB</b> 18.0 3.0 2.0	EB 13.0 3.0 2.0	EB 20.0 3.0 2.0
		Signal Timing Mitigation	<b>WB</b> 13.0 3.0 2.0	<b>WB</b> 23.0 3.0 2.0	<b>WB</b> 13.0 3.0 2.0	<b>WB</b> 17.0 3.0 2.0	<b>WB</b> 13.0 3.0 2.0	<b>WB</b> 16.0 3.0 2.0	<b>WB</b> 13.0 3.0 2.0	<b>WB</b> 18.0 3.0 2.0
			<b>NB / SB</b> 19.0 3.0 2.0	NB/SB 36.0 3.0 2.0	<b>NB / SB</b> 19.0 3.0 2.0	NB / SB 43.0 3.0 2.0	<b>NB/SB</b> 19.0 3.0 2.0	<b>NB / SB</b> 41.0 3.0 2.0	<b>NB / SB</b> 19.0 3.0 2.0	NB / SB 37.0 3.0 2.0
			Offset 0 sec	Offset 0 sec	Offset 0 sec	Offset 0 sec	Offset 0 sec	Offset 0 sec	Offset 0 sec	Offset 0 sec
			Cycle Length 60 sec	Cycle Length 90 sec	Cycle Length 60 sec	Cycle Length 90 sec	Cycle Length 60 sec	Cycle Length 90 sec	Cycle Length 60 sec	Cycle Length 90 sec
_			Manager No Action	APPAR A COLUMN TO THE PARTY OF		Maria Andrea Alberta I	N. A.C. W.	M. Anthon Albertania I	Manager No. Assess	Property Assessment of the Control o
		Impacts	Movement         No-Action           EB LT         57.7         E         62.5	With-Action Mitigated  E + 58.1 E	Movement No-Action V	Vith-Action Mitigated	Movement         No-Action         W           EB LT         49.3         D         80.1	ith-Action Mitigated F + 50.1 D	Movement No-Action W	ith-Action Mitigated
		Mitigation Description	Shift 1 second from NB phase to EB / WB	l .			Shift 5 seconds from NB phase to EB / WB ph	I		
			No-Action/With-Action	Mitigated			No-Action/With-Action	Mitigated		
27	Van Duzer Street and Beach Street		G A R	G A R			G A R	G A R		
			EB / WB 43.0 3.0 2.0	EB/WB 44.0 3.0 2.0			EB/WB 43.0 3.0 2.0	<b>EB/WB</b> 48.0 3.0 2.0		
		Signal Timing Mitigation	<b>NB</b> 67.0 3.0 2.0	NB 66.0 3.0 2.0			<b>NB</b> 67.0 3.0 2.0	<b>NB</b> 62.0 3.0 2.0		
			Offset 76 sec	Offset 76 sec			Offset 6 sec	Offset 6 sec		
			Cycle Length 120 sec	Cycle Length 120 sec			Cycle Length 120 sec	Cycle Length 120 sec		
_										
			Movement No-Action	With-Action Mitigated	Movement No-Action V	Vith-Action Mitigated	Movement No-Action W	ith-Action Mitigated	Movement No-Action W	ith-Action Mitigated
		Impacts	<b>NB L</b> 24.5 C 388.9	F + 23.1 C	<b>NB</b> L 348.4 F 373.4	F + 362.7 F +	<b>NB L</b> 921.0 F 971.4	F + 970.3 F +	<b>NB L</b> 359.2 F 383.0	F + 362.6 F +
		impacts	<b>NBT</b> 24.7 C 73.9	E + 7.0 A	<b>NBT</b> 63.8 E 120.2	F + 62.5 E	<b>NBT</b> 74.3 E 143.6	F + 135.5 F +	<b>NBT</b> 61.3 E 107.5	F + 63.4 E
			<b>SB TR</b> 67.8 E 80.7	F + 40.9 D	<b>SB TR</b> 204.5 F 252.9	F + 156.6 F	<b>SB TR</b> 174.3 F 277.2	F + 275.1 F +	<b>SB TR</b> 240.6 F 290.6	F + 211.8 F
20	Bay Street and	Mitigation Description	Shift 11 seconds from WB phase to NB / S seconds.	B phase. Change offset from 0 seconds to 25	Partial mitigation: Shift 8 seconds from WB p 0 seconds to 81 seconds.	hase to NB / SB phase. Change offset from	Unmitiç	gable	Partial mitigation: Shift 6 seconds from WB ph 0 seconds to 83 seconds.	ase to NB / SB phase. Change offset from
28	Water Street		No-Action/With-Action	Mitigated	No-Action/With-Action	Mitigated	No-Action/With-Action	Mitigated	No-Action/With-Action	Mitigated
			G A R	G A R	G A R	G A R	G A R	G A R	G A R	G A R
		Signal Timing Mitigation	<b>WB</b> 36.0 3.0 2.0	<b>WB</b> 25.0 3.0 2.0	<b>WB</b> 27.0 3.0 2.0	<b>WB</b> 19.0 3.0 2.0	<b>WB</b> 36.0 3.0 2.0	<b>WB</b> 36.0 3.0 2.0	<b>WB</b> 27.0 3.0 2.0	<b>WB</b> 21.0 3.0 2.0
		Signal Liming Witigation	<b>NB/SB</b> 74.0 3.0 2.0	<b>NB/SB</b> 85.0 3.0 2.0	<b>NB / SB</b> 53.0 3.0 2.0	<b>NB / SB</b> 61.0 3.0 2.0	<b>NB / SB</b> 74.0 3.0 2.0	<b>NB / SB</b> 74.0 3.0 2.0	<b>NB / SB</b> 53.0 3.0 2.0	<b>NB / SB</b> 59.0 3.0 2.0
			Offset 0 sec	Offset 25 sec	Offset 0 sec	Offset 81 sec	Offset 0 sec	Offset 0 sec	Offset 0 sec	Offset 83 sec
			Cycle Length 120 sec	Cycle Length 120 sec	Cycle Length 90 sec	Cycle Length 90 sec	Cycle Length 120 sec	Cycle Length 120 sec	Cycle Length 90 sec	Cycle Length 90 sec

# Table 21-5: Proposed Traffic Mitigation Table(con't)

	Intersection			Weel	kday AN	l Peak Hour			<u>Week</u>	day MI	O Peak Hour				Weekday	PM Peak Hou	<u>:</u>		Saturday N	/ID Peak Hour	
			Movement	No-Action	W	ith-Action	Mitigated	Movement	No-Action	V	Vith-Action	Mitigated	Move	ement No	o-Action	With-Action	Mitigated	Movement	No-Action	With-Action	Mitigated
		Impacts	NB TR	8.2 A	58.0	E +	15.0 B	NB TR	119.4 F	196.5		75.5 E	_	3 TR 84.		7.2 F +	214.8 F +	NB TR	97.7 F 179.2		72.3 E
								SB LT	1,052.7 F	1201.2	F + 1	27.3 F	SE	3 LT 1,303	3.9 F 165	52.0 F +	250.3 F	SB LT	1,167.3 F 1,309.	.0 F +	162.6 F
		Mitigation Description	Prohibit SB left tur prohibition)	rns. (Note: mitiga	ated condition	on includes detoure	d traffic due to turn				SB phase. Prohibit Slue to turn prohibition)					seconds to 99 second traffic due to turn	ds. Prohibit SB left turns. prohibition)		rom EB / WB phase to NB on includes detoured traffic		
29	Bay Street and Canal Street		No-Acti	ion/With-Action	ı	Mi	itigated	No-Act	ion/With-Action		Mitiç	gated		No-Action/Wi	ith-Action		Mitigated	No-Ac	tion/With-Action		Mitigated
				G A	R	-	G A R		G A	R	_	G A R		G	A I	₹	G A R		G A R		G A R
		Signal Timing Mitigation	EB/WB	37.0 3.0	2.0	EB/WB	37.0 3.0 2.0	EB / WB	35.0 3.0	2.0	EB/WB 2	25.0 3.0 2.	0 1	EB / WB 37.0	0 3.0 2	.0 <b>EB / W</b> E	37.0 3.0 2.0	EB / WB	35.0 3.0 2.0	EB / WB	26.0 3.0 2.0
		Signal Tilling Mitigation	NB / SB	73.0 3.0	2.0	NB / SB	73.0 3.0 2.0	NB / SB	45.0 3.0	2.0	NB / SB	55.0 3.0 2.	0	NB / SB 73.	0 3.0 2	.0 <b>NB / S</b> E	73.0 3.0 2.0	NB / SB	45.0 3.0 2.0	NB / SB	54.0 3.0 2.0
			Offset	34	sec	Offset	34 sec	Offset	12	sec	Offset	12 se	С	Offset	82 s	ec Offset	99 sec	Offset	12 sec	Offset	12 sec
Ĺ			Cycle Leng	jth 120	sec	Cycle Lengt	h 120 sec	Cycle Len	gth 90	sec	Cycle Length	90 se	c C	ycle Length	120 s	ec Cycle Ler	gth 120 sec	Cycle Len	igth 90 sec	Cycle Len	gth 90 sec
.=																					
		Impacts	Movement	No-Action	W	ith-Action	Mitigated	Movement	No-Action	٧	Vith-Action	Mitigated	Move	ement No	o-Action	With-Action	Mitigated	Movement	No-Action	With-Action	Mitigated
		Mitigation Description	Increased propose proposed mitigation				for consistency with		ed cycle length fro on at adjacent inte		onds to 90 seconds fo on Front Street.	r consistency with				seconds to 90 secontions on Front Street.	ds for consistency with		sed cycle length from 60 s ion at adjacent intersection		s for consistency with
20	Front Street and		No-Acti	ion/With-Action	ı	Mi	itigated	No-Act	ion/With-Action		Mitiç	gated		No-Action/Wi	ith-Action		Mitigated	No-Ac	tion/With-Action		Mitigated
30	Gallal Street			G A	R	_	G A R		G A	R		G A R	:	G	A I	र	G A R		G A R		G A R
		Signal Timing Mitigation	EB	19.0 3.0	2.0	ЕВ	25.0 3.0 2.0	EB	19.0 3.0	2.0	EB 3	35.0 3.0 2.	0	<b>EB</b> 19.	0 3.0 2	.0 <b>E</b> E	32.0 3.0 2.0	EB	19.0 3.0 2.0	ЕВ	35.0 3.0 2.0
		Signal Tilling Mitigation	NB/SB	31.0 3.0	2.0	NB / SB	55.0 3.0 2.0	NB / SB	31.0 3.0	2.0	NB / SB	45.0 3.0 2.	0	NB / SB 31.	0 3.0 2	.0 NB / SE	48.0 3.0 2.0	NB / SB	31.0 3.0 2.0	NB / SB	45.0 3.0 2.0
			Offset	0	sec	Offset	0 sec	Offset	0	sec	Offset	0 se	С	Offset	0 s	ec Offset	0 sec	Offset	0 sec	Offset	0 sec
			Cycle Leng	jth 60	sec	Cycle Lengt	h 90 sec	Cycle Len	gth 60	sec	Cycle Length	90 se	c C	ycle Length	60 s	ec Cycle Ler	gth 90 sec	Cycle Ler	igth 60 sec	Cycle Len	gth 90 sec
_																					
			Movement	No-Action	W	ith-Action	Mitigated	Movement	No-Action	٧	Vith-Action	Mitigated			o-Action	With-Action	Mitigated	Movement	No-Action	With-Action	Mitigated
					+									37.5	5 D 11	4.0 F +					
		Impacts			+									BL			43.8 D				
				40.0		_					-			B R		67.4 F +	40.2 D				207.0
			NB LT	18.9 B	69.0	E +	33.5 C	NB LT	1,234.7 F	1,418.4		087.7 F		3 LT 1,091			1,632.7 F +	NB LT	1,024.5 F 1,339.		995.2 F
								SB T	136.3 F	186.7	F + 1	02.6 F	51	BT 62.	0 E 13	3.8 F +	87.7 F +	SB T	180.6 F 229.5	5 F +	128.4 F
31	Bay Street and Broad Street	Mitigation Description		ne" regulation or	EB approa	ch by 75' (3 parking	11' TR lane. Extend " g spaces will be	No Parking Anytir		EB approa	o' turn bay) and one 11 ach by 75' (3 parking s NB / SB phase.		lane. Ex	tend " No Parkin	ng Anytime" regu		0' turn bay) and one 11' TF by 75' (3 spaces will be	No Parking Anyti	proach as one 14' L lane (1 me" regulation on EB app 3 seconds from EB phase	roach by 75' (3 parki	
			No-Acti	ion/With-Action	I	Mi	itigated	No-Act	ion/With-Action		Mitiç	gated		No-Action/Wi	ith-Action		Mitigated	No-Ac	tion/With-Action		Mitigated
				G A	R	_	G A R		G A	R		G A R	:	G	A I	₹	G A R		G A R		G A R
			LPI	2.0 3.0	2.0	LPI	2.0 3.0 2.0	LPI	2.0 3.0	2.0	LPI	2.0 3.0 2.	0	<b>LPI</b> 2.0	3.0 2	.0 <b>LP</b>	2.0 3.0 2.0	LPI	2.0 3.0 2.0	LPI	2.0 3.0 2.0
		Signal Timing Mitigation	EB	33.0 3.0	2.0	EB	30.0 3.0 2.0	EB	27.0 3.0	2.0	EB 2	20.0 3.0 2.	0	EB 33.	0 3.0 2	.0 <b>E</b> E	27.0 3.0 2.0	EB	27.0 3.0 2.0	ЕВ	19.0 3.0 2.0
			NB / SB	70.0 3.0	2.0	NB / SB	73.0 3.0 2.0	NB / SB	46.0 3.0	2.0	NB/SB 5	53.0 3.0 2.	0	<b>NB / SB</b> 70.	0 3.0 2	.0 NB / SE	76.0 3.0 2.0	NB / SB	46.0 3.0 2.0	NB / SB	54.0 3.0 2.0
			Offset	26	sec	Offset	26 sec	Offset	6	sec	Offset	6 se	С	Offset	90 s	ec Offset	90 sec	Offset	6 sec	Offset	6 sec
L			Cycle Leng	jth 120	sec	Cycle Lengt	h 120 sec	Cycle Len	gth 90	sec	Cycle Length	90 se	c C	ycle Length	120 s	ec Cycle Ler	gth 120 sec	Cycle Ler	ngth 90 sec	Cycle Len	gth 90 sec

Table 21-5: Proposed Traffic Mitigation Table (con't)

	Intersection		<u>Week</u>	day AM Peak Hou	<u>r</u>		Weekd	day MD Pe	ak Hour			<u>Week</u>	day PM	Peak Hour			<u>Satur</u>	day MD P	eak Hour	
			Movement No-Action  WB L 60.5 E	With-Action           76.0         E         +	Mitigated 76.0 E +	Movement	No-Action	With-A	ction	Mitigated	Movement EB L	No-Action 150.8 F	197.4	ith-Action F +	Mitigated 197.4 F +	Movement	No-Action	With-	Action	Mitigated
		Impacts				NB LTR SB LTR	35.4 D 105.3 F	52.7 D 181.5 F		.6 D +	WB TR  NB LTR  SB LT	76.6 E 40.8 D	87.0 191.0	F + F + F +	87.0 F + 191.2 F +	NB LTR SB LTR	37.7 D 65.3 E			5 D 5 E
35	Victory Boulevard and Cebra Avenue	Mitigation Description		Unmitigable				Unmitigable			3B LI	47.0	Unmitig		113.0 1 +	Shift 3 seconds fr	om EB / WB phas	e to NB / SB p	hase.	
		Signal Timing Mitigation	No-Action/With-Action           G         A           LPI         5.0         2.0           EB / WB         31.0         3.0           NB / SB         72.0         3.0           Offset         112           Cycle Length         120	R 0.0 LP 2.0 EB / WE 2.0 NB / SE C Offset sec Cycle Ler	31.0 3.0 2.0 72.0 3.0 2.0 112 sec	No-Acti  LPI  EB / WB  NB / SB  Offset  Cycle Leng	on/With-Action  G A  5.0 2.0  26.0 3.0  47.0 3.0  0  th 90	R 0 2.0 2.0 sec sec	Mitiga  LPI 5.  EB / WB 26  NB / SB 47  Offset  Cycle Length	6 A R 0 2.0 0 .0 3.0 2.0	No-Act  LPI  EB / WB  NB / SB  Offset  Cycle Leng	Gon/With-Action           G         A           5.0         2.0           29.0         3.0           74.0         3.0           57         9th           120	R 0 2.0 2.0 sec sec	LPI EB / WB NB / SB Offset Cycle Lengt	digated           G         A         R           5.0         2.0         0           29.0         3.0         2.0           74.0         3.0         2.0           57         sec           120         sec	No-Act  LPI  EB / WB  NB / SB  Offset  Cycle Len	47.0 3.0 <b>0</b>	R 0 2.0 2.0 sec sec	Mitigate G LPI 5.0 EB / WB 23.0 NB / SB 50.0 Offset Cycle Length	A R 0 2.0 0 0 3.0 2.0
		Impacts	Movement No-Action  SB LR 40.9 D	With-Action  50.2 D +	Mitigated  44.3 D	Movement  EB L  EB T  WB T  SB LR	No-Action 43.6 D 39.7 D 70.0 E 28.3 C	With-A 235.8 F 68.2 E 103.6 F 67.5 E	+ 238 + 68 + 103	.3 E + 3.9 F +	Movement EB L WB T SB LR	No-Action 66.3 E 79.3 E 43.3 D	93.0 70.5	F +  F +  E +	Mitigated       807.5     F     +       92.7     F     +       70.5     E     +	Movement EB L EB T WB T	No-Action 36.0 D 42.9 D 50.2 D	91.7 58.0	Action F + 96.1 E + 59.1 E + 64.1	9 E +
36	Victory Boulevard and Jersey Street	Mitigation Description	Shift 3 seconds from EB / WB phas	e to SB phase.				Unmitigable					Unmitig	able				Unmitigabl	е	
		Signal Timing Mitigation	No-Action/With-Action   G	R 2.0 EB/WE 2.0 SE	103 sec	EB / WB SB Offset Cycle Leng	31.0 3.0 <b>0</b>	2.0 2.0 sec	Mitiga  EB / WB 49  SB 31  Offset  Cycle Length	A R .0 3.0 2.0	EB / WB SB Offset Cycle Leng	33.0 3.0 33	R 2.0 2.0 sec sec	EB/WB	33.0 3.0 2.0 33 sec	EB / WB SB Offset Cycle Len	31.0 3.0 <b>0</b>	R 2.0 2.0 sec sec	Mitigat   G   G   49.	<b>A R</b> 0 3.0 2.0
		Impacts	Movement No-Action	With-Action	Mitigated	Movement NB L SB T	No-Action           52.2         D           75.8         E	With-A 103.9 F 80.3 F	+ 51	Mitigated  .6 D  .1 E	Movement NB L SB T	No-Action 30.4 C 74.1 E	86.4 79.8	f + E +	Mitigated           69.7         E         +           78.1         E         +	Movement NB L SB T	No-Action 67.8 E 64.8 E	100.8	Action + 63.4 E + 67.4	
		Mitigation Description				Shift 3 seconds fro	om EB phase to NE	B / SB phase.			Partial mitigation:	Shift 1 second fro	om EB phas	se to NB / SB phase	<b>)</b> .	Shift 2 seconds fr	om EB phase to N	IB / SB phase.		
38	Victory Boulevard and Forest Avenue	Signal Timing Mitigation				No-Acti LPI EB NB / SB Offset Cycle Leng	on/With-Action  G A  5.0 2.0  27.0 3.0  46.0 3.0  0  th 90	R 0 2.0 2.0 sec sec	Mitiga   C	A         R           0         2.0         0           .0         3.0         2.0	No-Act  LPI  EB  NB / SB  Offset  Cycle Leng	77	2.0 2.0	LPI EB NB / SB Offset Cycle Lengt	G         A         R           5.0         2.0         0           28.0         3.0         2.0           75.0         3.0         2.0           77         sec           n         120         sec	No-Act  LPI  EB  NB / SB  Offset  Cycle Len		R 0 2.0 2.0 sec sec	Mitigat	A R 0 2.0 0 0 3.0 2.0

Table 21-5: Proposed Traffic Mitigation Table (con't)

	Intersection		Weekday Al	M Peak Hour	Weekday MD Po	eak Hour	Weekday PM Peak I	<u>Hour</u>	<u>Saturday M</u> i	D Peak Hour
Г			Movement No-Action	With-Action Mitigated	Movement No-Action With-	Action Mitigated	Movement No-Action With-Action	Mitigated	Movement No-Action	With-Action Mitigated
		Impacts	<b>EB LT</b> 47.4 D 53.7	D + 29.3 C						
			<b>NB LT</b> 52.5 D 58.7	E + 54.3 D						
		Mitigation Description	Change offset from 10 seconds to 92 second phase.	ds. Shift 1 second from EB / WB phase to NB						
43	Broad Street and Targee Street		No-Action/With-Action	Mitigated						
	<b>3</b>		G A R	G A R						
			EB / WB 43.0 3.0 2.0	EB/WB 42.0 3.0 2.0						
		Signal Timing Mitigation	NB 67.0 3.0 2.0	NB 68.0 3.0 2.0						
			Offset 10 sec	Offset 92 sec						
			Cycle Length 120 sec	Cycle Length 120 sec						
<u> </u>										
Г			Movement No-Action	With-Action Mitigated	Movement No-Action With-	Action Mitigated	Movement No-Action With-Action	Mitigated	Movement No-Action	With-Action Mitigated
			<b>EB LTR</b> 40.4 D 49.9	D + 49.9 D +	EB LTR 63.3 E 79.5	E + 79.5 E +				
		Impacts					<b>WB LTR</b> 37.2 D 50.7 D	+ 50.3 D +		
		•	<b>NB LTR</b> 177.2 F 220.2	F + 220.2 F +	<b>NB LTR</b> 162.3 F 177.3	F + 177.3 F +	<b>NB LTR</b> 79.9 E 87.8 F	+ 87.8 F +		
			<b>SB LTR</b> 99.8 F 113.7	F + 113.7 F +						
		Mitigation Description	Unmit	tigable	Unmitigable	9	Unmitigable			
44	Vanderbilt Avenue and Tompkins Avenue		No-Action/With-Action	Mitigated	No-Action/With-Action	Mitigated	No-Action/With-Action	Mitigated		
			G A R	G A R	G A R	G A R	G A R	G A R		
			EB/WB 62.0 3.0 2.0	EB/WB 62.0 3.0 2.0	EB/WB 42.0 3.0 2.0	EB/WB 42.0 3.0 2.0	<del> </del>	3/WB 61.0 3.0 2.0		
		0	LPI 2.0 3.0 2.0	LPI 2.0 3.0 2.0	LPI 2.0 3.0 2.0	LPI 2.0 3.0 2.0	LPI 2.0 3.0 2.0	LPI 2.0 3.0 2.0		
		Signal Timing Mitigation		NB / SB 41.0 3.0 2.0	NB/SB 31.0 3.0 2.0			B/SB 42.0 3.0 2.0		
				<del>                                     </del>						
L			Cycle Length 120 sec	Cycle Length 120 sec	Cycle Length 90 sec	Cycle Length 90 sec	Cycle Length 120 sec Cycle	le Length 120 sec		
-			Marramant Na Astion	With-Action Mitigated	Manager No Asting Mile	Antina Minimate I	Management No Assissa	Minimum d	Manager Na Astion	Aliah Assisus Balaineas A
		lana di	Movement No-Action NB LT 13.9 B 46.8	With-Action Mitigated D + 38.4 D	Movement         No-Action         With-Action           NB LT         1,912.8         F         3,368.1	Action Mitigated F + 1,225.0 F	Movement         No-Action         With-Action           NB LT         508.0         F         997.9         F	Mitigated + 901.9 F +	Movement         No-Action         No-Action           NB LT         3,246.2         F         3,598.7	With-Action Mitigated F + 3,147.0 F
		Impacts	NB E1 13.9 B 40.0	D + 30.4 D		F + 80.3 F	NB E1 300.0 1 337.3 1	7 301.9 1 7	SBT 145.4 F 180.4	F + 139.9 F
					36 I 105.3 F 126.1	F + 00.5 F			3B I 143.4 F 160.4	F + 139.9 F
		Mitigation Description	Shift 1 second from EB phase to NB / SB ph	ase.	Shift 4 seconds from EB phase to NB / SB phase.		Partial mitigation: Shift 1 second from EB phase to NB / S	SB phase.	Shift 3 seconds from EB phase to NB / SB pl	nase.
45	Bay Street and Vanderbilt Avenue		No-Action/With-Action	Mitigated	No-Action/With-Action	Mitigated	No-Action/With-Action	Mitigated	No-Action/With-Action	Mitigated
			G A R	G A R	G A R	G A R	G A R	G A R	G A R	G A R
		Cinnal Timina Misimasian	<b>EB</b> 37.0 3.0 2.0	<b>EB</b> 36.0 3.0 2.0	<b>EB</b> 35.0 3.0 2.0	<b>EB</b> 31.0 3.0 2.0	<b>EB</b> 37.0 3.0 2.0	<b>EB</b> 36.0 3.0 2.0	<b>EB</b> 35.0 3.0 2.0	EB 32.0 3.0 2.0
		Signal Timing Mitigation	NB / SB 73.0 3.0 2.0	<b>NB / SB</b> 74.0 3.0 2.0	<b>NB / SB</b> 45.0 3.0 2.0	<b>NB/SB</b> 49.0 3.0 2.0	NB / SB 73.0 3.0 2.0 NI	B/SB 74.0 3.0 2.0	<b>NB / SB</b> 45.0 3.0 2.0	<b>NB / SB</b> 48.0 3.0 2.0
			Offset 1 sec	Offset 1 sec	Offset 52 sec	Offset 52 sec	Offset 115 sec	Offset 115 sec	Offset 52 sec	Offset 52 sec

Table 21-5: Proposed Traffic Mitigation Table(con't)

	Intersection			Week	day AM Pea	ak Hour			Week	day MD	Peak Hour				Week	day PN	l Peak Hour				<u>Satu</u>	rday MI	) Peak Hour	<u>1</u>		
		Impacts	Movement	No-Action	With-Ac	ction	Mitigated	Movement	No-Action	W	ith-Action	Mitigated		Movement	No-Action	V	/ith-Action	Mitigated	i	Movement	No-Action		Vith-Action	07.1	Mitigated	
		Mitigation Description																	;	SB T Shift 2 seconds fro	36.9 D	55.5	E +	37.8	D	
47	Bay Street and Edgewater Drive																			No-Acti	on/With-Action	R		Mitigate G	d A	R
							$\overline{}$										[			WB / NWB	31.0 3.0	2.0	WB / NWB			2.0
		Signal Timing Mitigation																		NB/SB	49.0 3.0	2.0	NB / SB			2.0
																				Offset	45	sec	Offset		45	sec
																				Cycle Leng	th 90	sec	Cycle Len	gth	90	sec
-					·																			•		
			Movement	No-Action	With-Ac	ction	Mitigated	Movement	No-Action		ith-Action	Mitigated		Movement	No-Action		/ith-Action	Mitigated		Movement	No-Action		Vith-Action		Mitigated	
			WDITD	100 G E	106.0 F	. 1	06.0 F +	EB LTR	81.1 F	110.0	F +	110.0 F	+	EB LTR WB LTR	95.8 F 89.2 F	169.4 92.4	F +	169.4 F 92.4 F	+	EB LTR	77.9 E	110.3	F +	110.3	B F	+
		Impacts	WB LTR NB LTR	100.6 F 176.2 F	713.8 F		16.3 F +	NB LTR	1,762.1 F	2463.6	F +	2.463.6 F	+	NB LTR	1,326.7 F	1869.2	F +	1.867.8 F	+	NB LTR	1.540.4 F	1,909.6	F +	1.909.	6 F	
			SBT	39.1 D	73.0 E		72.9 E +	SBT	97.0 F	134.6	F +	134.7 F	+	SBT	85.3 F	143.6	F +	143.0 F	+	SBT	90.6 F	128.0	F +	128.3		+
						i i	-				<u> </u>						Į.			<del></del>						
		Mitigation Description			Unmitigable					Unmitio	gable					Unmiti	gable					Unmiti	gable			
48	Bay Street and Hylan Boulevard		No-Act	tion/With-Action		Mitig	gated	No-Acti	on/With-Action		М	itigated		No-Acti	on/With-Action		Mi	tigated		No-Acti	on/With-Action			Mitigate	d	
	,			G A	R		G A R		G A	R		G A	R		G A	R		G A	R		G A	R	1	G	Α	R
			SBR / EBL	13.0 3.0		SBR / EBL 1	13.0 3.0 2.0	SBR / EBL	9.0 3.0	2.0	SBR / EBL	9.0 3.0	2.0	SBR / EBL	13.0 3.0	2.0	SBR / EBL	13.0 3.0	2.0	SBR / EBL	9.0 3.0	2.0	SBR / EBL	9.0	3.0	2.0
		Signal Timing Mitigation	EB / WB	31.0 3.0	2.0	_	31.0 3.0 2.0	EB / WB	22.0 3.0	2.0	EB / WB		2.0	EB/WB	31.0 3.0	2.0	EB/WB	31.0 3.0	2.0	EB/WB	22.0 3.0	2.0	EB/WB			2.0
			LPI	2.0 3.0	2.0		2.0 3.0 2.0	LPI	2.0 3.0	2.0	LPI	<del></del>	2.0	LPI	2.0 3.0	2.0	LPI	2.0 3.0	2.0	LPI	2.0 3.0	2.0	LPI		_	2.0
			NB / SB	54.0 3.0	2.0		54.0 3.0 2.0	NB / SB	37.0 3.0	2.0	NB / SB		2.0	NB / SB Offset	54.0 3.0	2.0	NB / SB	54.0 3.0	2.0	NB / SB	37.0 3.0	2.0	NB / SB			2.0
			Offset Cycle Leng	55 gth 120	sec	Offset  Cycle Length	55 sec 120 sec	Offset Cycle Leng	0 th 90	sec	Offset Cycle Lengt		sec	Cycle Leng	61 th 120	sec	Offset Cycle Lengt	61 h 120	sec	Offset Cycle Leng	0 th 90	sec	Offset Cycle Len		90	sec
L			Oyole Len	9 120	300	Oyole Length	120 360	Oyole Leng	30	360	Oyole Lelig	30	360	Oyole Leng	120	360	Oyolo Longe	120	360	Oyole Leng	30	360	Oyole Len	gui		360
			Movement	No-Action	With-Ac	ction	Mitigated	Movement	No-Action	W	ith-Action	Mitigated		Movement	No-Action	V	/ith-Action	Mitigated	d	Movement	No-Action	V	Vith-Action		Mitigated	
		Impacts	EB L	93.1 F	146.1 F	+ 9	91.4 F	EB L	195.2 F	252.6	F +	189.8 F		EB L	233.4 F	341.1	F +	306.5 F	+	EB L	210.7 F	277.4	F +	197.5	B F	
		Mitigation Description	Shift 6 seconds fr	rom NB / SB phase	to EB / WB pha	ase.		Shift 4 seconds fro	om NB / SB phase	to EB / W	/B phase.			Partial mitigation: s from 116 seconds	Shift 3 seconds fr to 36 seconds.	om NB / S	B phase to EB / WE	3 phase. Change	offset	Shift 5 seconds fro	om NB / SB pha	se to EB / V	VB phase.			
49	Bay Street and		No-Act	tion/With-Action		Mitig	gated	No-Acti	on/With-Action		М	itigated		No-Acti	on/With-Action		Mi	tigated		No-Acti	on/With-Actior			Mitigate	d	
49	9 School Road			G A	R		G A R	,	G A	R		G A	R	,	G A	R		G A	R	ı	G A	R	I	G	Α	R
		Signal Timing Mitigation	EB / WB		2.0	_	51.0 3.0 2.0	EB / WB	38.0 3.0	2.0	EB / WB		2.0	EB/WB	63.0 3.0	2.0	H	66.0 3.0	2.0	EB/WB	38.0 3.0		EB / WB			2.0
		5 5	NB / SB	65.0 3.0	2.0		59.0 3.0 2.0	NB / SB	42.0 3.0	2.0	NB / SB		2.0	NB / SB	47.0 3.0	2.0	NB / SB	44.0 3.0	2.0	NB / SB	42.0 3.0	2.0	NB / SB			2.0
			Offset	0	sec	Offset	0 sec	Offset	25	sec	Offset		sec	Offset	116	-	Offset	36	sec	Offset	25	sec	Offset		25	sec
			Cycle Leng	gth 120	sec	Cycle Length	120 sec	Cycle Leng	th 90	sec	Cycle Lengt	th 90	sec	Cycle Leng	th 120	sec	Cycle Lengt	h 120	sec	Cycle Leng	th 90	sec	Cycle Len	gth	90	sec

The potential significant adverse traffic impacts at the following study locations would be fully mitigated through an increased cycle length. The specific cycle length and signal timing changes for each study intersection are outlined in Table 21-5.

- Front Street and Wave Street (Intersection 25 on Figure 14-6)
  - O Potential significant adverse traffic impacts are not expected at this intersection during the Weekday AM, MD, or Saturday MD peak hours; however, increased cycle lengths are recommended for consistency with mitigation measures proposed at adjacent intersections on Front Street.
- Front Street and Prospect Street (Intersection 26 on Figure 14-6)
- Front Street and Canal Street (Intersection 30 on Figure 14-6)
  - Potential significant adverse traffic impacts are not expected at this intersection; however, increased cycle lengths are recommended for consistency with mitigation measures proposed at adjacent intersections on Front Street.

#### PARTIALLY MITIGATED SIGNIFICANT ADVERSE TRAFFIC IMPACTS

Mitigation measures implemented at the following study locations would partially mitigate significant adverse traffic impacts. The specific signal timing, offset modifications, cycle lengths, and geometric changes for each study intersection are outlined in Table  $21-\underline{5}$ .

- Richmond Terrace and Jersey Street (Intersection 2 on Figure 14-6)
  - o Restriping the westbound approach as one 10-foot left-turn lane and one 11-foot through/right-turn lane for 100 feet, reallocating green time, and modifying offsets would mitigate the potential significant adverse traffic impacts at this intersection for the Weekday AM, MD, and Saturday MD peak hours.
  - O Potential significant adverse traffic impacts during the Weekday PM peak hour would be partially mitigated. The implementation of the recommended mitigation measures would result in a new potential significant impact for the westbound through/right-turn lane group during the Weekday PM peak hour, which would be unmitigable.
- Richmond Terrace and Ferry Terminal (parking lot) (Intersection 9 on Figure 14-6)
  - o Reallocating green time would mitigate the potential significant adverse traffic impact at this intersection for the Weekday AM peak hour.
  - O Potential significant adverse traffic impacts during the Weekday MD, PM, and Saturday MD peak hours would be unmitigable.
- Victory Boulevard and Bay Street (Intersection 12 on Figure 14-6)
  - Proposed mitigation measures at this intersection include the reallocation of green time to allow for a leading northbound left-turn phase as well as modified offsets.
  - o Potential significant adverse traffic impacts during the Weekday AM peak hour would be fully mitigated.
  - o Potential significant adverse traffic impacts during the Weekday MD, PM, and Saturday MD peak hours would be partially mitigated. The implementation of the recommended mitigation measures would result in a new potential significant impact for the eastbound left-turn/through and southbound right-turn lane groups during the Weekday MD peak hour.

- Bay Street and Hannah Street (Intersection 13 on Figure 14-6)
  - o Proposed mitigation measures at this intersection include the reallocation of green time, modified offsets, new protected turn phases, and the reconfiguration of the south leg of the intersection. The northbound direction would include a permanent curb extension and would be restriped as one 5-foot bicycle lane, two 11-foot through/right-turn lanes, and one-11 foot left-turn bay (75 feet long). This mitigation measure would include the removal of on-street parking on the east side of Bay Street between Swan Street and Hannah Street for a distance of approximately 125 feet (6 parking spaces). The west side of the south leg of the intersection would be modified to create a permanent curb extension, which was included as a recommendation in the *TIS*.
  - o Potential significant adverse traffic impacts during the Weekday MD, PM, and Saturday MD peak hours would be fully mitigated.
  - Potential significant adverse traffic impacts during the Weekday AM peak hour would be partially mitigated.
- Bay Street and Swan Street/Van Duzer Street (Intersection 15 on Figure 14-6)
  - Reallocating green time and changing the offset would mitigate the potential significant adverse traffic impact at this intersection for the Weekday AM peak hour.
  - o Potential significant adverse traffic impacts during the Weekday PM peak hour would be unmitigable.
- Bay Street and Grant Street (Intersection 18 on Figure 14-6)
  - The installation of a new traffic signal would partially mitigate the potential significant adverse traffic impact at this intersection during the Weekday AM peak hour. Signal warrant #4 (Pedestrian Warrant) would be met at this intersection during the Weekday MD, PM, and Saturday MD peak hours.
  - O While the installation of a traffic signal would mitigate the potential significant impact for the side street approach during the AM peak hour and create an opportunity for pedestrians to safely cross Bay Street, it would result in additional delay for southbound traffic on Bay Street which would result in a new potential significant adverse traffic impact for the southbound approach during the Weekday AM, MD, PM, and Saturday MD peak hours.
- Bay Street and Baltic Street (Intersection 21 on Figure 14-6)
  - o The installation of a new traffic signal is recommended at this intersection to facilitate pedestrian crossings. Signal warrant #4 (Pedestrian Warrant) is met at this intersection during the Weekday AM, MD, PM, and Saturday MD peak hours.
  - O While the installation of a traffic signal would create an opportunity for pedestrians to safely cross Bay Street, it would result in additional delay for northbound and southbound traffic on Bay Street which would result in a new potential significant adverse traffic impact for the southbound approach during the Weekday MD, PM, and Saturday MD peak hours.
- Bay Street and Wave Street (Intersection 24 on Figure 14-6)
  - o Restriping the westbound approach as one 10-foot left-turn lane (70 feet long) and one 10-foot through/right-turn lane, reallocating green time, modifying offsets, and eliminating parking on the north side of the west approach (4 parking

- spaces) would mitigate the potential significant adverse traffic impacts at this intersection for the Weekday AM, MD, and Saturday MD peak hours.
- o Potential significant adverse traffic impacts during the Weekday PM peak hour would be partially mitigated.
- Bay Street and Water Street (Intersection 28 on Figure 14-6)
  - Reallocating green time and modifying offset would mitigate the potential significant adverse traffic impacts at this intersection for the Weekday AM peak hour.
  - o Reallocating green time and modifying offset would partially mitigate the potential significant adverse traffic impacts at this intersection for the Weekday MD and Saturday MD peak hours.
  - o Potential significant adverse traffic impacts during the Weekday PM peak hour would be unmitigable.
- Bay Street and Canal Street (Intersection 29 on Figure 14-6)
  - Proposed mitigation measures at this intersection include the prohibition of the southbound left-turn movement. Vehicles expected to make southbound left turns at this intersection would continue south on Bay Street, turn right onto Thompson Street, right onto Wright Street, and right onto Canal Street to reach their destination.
  - o The analyses of the mitigated conditions at this intersection account for diverted traffic associated with the southbound left-turn prohibition.
  - Prohibiting the southbound left-turn movement would fully mitigate the potential significant adverse traffic impact at this intersection for the Weekday AM peak hour.
  - o Prohibiting the southbound left-turn movement and reallocating green time would fully mitigate the potential significant adverse traffic impacts at this intersection for the Weekday MD and Saturday MD peak hours.
  - o Prohibiting the southbound left-turn movement and changing the offset would partially mitigate the potential significant adverse traffic impacts at this intersection for the Weekday PM peak hour.
- Bay Street and Broad Street (Intersection 31 on Figure 14-6)
  - o Restriping the eastbound approach as one 14-foot left-turn lane (100 feet long) and one 11-foot through/right-turn lane, reallocating green time, and eliminating 3 parking spaces on the south side of the east approach would fully mitigate the potential significant adverse traffic impacts at this intersection for the Weekday AM, MD, and Saturday MD peak hours and partially mitigate the potential significant adverse traffic impacts at this intersection for the Weekday PM peak hour.
- Victory Boulevard and Cebra Avenue (Intersection 35 on Figure 14-6)
  - o Reallocating green time would fully mitigate the potential significant adverse traffic impacts at this intersection for the Saturday MD peak hour.
  - o Potential significant adverse traffic impacts during the Weekday AM, MD, and PM peak hours would be unmitigable.
- Victory Boulevard and Jersey Street (Intersection 36 on Figure 14-6)
  - o Reallocating green time would fully mitigate the potential significant adverse traffic impact at this intersection for the Weekday AM peak hour.

- o Potential significant adverse traffic impacts during the Weekday MD, PM, and Saturday MD peak hours would be unmitigable.
- Victory Boulevard and Forest Avenue (Intersection 38 on Figure 14-6)
  - o Reallocating green time would fully mitigate the potential significant adverse traffic impacts at this intersection for the Weekday MD and Saturday MD peak hours.
  - o Reallocating green time would partially mitigate the potential significant adverse traffic impacts at this intersection for the Weekday PM peak hour.
- Bay Street and Vanderbilt Avenue (Intersection 45 on Figure 14-6)
  - Reallocating green time would mitigate the potential significant adverse traffic impacts at this intersection for the Weekday AM, MD, and Saturday MD peak hours.
  - o Reallocating green time would partially mitigate the potential significant adverse traffic impacts at this intersection for the Weekday PM peak hour.
- Bay Street and School Road (Intersection 49 on Figure 14-6)
  - Reallocating green time would mitigate the potential significant adverse traffic impacts at this intersection for the Weekday AM, MD, and Saturday MD peak hours.
  - Reallocating green time and changing the offset would partially mitigate the potential significant adverse traffic impacts at this intersection for the Weekday PM peak hour.

## Unmitigatable Significant Adverse Traffic Impacts

Due to congested conditions on multiple approaches, constrained right-of-way, and/or low volumes that do not meet signal warrants, signal timing and/or geometric measures to mitigate the potential significant adverse impacts at the following study locations are not feasible. Therefore, these intersections could not be mitigated and the impacts are considered significant and unavoidable.

- Richmond Terrace and Ferry Terminal (bus) (Intersection 8 on Figure 14-6)
  - O Potential significant adverse traffic impacts are not expected at this intersection during the Weekday AM peak hour; however, the proposed signal timing change is recommended to help resolve the potential significant adverse traffic impact expected at Richmond Terrace and Ferry Terminal (parking lot) during the Weekday AM peak hour.
- Victory Boulevard and Bay Street/St. Marks Place (Intersection 11 on Figure 14-6)
  - O Potential significant adverse traffic impacts are not expected at this intersection during the Weekday AM peak hour; however, the modified offset is recommended to help resolve the potential significant adverse traffic impact expected at Victory Boulevard and Bay Street during the Weekday AM peak hour.
- Bay Street and William Street (Intersection 22 on Figure 14-6)
  - The implementation of mitigation measures at adjacent intersections would result in new potential significant impacts for the northbound approach at this intersection during the Weekday MD and Saturday MD peaks hours, which would be unmitigable.
  - o Potential significant adverse traffic impacts during the Weekday AM and PM peak hours would be unmitigable.

- Bay Street and Congress Street (Intersection 23 on Figure 14-6)
  - o The implementation of mitigation measures at adjacent intersections would result in a new potential significant impact for the northbound approach at this intersection during the Weekday PM peak hour, which would be unmitigable.
- Vanderbilt Avenue and Tomkins Avenue (Intersection 44 on Figure 14-6)
- Bay Street and Hylan Boulevard (Intersection 48 on Figure 14-6)

Tables  $21-\underline{6}$  through  $21-\underline{13}$  show the v/c ratios, delays, and LOS for impacted lane groups at each intersection with implementation of these mitigation measures and compares them to No-Action and With-Action conditions for the Weekday AM, MD, PM, and Saturday MD peak hours. Tables  $21-\underline{6}$  through 21-12 also show that significant adverse impacts would be fully mitigated at all but 11 lane groups at 6 intersections during the Weekday AM peak hour, 24 lane groups at 11 intersections during the Weekday MD peak hour, 44 lane groups at 20 intersections during the Weekday PM peak hour, and 14 lane groups at 9 intersections during the Saturday MD peak hour. In total, impacts to one or more approach movements would remain unmitigated in one or more peak hours at 21 intersections. Consequentially, these impacts would constitute unavoidable significant adverse traffic impacts as a result of the Proposed Actions (refer to Chapter 23, "Unavoidable Adverse Impacts").

Table 21- $\underline{6}$ : Signalized Level of Service Analysis – Weekday AM Peak Hour No-Action vs. With-Action vs. Mitigated Conditions

with	-Action vs.	Mittig	atea	Cona	Itto	18												
			No-Act	ion Cond	itions			With-Ac	tion Con	ditions			With-A	ction Wit	h Mitigati	on Con	ditions	
#	Intersection & Approach	Lane Group	v/c Ratio	Delay (sec)	LOS	Queue Length (ft)	Lane Group	v/c Ratio	Delay (sec)	LOS	Queue Length (ft)		Lane Group	v/c Ratio	Delay (sec)	LOS	Queue Length (ft)	
-	Richmond Terrace	and Frank	din Aven	ue		(,					()						(,	
	Eastbound	TR	0.77	9.2	Α	332	TR	0.81	11.0	В	363		TR	0.79	19.0	В	473	
1	Westbound	LT	0.88	37.3	D	634	LT	1.09	80.3	F	640	+	LT	1.00	42.5	D	844	
	Northbound	LR	0.25	37.1	D	112	LR	0.26	37.1	D	112		LR	0.27	39.0	D	115	
		Inters		22.7	С		Inters	ection	42.5	D			Inters	ection	30.4	С		
	Richmond Terrace Eastbound	and Jerse	1.07	87.4	F	197		1.36	208.5	F	360	H.	-	1.02	68.7	Е	264	-
	Easibound	TR	0.70	7.4	A	332	TR	0.75	8.6	A	432	+	TR	0.71	15.0	В	727	1
	Westbound	LT	1.06	68.6	E	941	LT	1.18	110.7	F	1051	+	IIX	0.71	13.0	Ь	121	
	W colbound	R	0.00	7.7	A	1	R	0.00	9.0	A	1							
2													L	0.10	9.9	Α	12	
2													TR	0.94	37.9	D	860	
	Northbound	L	0.09	35.6	D	37	L	0.09	35.6	D	37	Ш	L	0.11	39.9	D	40	
	O th h	TR	0.26	38.3	D	102	TR	0.27	38.4	D	103	ш	TR	0.32	43.5	D	109	<u> </u>
	Southbound	L	0.01	34.0	С	11	L TR	0.01	34.0	0	11	$\vdash$	L	0.02	38.0	D	11	<del> </del>
		TR Inters	0.08	35.3 45.9	D D	43	Inters	0.08	35.3 80.4	D F	43	$\vdash$	TR Inters	0.10 ection	39.5 33.6	D	45	<del>                                     </del>
	Richmond Terrace				U	-	1111015	JULIUIT	00.4	Г	-	H	111612	COLIOTI	JJ.0	U		<del>                                     </del>
	Eastbound	TR	0.78	13.9	В	231	TR	0.83	17.0	В	279		TR	0.83	11.7	В	206	
3	Westbound	LT	0.71	47.0	D	636	LT	0.87	88.8	F	779	+	LT	0.87	43.2	D	779	
	Northbound	LR	0.37	35.0	D	158	LR	0.37	35.0	D	158		LR	0.37	35.0	D	158	
		Inters		29.9	С		Inters	ection	49.6	D			Inters	ection	27.6	С		
	Hamilton Avenue a				-	400		0.04	40.0	-	4.47			0.04	40.4	-	454	
5	Northbound Southbound	LT TR	0.71	13.2 9.0	В	139 87	LT TR	0.81	19.3 9.7	В	147 101		LT TR	0.81	19.1 9.2	B A	151 101	
	Southbourid	Inters		11.2	A B	01	Inters		14.9	A B	101		Inters		14.6	В	101	<b>!</b>
	Wall Street and Ric			11.2	Ь		IIIIGIS	CLIOIT	14.9	Ь			IIILEIS	ection	14.0	В		
	Westbound	LTR	0.18	28.8	С	75	LTR	0.18	28.8	С	75		LTR	0.18	28.8	С	75	
	W colbound	L	0.23	29.9	Č	71	L	0.23	29.9	Č	71		L	0.23	29.9	Č	71	
7	Northbound	Т	0.48	11.7	В	134	Т	0.54	12.9	В	223		Т	0.54	11.8	В	141	
		R	0.29	10.9	В	63	R	0.29	10.7	В	61		R	0.29	10.0	В	57	
	Southbound	LTR	0.46	7.4	Α	43	LTR	0.50	7.7	Α	45		LTR	0.50	7.2	Α	45	
	5:	Inters		11.4	В		Inters	ection	12.0	В			Inters	ection	11.2	В		
	Richmond Terrace	and Ferry	0.47	45.7	D	173		0.47	45.7	D	470		-	0.49	47.2	D	175	
	Westbound	R	0.47	45.7	D	108	R	0.47	45.7	D	173 108		R	0.49	46.9	D	109	
8	Northbound	T	0.41	13.2	В	80	T	0.47	18.0	В	80		T	0.46	13.5	В	83	
	Southbound	Ť	0.63	85.6	F	478	Ť	0.67	88.0	F	512		Ť	0.66	88.5	F	512	
		Inters		50.2	D		Inters		52.4	D			Inters		50.9	D		
	Richmond Terrace			l (parking	lot)													
	Westbound	L	0.74	55.7	Е	315	L	0.74	55.7	Е	315		L	0.77	58.7	Е	336	
		R	0.20	11.8	В	47	R	0.20	11.8	В	47		R	0.21	12.6	В	50	Ш
_	Northbound	T	0.78	39.0	D	257	T	0.91	51.5	D	358	+	T	0.85	34.2	С	335	<u> </u>
9		R R	0.35	16.1 15.4	B B	209 121	R R	0.35	16.5 16.0	В	233 133	$\vdash$	R R	0.34	19.6 18.8	B B	278 159	1
	Southbound	IX.	5.82	2211.1	F	573	I R	5.70	2156.9	F	573	$\vdash$	- IX	5.82	2210.1	F	574	<del>                                     </del>
	Souribouriu	TR	0.55	2.6	A	5	TR	0.59	3.4	A	17		TR	0.59	3.4	A	18	
		Inters		285.6	F		Inters		268.9	F				ection	271.4	F		
	Bay Street and Slo																	
	Eastbound	LR	0.10	32.7	С	41	LR	0.13	33.3	С	52		LR	0.13	33.3	С	52	
10	Northbound	L	0.69	30.0	С	158		1.07	89.9	F	328	+	L	0.82	42.2	D	299	
	Cauthhamai	T	0.66 0.71	14.1	В	254 314	TD	0.72	14.9 22.2	В	315 467	Ш	T	0.72 0.91	21.0	C	365	<u> </u>
	Southbound	TR Inters		19.9 18.4	B B	314	TR Inters		27.5	OO	40/	$\vdash$	TR	0.91 ection	43.6 33.3	D C	555	$\vdash$
	Victory Boulevard						inters	JULIUIT	21.5	·		H	inters	COLIUII	JJ.J	U		$\vdash$
	Eastbound	TR	0.35	6.2	A	56	TR	0.47	9.2	Α	107	$\vdash$	TR	0.47	12.6	В	151	
	Labiboaria	R	0.36	6.3	A	43	R	0.38	8.1	A	63		R	0.38	11.5	В	94	
44	Westbound	T	0.44	16.8	В	248	T	0.51	27.5	C	244		T	0.51	17.0	В	329	
11		L	0.07	4.9	Α	11	L	0.08	5.0	Α	11		L	0.08	4.8	Α	12	
	Southbound	LT	0.44	42.8	D	166	LT	0.45	43.0	D	169		LT	0.45	43.0	D	169	
		R	0.35	41.9	D	115	R	0.35	42.2	D	116		R	0.35	42.2	D	116	Ш
		Inters	ection	16.6	В		Inters	ection	20.5	С			Inters	ection	18.7	В		1

Table 21-<u>6</u>: Signalized Level of Service Analysis – Weekday AM Peak Hour No-Action vs. With-Action vs. Mitigated Conditions (con't)

NO-A	ction vs. W	itn-A	ction	VS. IV	litig	atea (	Lonai	tions	(con	tj								
			No-Act	ion Cond	itions			With-Ac	tion Cond	ditions			With-A	ction Wit	th Mitigati	on Con	ditions	
#	Intersection & Approach	Lane Group	v/c Ratio	Delay (sec)	LOS	Queue Length (ft)	Lane Group	v/c Ratio	Delay (sec)	LOS	Queue Length (ft)		Lane Group	v/c Ratio	Delay (sec)	LOS	Queue Length (ft)	
	Victory Boulevard	and Bay S	treet															
	Eastbound	L	0.58	31.3	С	197		0.82	49.9	D	328	+	<u>L</u>	0.77	41.3	D	312	
	Westbound	LT LTR	0.58	31.4 31.8	C	198 45	LT LTR	0.77 0.40	43.5 39.2	D D	320 115		LT LTR	0.72	36.6 36.4	ם ם	304 111	<b>—</b>
12	Northbound	LIK	0.09	32.8	C	123	LIK	1.15	97.3	F	142	+	LIK	0.86	44.6	D	159	
	Horanboana	TR	0.67	17.6	В	243	TR	0.75	19.6	В	230		TR	0.78	15.0	В	234	
	Southbound	LT	0.53	7.1	Α	43	LT	0.68	9.3	Α	48		LT	1.02	40.1	D	416	
		R	0.36	7.0	A	30	R	0.38	7.1	A	32		R	0.63	11.2	В	24	
	Bay Street and Han	Interse		17.1	В		Inters	ection	28.0	С			Interse	ection	28.3	С	-	$\vdash$
	Eastbound	LTR	0.09	30.2	С	57	LTR	0.09	30.2	С	57		LTR	0.07	24.6	С	51	
	Westbound	LTR	0.86	56.7	Е	518	LTR	1.12	117.1	F	734	+	LTR	0.91	58.7	Е	638	
	Northbound	LTR	1.09	82.4	F	352	LTR	1.28	158.2	F	830	+		0.00	44.0	<u> </u>	00	
13													L TR	0.63 1.01	41.8 98.5	D F	98 656	+
	Southbound	L	1.52	284.4	F	436	L	2.69	798.1	F	555	+	L	1.46	255.8	F	312	_
		Т	0.39	8.2	Α	104	Т	0.41	9.7	Α	138		Т	0.60	34.6	С	231	
		R	0.17	2.1	A	16	R	0.18	3.0	A	20		R	0.26	15.6	В	41	
$\vdash$	Front Street and Ha	Interse		71.8	Е		Inters	ection	162.4	F		$\vdash$	Interse	CUON	82.6	F		
	Eastbound	TR	0.32	4.0	Α	61	TR	0.36	3.9	Α	63		TR	0.36	3.9	Α	63	
14	Westbound	LT	0.08	13.2	В	45	LT	0.09	13.2	В	45		LT	0.09	13.2	В	45	
	Northbound	LR	0.56	23.9	С	264	LR	0.77	32.1	С	381		LR	0.77	32.1	С	381	
	Bay Street and Swa	Interse		15.0	В		Inters	ection	20.0	В			Interse	ection	20.0	В		<b>—</b>
	Eastbound	L	0.94	125.1	F	362	L	1.11	128.3	F	449	+	L	0.95	119.2	F	407	
		LTR	1.09	125.2	F	488	LTR	1.06	127.8	F	467		LTR	0.91	117.0	F	426	
15	Westbound	LTR	0.03	30.0	C	11	LTR	0.03	30.0	С	11		LTR	0.02	25.3	С	10	
	Northbound Southbound	LTR LTR	0.45	6.8 11.2	A B	46 111	LTR LTR	0.57 0.48	9.4	A B	48 105		LTR LTR	0.62	29.9 18.9	C B	318 155	$\vdash$
	Southbound	Interse		42.4	D	- ' ' ' '		ection	41.5	D	103		Interse		49.5	D	133	H
	Bay Street and Gra																	
	Eastbound												LTR	0.36	42.8	D	123	
18	Westbound		He	signalize	a			He	signalize	4			R TR	0.05	36.4 7.2	D A	26 125	<b>—</b>
	Northbound Southbound		O.	isigilalize	u			O.	isigilalize	u		Н	T	0.41	76.8	E	972	+
													Interse		42.7	D		
	Van Duzer Street a																	
19	Westbound Northbound	TR LT	0.22	41.1 13.8	D B	60 305	TR LT	0.28	43.9 14.8	D B	75 333		TR LT	0.28	36.9 14.8	D B	86 333	
	Northbourid	Interse		16.5	В	303	Inters		18.2	В	333		Interse		17.4	В	333	
	Bay Street and Clin																	
	Westbound	LTR	0.11	30.6	С	59	LTR	0.12	31.1	С	59		LTR	0.14	33.9	C	63	
20	Northbound	L TR	0.07	20.3	C	17 305	L TR	0.23	27.7 27.5	C	29 398		L TR	0.17	5.6 5.3	A	<u>3</u> 47	
20	Southbound	L	0.17	12.3	В	51	L	0.22	16.1	В	54		L	0.20	3.9	A	6	
		TR	0.84	33.8	С	563	TR	0.97	66.1	Е	940	+	TR	0.92	31.2	С	356	
		Interse	ection	29.0	С		Inters	ection	45.8	D			Interse	ection	18.6	В		
	Bay Street and Balt Eastbound	ic Street											LTR	0.19	38.7	D	61	
0.4	Westbound												LTR	0.01	35.0	C	10	
21	Northbound		Un	signalize	d			Un	signalize	d			TR	0.75	16.5	В	360	
	Southbound												LT	0.97	30.2	С	922	
	Bay Street and Way	e Street											Interse	ection	24.1	С	-	
	Westbound		0.18	28.4	С	53	LTR	0.19	28.2	С	49							
													L	0.13	39.8	D	44	
													TR	0.19	41.3	D	60	
24	Northbound	LT R	0.54	18.7 14.0	B B	264 43	LT R	0.70 0.13	18.5 12.0	B B	327 34		LT R	0.60	13.2 7.7	B A	380 37	
	Southbound	L	0.26	7.0	A	23	L	0.38	10.6	В	27		L	0.11	2.2	A	3	
		TR	0.85	23.5	С	807	TR	1.08	77.8	Е	1021	+	TR	0.94	17.2	В	42	
		Interse		20.8	С		Inters	ection	49.0	D			Interse	ection	15.6	В		
	Front Street and War	ave Street	0.30	19.3	68	LR	0.32	19.9	В	60	$\vdash\vdash$	LR	0.32	26.3	С	78	<b>—</b>	
25	Northbound	LT	0.66	5.0	B A	29	LT	0.32	7.6	A	23		LT	0.32	8.8	A	108	
1 1	Southbound	TR	0.40	10.7	В	116	TR	0.55	13.2	В	176		TR	0.51	14.4	В	223	
		Interse		8.7	Α		Inters	ection	11.0	В			Interse	ection	12.7	В		
	Front Street and Pr Eastbound	ospect St LTR		21.8	С	47	LTR	0.26	22.2	С	47	$\vdash\vdash$	LTR	0.33	37.0	D	90	<u> </u>
1	Westbound Westbound	LTR	0.26	45.1	D	227	LTR	0.26	45.7	D	228		LTR	0.33	40.7	D	80 255	
26	Northbound	TR	0.77	41.6	D	218	TR	0.96	70.6	E	514	+	TR	0.76	27.0	С	249	
	Southbound	LT	0.83	31.7	С	301	LT	1.25	152.2	F	665	+	LT	0.84	29.9	С	429	
		Interse	ection	37.9	D		Inters	ection	93.2	F			Interse	ection	31.7	С		ш

Table 21-6: Signalized Level of Service Analysis – Weekday AM Peak Hour No-Action vs. With-Action vs. Mitigated Conditions (con't)

With	-Action vs.	Mitig	ated	Cond	itioı	ıs (co	n't)											
			No-Act	ion Cond	itions			With-Ac	tion Con	ditions			With-A	ction Wit	h Mitigat	ion Con	ditions	
#	Intersection & Approach	Lane Group	v/c Ratio	Delay (sec)	LOS	Queue Length (ft)	Lane Group	v/c Ratio	Delay (sec)	LOS	Queue Length (ft)		Lane Group	v/c Ratio	Delay (sec)	LOS	Queue Length (ft)	
	Van Duzer Street a	nd Beach	Street															
	Eastbound	LT	0.87	57.7	Е	391	LT	0.90	62.5	E	413	+	LT	0.88	58.1	Е	404	
27	Westbound	TR	0.25	28.9	С	106	TR	0.26	29.1	С	110		TR	0.25	28.3	С	109	_
	Northbound		0.32	15.5	В	172	L	0.33	15.7	В	178		L	0.34	16.3	В	182	<u> </u>
		TR	0.88 ection	37.0	D	731	TR	0.91 ection	41.6	D	783		TR	0.93 ection	44.4	D D	793	┢
	Bay Street and Wa		ection	37.2	D	L	IIILEIS	ection	40.6	D			IIILEIS	ection	41.0	U		┢
	Westbound	LTR	0.20	32.9	С	85	LTR	0.21	33.0	С	85		LTR	0.31	44.8	D	98	t
20	Northbound	L	0.56	24.5	Ċ	73	L	1.72	388.5	F	190	+	L	0.70	23.1	C	19	T
28		Т	0.60	24.7	С	277	Т	0.77	73.9	Е	419	+	Т	0.67	7.0	Α	109	
	Southbound	TR	0.81	67.8	Е	299	TR	1.04	80.7	F	862	+	TR	0.90	40.9	D	368	
			ection	47.0	D		Inters	ection	93.4	F			Inters	ection	27.3	С		
	Bay Street and Car	nal Street																_
	Eastbound	L	0.34	38.1	D	112	L	0.37	39.3	D	119		L	0.37	37.8	D	119	▙
29	\\/ = a4b =	TR	0.20	32.2	C	89	TR LTR	0.20	32.3	C	89 68		TR	0.22	32.6	C D	99 91	₩
29	Westbound Northbound	LTR TR	0.18 0.61	29.8 8.2	C A	49 81	TR	0.31	33.9 58.0	E	102		LTR TR	0.31	36.2 15.0	В	204	₩
	Southbound		0.61	71.9	E	694	LT	0.77	75.0	E	755	-	T	0.77	45.8	D	853	t
		Intersection		40.6	D		Intersection		62.9	E	, 55		Intersection	•	32.1	С	555	t
	Front Street and Ca													•				
	Eastbound	LR	0.39	24.1	С	79	LR	0.41	23.3	С	77		LR	0.47	32.3	С	120	
30	Northbound	LT	0.42	11.0	В	122	LT	0.53	12.6	В	162		LT	0.44	11.2	В	181	
	Southbound	TR	0.55	10.9	В	92	TR	0.68	10.8	В	90		TR	0.58	5.3	Α	93	
			ection	13.0	В		Inters	ection	13.1	В			Inters	ection	11.0	В		
	Bay Street and Bro				_	400			40.0	_	225							▙
	Eastbound	LR	0.34	41.0	D	186	LR	0.44	42.3	D	235		_	0.00	20.0		100	▙
													R	0.28	36.6 38.1	D D	129 115	
31	Northbound	LT	0.62	18.9	В	332	LT	1.04	69.0	Е	691	+	LT	0.91	33.5	C	560	t
	Southbound	T	0.71	11.0	В	221	T	0.92	39.2	D	404	_	T	0.88	26.2	C	287	1
	Codinboana	R	0.12	6.9	A	35	R	0.18	11.8	В	52		R	0.18	10.3	В	48	f
		Inters	ection	16.8	В		Inters		48.1	D			Inters	ection	28.7	С		
	Richmond Terrace	and Clove																
	Eastbound		0.89	27.9	С	895	LT	0.93	33.7	С	962		LT	0.93	33.7	С	962	
		R	0.16	4.4	Α	27	R	0.16	4.5	A	27		R	0.16	4.5	Α	27	<u> </u>
32	Westbound	L	0.56	25.1	С	56	L	0.68	42.0	D	87		L	0.68	42.0	D	87	₩
	No while a const	TR LTR	0.57 0.44	12.4	B D	284 193	TR LTR	0.66	15.3 39.2	В	390 208		TR LTR	0.66 0.47	15.3 39.2	B D	390	₩
	Northbound		ection	38.4 22.5	С	193	Inters		26.8	DC	∠∪8			ection	26.8	С	208	1
	Victory Boulevard			ZZ.J			111010		20.0	U			1111010		20.0			$\vdash$
	Eastbound	L	0.55	56.2	Е	95	L	0.56	57.5	Е	96		L	0.56	57.5	Е	96	1
		TR	0.82	60.2	Е	304	TR	0.82	60.2	Е	304		TR	0.82	60.2	Е	304	
	Westbound	L	0.59	60.5	Е	112	L	0.74	76.0	Е	152	+	L	0.74	76.0	Е	152	+
35		TR	0.69	50.2	D	292	TR	0.71	51.3	D	300		TR	0.71	51.3	D	300	
	Northbound	LT	0.66	16.2	В	284	LT	0.76	19.8	В	421		LT	0.76	19.8	В	421	
	O - vith h - v - d	R	0.11	10.0	A	30	R	0.12	10.0	В	33		R	0.12	10.0	В	33	-
	Southbound	LTR	0.68 ection	19.7 31.8	B C	473 0	LTR Inters	0.93	42.2 38.9	D D	649		LTR	0.93 ection	41.2 38.6	D D	650	₩
	Victory Boulevard			31.0	C	U	inters	DOLIOI I	36.9	ט			inters	CUIUII	30.0	ע		┢
	Eastbound	L L	0.18	8.1	Α	27		0.22	9.4	Α	34			0.23	11.4	В	38	┢
	200.000110	Ť	0.68	12.1	В	238	T	0.78	15.0	В	351		Ť	0.81	18.7	В	382	Т
36	Westbound	Ť	0.50	21.2	C	303	Ť	0.55	20.4	C	325		Ť	0.57	24.7	C	334	
		R	0.10	13.3	В	47	R	0.16	12.9	В	61		R	0.17	16.7	В	74	
	Southbound	LR	0.47	40.9	D	172	LR	0.68	50.2	D	242	+	LR	0.61	44.3	D	232	
			ection	18.0	В		Inters	ection	20.8	С			Inters	ection	23.3	С		_
	Victory Boulevard				_	050	- 15	0.75	45.0		000		- 15	0 ==	45.0	_	000	<u> </u>
	Eastbound	LR	0.72	44.1	D	253	LR	0.75	45.6	D	268		LR	0.75	45.6	D	268	₩
38	Northbound	L	0.24	14.5 74.4	B E	74 373	L	0.27	15.0 75.8	B E	76 454		L T	0.27 0.66	15.0 75.8	B E	76 454	⊢
30	Southbound	÷	0.58	21.3	C	186	÷	0.66	24.1	С	216		Ť	0.66	24.1	C	216	$\vdash$
	Couribouliu	R	0.40	4.1	A	22	R	0.43	4.2	A	25		R	0.43	4.2	A	25	t
			ection	41.0	D		Inters		42.8	D				ection	42.8	D		Н

Table 21-<u>6</u>: Signalized Level of Service Analysis – Weekday AM Peak Hour No-Action vs. With-Action vs. Mitigated Conditions (con't)

			No-Act	ion Cond	itions			With-Ac	tion Cond	ditions			With-A	ction Wit	h Mitigati	on Con	ditions	ı
#	Intersection & Approach	Lane Group	v/c Ratio	Delay (sec)	LOS	Queue Length (ft)	Lane Group	v/c Ratio	Delay (sec)	LOS	Queue Length (ft)		Lane Group	v/c Ratio	Delay (sec)	LOS	Queue Length (ft)	1
	Broad Street and C	anal Stree	et															Ι
	Eastbound	L	0.24	12.3	В	97	_	0.26	12.4	В	91		L	0.26	10.3	В	91	Ι
		TR	0.47	15.9	В	219	TR	0.52	16.2	В	235		TR	0.52	14.0	В	252	Τ
41	Westbound	LTR	0.16	16.9	В	86	LTR	0.22	16.1	В	102		LTR	0.25	17.0	В	111	Т
41	Northbound	L	0.47	44.2	D	102	L	0.50	46.2	D	103		L	0.50	46.2	D	103	T
		TR	0.54	41.2	D	199	TR	0.53	41.1	D	198		TR	0.53	41.1	D	198	T
	Southbound	LT	0.39	37.2	D	161	LT	0.47	39.3	D	187		LT	0.47	39.3	D	187	Т
		Interse	ection	26.5	С		Inters	ection	26.4	С			Interse	ection	25.6	C		1
	Broad Street and V	an Duzer	Street															T
	Westbound	L	0.74	91.9	F	225	L	0.78	89.9	F	243		L	0.78	30.7	С	257	1
42	Southbound	L	0.27	6.4	Α	122	L	0.29	8.3	Α	143		L	0.29	8.3	Α	143	1
		Т	0.50	8.8	Α	301	Т	0.53	11.5	В	356		Т	0.53	11.5	В	356	٦
		Interse	ection	22.0	С		Inters	ection	26.7	С			Interse	ection	14.6	В		٦
	Broad Street and Ta	argee Stre	eet															1
	Eastbound	LT	0.55	47.4	D	336	LT	0.56	53.7	D	336	+	LT	0.57	29.3	С	279	1
12	Westbound	TR	0.36	41.7	D	193	TR	0.47	41.3	D	249		TR	0.48	38.5	D	267	٦
13	Northbound	LT	0.98	52.5	D	834	LT	1.00	58.7	Ē	868	+	LT	0.99	54.3	D	858	٦
		R	0.45	18.5	В	188	R	0.51	20.1	С	225		R	0.50	19.3	В	220	٦
		Interse		44.4	D		Inters		48.2	D			Interse		41.2	D		٦
	Vanderbilt Avenue	and Tomp	kins Ave	nue														٦
	Eastbound	LTR	0.88	40.4	D	741	LTR	0.95	49.9	D	826	+	LTR	0.95	49.9	D	826	٦
	Westbound	LTR	0.43	15.2	В	145	LTR	0.51	16.2	В	141		LTR	0.51	16.5	В	144	٦
4	Northbound	LTR	1.26	177.2	F	476	LTR	1.37	220.2	F	529	+	LTR	1.37	220.2	F	529	-
	Southbound	LTR	1.08	99.8	F	587	LTR	1.12	113.7	F	618	+	LTR	1.12	113.7	F	618	┪
	Countracting	Interse		79.8	Ē	00.		ection	94.6	F	0.0		Interse		94.6	F	0.0	٦
	Bay Street and Van			70.0				0011011	04.0					3011011	04.0			٦
	Eastbound	I	0.44	24.7	С	96		0.63	27.7	С	141			0.64	28.7	С	144	┪
	Lastboaria	R	0.44	24.9	Č	89	R	0.44	25.4	Ĉ	82		R	0.45	26.2	Č	84	┪
15	Northbound	LT	0.74	13.9	B	235	ĹŤ	0.99	46.8	D	659	+	LT	0.96	38.4	D	644	7
•	Southbound	Ť	0.63	28.8	C	491	Ť	0.81	35.8	D	567	Ė	T	0.80	33.8	C	584	-
	Coulibouria	R	0.25	5.9	A	77	R	0.31	8.2	A	86		R	0.31	7.3	A	83	┪
		Interse		20.2	Ĉ	- ' '	Inters		33.1	Ĉ	- 00		Interse		30.0	Ĉ	- 00	-
	Bay Street and Edg			20.2	Ŭ			0011011	00.1	Ū				3011011	00.0	Ŭ		-
	Westbound	LR	0.42	34.5	С	182	LR	0.51	36.2	D	224		LR	0.51	36.2	D	224	-
	Northbound	TR	0.37	8.5	A	70	TR	0.45	9.3	A	62		TR	0.45	9.3	A	62	-
7	Southbound	T	0.69	12.3	В	361	T	0.45	23.4	C	533	$\vdash$	T	0.45	23.4	C	556	٦
	Northwestbound	R	0.03	0.5	A	0	R	0.20	0.6	A	0	$\vdash$	R	0.20	0.6	A	0	٦
	T TOTAL TO COLD COLLIG	Interse		14.9	В		Inters		19.8	В	Ů		Interse		19.8	В	_	٦
	Bay Street and Hyla			17.0					10.0			$\vdash$			10.0			٦
	Eastbound	LTR	0.73	29.8	С	208	LTR	0.86	41.0	D	505	$\vdash$	LTR	0.86	41.0	D	505	٦
	Westbound	LTR	1.02	100.6	F	449	LTR	1.04	106.0	F	454	+	LTR	1.04	106.0	F	454	٦
8	Northbound	LTR	1.31	176.2	F	696	LTR	2.54	713.8	F	800	+	LTR	2.54	716.3	F	912	٦
-	Southbound	T	0.82	39.1	D	546	T	1.05	73.0	Ė	876	+	T	1.05	72.9	Ė	876	٦
	Coulibodila	R	0.82	10.0	A	67	R	0.37	11.8	В	90	ŕ	R	0.37	11.8	В	90	٦
		Interse		85.5	F	01	Inters		249.5	F	30		Interse		250.2	F	30	۲
	Bay Street and Sch		- 5	00.0			.111013	- 5	2-70.0			$\vdash$			200.2			٦
	Eastbound	I	1.06	93.1	F	660	-	1.21	146.1	F	792	+	L	1.07	91.4	F	738	٦
	Lasibouliu	TR	0.14	13.3	В	48	TR	0.14	13.3	В	48	-	TR	0.13	11.3	В	43	۲
	Westbound	LTR	0.00	23.5	С	7	LTR	0.00	23.5	С	7		LTR	0.00	20.0	В	6	-
19	Northbound	LTR	0.00	13.6	В	47	LTR	0.00	13.6	В	47	$\vdash$	LTR	0.00	16.7	В	52	4
	Southbound	LTR	0.09	6.4	A	20	LTR	0.09	5.6	A	25	$\vdash$	LTR	0.10	10.7	В	35	4
	Southbound	R	0.09	3.9	A	30	R	0.18	4.9	A	20	$\vdash$	R	0.20	5.8	A	42	4
		Interse		37.9	D	30	Inters		56.6	E	20	$\vdash$	Interse		37.8	D	42	4
		11110130	JULIUII	<b>■</b> 31.9			1111013	COHOII	0.00				11110130	JULIUII	37.0			J

Table 21- $\underline{7}$ : Signalized Level of Service Analysis – Weekday MD Peak Hour No-Action vs. With-Action vs. Mitigated Conditions

VVIU	-Action vs	. Milu	gatet	ı Culi	uiu	)115	_						_					
			No-Act	ion Cond	itions			With-Ac	tion Con	ditions			With-A	ction Wit	h Mitigati	on Con	ditions	
Int #	Intersection &	Lane Group	v/c Ratio	Delay (sec)	LOS	Queue Length (ft)	Lane Group	v/c Ratio	Delay (sec)	LOS	Queue Length (ft)		Lane Group	v/c Ratio	Delay (sec)	LOS	Queue Length (ft)	
IIIL#	Approach Richmond Terrace	and Frank	din Avon			(11)					(11)						(11)	Н
	Eastbound	TR	0.66	11.7	В	366	TR	0.71	13.2	В	404		TR	0.70	11.9	В	423	H
1	Westbound	LT	0.91	11.8	В	129	LT	1.04	35.5	D	116		LT	1.01	37.5	D	1014	
	Northbound	LR	0.19	36.2	D	81	LR	0.19	36.2	D	81		LR	0.20	37.1	D	82	
		Inters		12.8	В		Inters	ection	25.5	С			Inters	ection	26.0	С		
	Richmond Terrace	and Jerse		27.0		444		0.00	20.5		400			0.50	45.0	-	<b>67</b>	$\blacksquare$
	Eastbound	TR	0.66	37.6 27.1	D C	111 558	TR	0.66	36.5 32.1	D C	102 612		TR	0.52 0.78	15.9 37.1	В	57 822	$\vdash$
	Westbound	LT	1.44	227.7	F	1256	LT	1.69	337.5	F	1332	+	IIX	0.76	37.1		022	
	Westboard	R	0.02	8.5	A	4	R	0.02	8.3	Ä	3	Ė						
2													L	0.34	17.8	В	52	
													TR	0.91	42.8	D	653	
	Northbound	L	0.10	34.5	С	37	L	0.10	34.5	С	37		L	0.13	39.8	٥	40	ш
	0	TR	0.18	35.4	D	83	TR	0.19	35.5	D	88		TR	0.23	41.0	О	94	Н
	Southbound	L	0.02	32.8	С	13	L	0.02	32.8	С	13	<b>—</b>	L	0.02	37.4	ם ם	14	Н
		TR Inters	0.33	37.8 118.0	D F	131	TR Inters	0.33	37.8 169.4	D F	131	<del>                                     </del>	TR Inters	0.40 ection	44.3 38.0	D D	141	Н
	Richmond Terrace						1111015	COLIUIT	109.4				111015	COUCH	JO.U	U		H
	Eastbound	TR	0.81	20.9	С	346	TR	0.87	24.6	С	633		TR	0.87	30.9	С	878	
3	Westbound	LT	0.80	71.4	Е	424	LT	0.91	80.8	F	863	+	LT	0.91	31.1	С	863	
	Northbound	LR	0.45	37.0	D	186	LR	0.45	37.0	D	187		LR	0.45	38.0	D	187	
		Inters		44.9	D		Inters	ection	50.7	D			Inters	ection	31.8	С		
	Hamilton Avenue a Northbound	nd Richm ⊥T	0.90	22.7	С	526	ΙT	0.98	33.9	С	589		ΙΤ	0.98	33.9	С	589	$\vdash$
5	Southbound	TR	0.90	12.1	В	153	TR	0.98	13.0	В	172		TR	0.98	12.0	В	172	+
	Southbound	Inters		18.3	В	155	Inters		25.1	С	172		Inters		24.7	С	172	$\vdash$
	Wall Street and Ric			10.5	ט		IIICIO	COLIOIT	23.1				IIICIS	COLIOIT	24.1	U		H
	Westbound	LTR	0.86	66.0	Е	376	LTR	0.86	66.5	Е	376		LTR	0.86	66.5	Е	376	
		L	0.98	93.5	F	350	L	0.98	95.3	F	350		L	0.98	95.3	F	350	
7	Northbound	T	0.56	10.4	В	337	T	0.59	11.8	В	370		T	0.59	11.8	В	370	
		R	0.51	11.5	В	292	R	0.51	11.5	В	292		R	0.51	11.5	В	292	
	Southbound	LTR Inters	0.59	14.6 27.4	B C	95	LTR Inters	0.65	15.5 27.8	B C	101		LTR Inters	0.65	17.1 28.2	ВС	101	ш
_	Richmond Terrace				U		mers	ection	21.8	U			mers	ection	28.2	C		lacktriangledown
	Westbound	and Ferry	0.98	134.0	F	165		0.98	139.4	F	165	+		0.98	139.4	F	165	+
	TT COLDOURIG	R	0.46	51.0	D	63	R	0.46	51.0	D	63	Ė	R	0.46	51.0	D	63	Ħ
8	Northbound	Т	0.66	19.0	В	57	T	0.70	34.1	С	57		T	0.70	33.8	С	57	М
	Southbound	Т	0.88	65.2	Е	521	Т	0.92	82.4	F	569	+	T	0.92	82.4	F	569	+
		Inters		47.1	D		Inters	ection	62.0	E			Inters	ection	61.9	Е		
	Richmond Terrace	and Ferry				0.5		0.50	10.1	_	05	_		0.50	40.4		0.5	ш
	Westbound	L	0.53	48.4 15.8	D B	95	L	0.53	48.4	D	95 19	<b>-</b>	L R	0.53 0.11	48.4	D B	95	$\vdash$
	Northbound	R T	0.11	15.8 64.6	E	19 429	R T	0.11 1.03	16.6 91.1	B F	469	+	T	1.03	16.6 92.2	F	19 469	
9	Northbourid	R	0.38	17.0	В	58	R	0.18	16.7	В	58	H	R	0.18	16.9	В	58	H
		R	0.20	17.5	В	32	R	0.20	17.2	В	32		R	0.20	17.3	В	32	П
	Southbound	L	1.80	425.3	F	92	١	1.76	404.1	F	90		L	1.76	404.1	F	90	
		TR	1.11	69.4	E	882	TR	1.17	93.8	F	890	+	TR	1.17	93.8	F	890	+
	D 011 1 01	Inters		74.0	Е		Inters	ection	93.8	F			Inters	ection	94.3	F		щ
	Bay Street and Slos			24.7		EC	LD	0.20	20.2	_	109	-	LD	0.42	21.7	С	115	$\vdash$
	Eastbound Northbound	LR L	0.17 0.61	24.7 31.2	C	56 61	LR L	0.38	28.2 50.0	C D	90	+	LR L	0.43	31.7 32.4	C	115 76	$\vdash$
10	Nonthbound	÷	0.90	15.7	В	180	+	0.89	17.3	В	287	Ť	+	0.88	29.2	С	485	Н
	Southbound	TR	1.17	103.1	F	689	TR	1.21	122.1	F	724	+	TR	1.15	95.2	F	696	М
		Inters		59.8	E		Inters		69.4	E				ection	60.8	Е		
	Victory Boulevard	and Bay S			ice													
	Eastbound	TR	0.42	18.5	В	188	TR	0.53	22.8	С	237		TR	0.53	22.8	С	237	
	100 0	R	0.45	18.6	В	167	R	0.51	20.2	С	184	_	R	0.51	20.2	C	184	Щ
11	Westbound	Ţ	0.81	89.8	F	382	Ţ	0.95	86.1	F	344	-	T	0.95	57.8	E	56 3	$\vdash$
	Southbound	LT	0.11	18.8 31.9	B C	18 171	LT	0.13 0.54	17.6 32.3	B C	13 174	<del>                                     </del>	LT	0.13 0.54	4.4 32.3	A C	174	$\vdash$
	Southbound	R	0.53	33.3	C	107	R	0.53	35.5	D	111		R	0.53	35.5	D	111	Н
		Inters		50.2	D		Inters		50.5	D	<del>-                                    </del>			ection	38.5	D		М

Table 21-<u>7</u>: Signalized Level of Service Analysis – Weekday MD Peak Hour No-Action vs. With-Action vs. Mitigated Conditions (con't)

With	-Action vs	. Miti	gated	d Con	ditio	ons (c	on't)											
			No-Act	tion Cond	itions			With-Ac	tion Con	ditions			With-A	ction Wit	h Mitigati	ion Con	ditions	
Int #	Intersection & Approach	Lane Group	v/c Ratio	Delay (sec)	LOS	Queue Length (ft)	Lane Group	v/c Ratio	Delay (sec)	LOS	Queue Length (ft)		Lane Group	v/c Ratio	Delay (sec)	LOS	Queue Length (ft)	
	Victory Boulevard	and Bay S																
	Eastbound	L LT	0.62 0.61	31.5 30.6	C	186 144	L LT	0.90	60.2 41.1	E D	272 262	+	L LT	1.05 0.91	104.3 67.0	F E	306 298	+
	Westbound	LTR	0.35	26.7	C	93	LTR	1.40	228.6	F	401	+	LTR	1.75	381.3	F	434	+
12	Northbound	L	2.78	829.5	F	176	L	3.62	1204.3	F	164	+	L	1.67	323.1	F	160	
	Southbound	TR LT	0.86	26.3 41.9	C D	172 318	TR LT	0.89 1.20	26.2 126.2	C F	162 348	+	TR LT	0.81 1.28	19.6 143.9	B F	350 426	+
	Southbound	R	0.90	93.8	F	225	R	1.20	90.4	F	245	_	R	1.20	159.3	F	322	+
		Inters	ection	98.4	F		Inters	ection	165.8	F			Inters		135.6	F		
	Bay Street and Han Eastbound		0.07	17.8	В	35	LTR	0.07	17.9	В	35		LTR	0.07	18.5	В	36	
	Westbound	LTR	0.67	15.2	В	76	LTR	0.07	30.9	С	359		LTR	0.07	40.5	D	392	
	Northbound	LTR	1.82	394.1	F	799	LTR	2.04	488.8	F	853	+						
13												_	L TR	0.92 1.15	66.8 92.9	E F	95	
	Southbound	L	4.65	1675.8	F	429	L	5.97	2255.1	F	426	+	L	2.40	653.3	F	609 327	
1		Т	0.73	11.9	В	142	T	0.79	14.5	В	141		T	1.01	36.0	D	308	
		R Inters	0.30	3.0	A F	1	R	0.41	8.9	A F	26		R Inters	0.61	15.0 122.5	B F	70	Ш
	Front Street and Ha			321.1		•	inters	ection	439.6		•	H	inters	COLIUIT	122.5			Н
	Eastbound	TR	0.38	10.2	В	0	TR	0.45	10.1	В	0		TR	0.45	11.6	В	4	
14	Westbound Northbound	LT LR	0.10 0.52	13.4 23.1	B C	47 243	LT LR	0.10 0.88	13.4 45.8	B D	47 424		LT LR	0.11 0.85	14.0 40.8	B D	48 413	
	Nonnbound	Inters		16.2	В	243		ection	26.4	С	424	+	Inters		24.9	С	413	
	Bay Street and Swa		Van Duze	r Street		•											•	
	Eastbound	L	0.61	31.9	С	185	L	0.68	36.2	D	220		L	0.68	37.6	D	220	
15	Westbound	LTR LTR	0.60	31.6 17.5	C B	177 5	LTR LTR	0.67	35.8 17.5	D B	210 5		LTR LTR	0.67	37.1 17.5	D B	210 5	
	Northbound	LTR	0.71	64.5	Ē	309	LTR	0.78	66.3	Ē	407		LTR	0.78	37.1	D	406	
	Southbound	LTR	0.83	17.3	В	146	LTR	0.90	19.9	В	183		LTR	0.90	14.0	В	77	
	Bay Street and Gra	Interse nt Street	ection	37.5	D		Inters	ection	40.2	D			Inters	ection	26.4	С		
	Eastbound												LTR	0.15	28.5	С	46	
18	Westbound												R	0.17	28.6	С	55	
	Northbound Southbound		Ur	nsignalize	ea			Un	signalize	a			TR T	0.51 1.54	5.7 272.7	A F	70 1359	+
													Inters		153.3	F	1000	
	Van Duzer Street a			24.4	_		TD	0.00	244	_			TD	0.00	24.0		64	
19	Westbound Northbound	TR LT	0.36	34.4 9.3	C A	62 152	TR LT	0.36 0.52	34.1 9.6	C A	60 163		TR LT	0.36 0.52	34.2 9.6	C A	64 163	
		Inters	ection	14.2	В		Inters	ection	14.3	В			Inters		14.4	В		
	Bay Street and Clin	ton Stree		23.7	С	89	LTR	0.29	23.7	С	89		LTR	0.37	29.2	С	99	
	Westbound Northbound	LIK	0.29 0.41	20.1	C	11	LIK	0.29	20.1	C	10		LIK	0.37	18.0	В	99	
20		TR	0.66	18.0	В	138	TR	0.73	18.7	В	136		TR	0.66	13.3	В	144	
	Southbound	L TR	0.35	7.9 188.1	A	12 1236	L TR	0.42	10.5 242.5	B F	12 1310	_	L TR	0.34	8.8 177.9	A F	7 148	
		Inters	1.37 ection	101.7	F F	1230		1.49 ection	129.3	F	1310	+	Inters	1.35 ection	95.3	F	140	
	Bay Street and Balt	tic Street																
	Eastbound Westbound											-	LTR LTR	0.21	39.6 35.2	D D	32 17	
21	Northbound		Ur	nsignalize	d			Un	signalize	d			TR	0.89	12.9	В	144	H
	Southbound												LT	1.28	142.5	F	61	+
	Bay Street and Way	e Street										-	Inters	ection	82.0	F		
	Westbound	LTR	0.31	25.4	С	77	LTR	0.30	25.0	С	78							
													L	0.35	40.3	D	46	
24	Northbound	LT	1.38	204.3	F	826	LT	1.56	279.3	F	940	+	TR LT	0.40 1.17	42.7 104.1	D F	50 864	$\vdash$
	. torti bodi id	R	0.13	13.6	В	26	R	0.13	13.3	В	25		R	0.09	4.9	A	14	
	Southbound	L	0.84	41.2	D	17	L	0.82	38.8	D	16		L	0.45	9.3	A	10	
		TR Interse	1.43 ection	215.4 196.0	F F	658	TR Inters	1.55 ection	268.9 255.4	F F	665	+	TR Interse	1.20 ection	107.4 99.9	F F	250	Н
	Front Street and W			150.0				- 50.071	200.7					- 5.10/1	55.5			
	Eastbound		0.28	18.7	В	47	LR	0.29	19.0	В	47		LR	0.30	23.9	C	69	
25	Northbound Southbound	LT TR	0.65 0.47	6.2 11.4	A B	12 154	LT TR	0.79 0.58	9.9 13.2	A B	11 203	<u> </u>	LT TR	0.70 0.52	6.2 14.1	A B	56 251	$\vdash$
	Souriboullu	Inters		9.4	A	1.5-4		ection	12.0	В	200		Inters		10.9	В	201	
	Front Street and Pr			a : -													-	
	Eastbound Westbound	LTR LTR	0.20	21.5 22.4	C	43 65	LTR LTR	0.21	21.6 22.5	C	45 65	<del> </del>	LTR LTR	0.27	36.7 35.5	D D	66 94	Н
26	Northbound	TR	1.00	72.5	E	369	TR	1.22	141.8	F	466	+	TR	0.80	23.5	С	284	
	Southbound	LT	1.43	231.4	F	380	LT	2.56	731.1	F	517	+	LT	0.92	35.1	D	514	
		Inters	ection	133.2	F		Inters	ection	384.1	F			Inters	ection	30.0	С		

Table 21-<u>7</u>: Signalized Level of Service Analysis – Weekday MD Peak Hour No-Action vs. With-Action vs. Mitigated Conditions (con't)

			No-Act	ion Cond	itions			With-Ac	tion Con	ditions			With-A	ction Wit	h Mitigati	on Con	ditions	П
Int #	Intersection & Approach	Lane Group	v/c Ratio	Delay (sec)	LOS	Queue Length (ft)	Lane Group	v/c Ratio	Delay (sec)	LOS	Queue Length (ft)		Lane Group	v/c Ratio	Delay (sec)	LOS	Queue Length (ft)	
	Van Duzer Street a	nd Beach	Street							•				•				
	Eastbound	LT	0.77	41.3	D	215	LT	0.81	44.7	D	232		LT	0.81	44.7	D	232	
27	Westbound	TR	0.35	24.8	С	105	TR	0.37	25.2	С	111		TR	0.37	25.2	С	111	
21	Northbound	L	0.41	13.9	В	171	L	0.41	13.9	В	171		L	0.41	13.9	В	171	
		TR	0.69	21.0	С	326	TR	0.71	22.0	С	344		TR	0.71	22.0	С	344	
		Interse	ection	24.3	С		Inters	ection	25.6	С			Interse	ection	25.6	С		
	Bay Street and Wat		0.00	00.0		81	LTD	0.00	26.7		- 00		LTR	0.41	00.5	D	92	ш
	Westbound Northbound	LTR L	0.28 1.72	26.8 348.4	C F	89	LTR L	0.28 1.77	373.4	C F	80 82	+	LIR	1.75	36.5 362.7	F	92	←
28	Northbourid	Ť	1.10	63.8	E	187	Ť	1.23	120.2	F	175	+	<u> </u>	1.73	62.5	E	299	+
	Southbound	TR	1.38	204.5	F	897	TR	1.49	252.9	F	996	+	TR	1.29	156.6	F	1060	Н
	Countracting	Interse		147.8	F	- 00.	Inters		195.7	F	- 000		Interse		122.9	F	1000	
	Bay Street and Can	al Street				•					•							
	Eastbound	L	0.73	171.3	F	186	L	0.64	161.1	F	165		L	0.98	151.3	F	216	
		TR	0.24	20.9	С	73	TR	0.24	20.8	С	73		TR	0.41	32.3	С	109	
29	Westbound	LTR	0.20	141.3	F	51	LTR	0.28	144.2	F	66		LTR	0.42	72.9	E	76	ш
	Northbound	TR	1.22	119.4	F	59	TR	1.39	196.5	F	71	+	TR	1.13	75.5	Е	58	ш
	Southbound	LT	3.31	1052.7	F	618	LT	3.64	1201.2	F	642	+	T	1.24	127.3	F	632	ш
	Front Street and Ca	Intersection		547.2	F		ntersection	n	643.7	F			Intersection	n	101.1	F		Н
	Eastbound	LR	0.60	27.5	С	98	LR	0.67	31.3	С	113		LR	0.51	29.8	С	111	Н
30	Northbound	LT	0.60	14.1	В	189	LT	0.69	16.9	В	240		LT	0.72	24.3	C	359	
	Southbound	TR	0.49	11.7	В	60	TR	0.60	13.5	В	48		TR	0.62	16.4	В	185	
		Interse		15.4	В		Inters		17.8	В			Interse	ection	21.9	С		
	Bay Street and Bro	ad Street																
	Eastbound	LR	0.25	26.7	С	107	LR	0.32	25.6	С	140							
													L	0.36	32.0	С	130	ш
31	Newthern	17	0.74	40047	_	200	17	111	4440.4	_	070		R	0.13	29.7	C	43	ш
	Northbound Southbound	LT T	3.71 1.25	1234.7	F	239 114	LT T	4.11 1.36	1418.4 186.7	F	272 119	+	LT T	3.38 1.18	1087.7 102.6	F	485 266	Н
	Southbound	R	0.20	136.3 14.3	В	15	R	0.25	14.5	В	119	+	R	0.21	102.6	В	36	Н
		Interse		574.6	F	10	Inters		666.5	F	13		Interse	_	493.2	F	30	Н
	Richmond Terrace			0	•				000.0						100.2			
	Eastbound	LT	0.65	18.4	В	539	LT	0.69	20.1	С	571		LT	0.69	20.1	С	571	
		R	0.13	2.3	Α	26	R	0.13	2.5	Α	30		R	0.13	2.5	Α	30	
32	Westbound	L	0.35	21.1	С	98	L	0.42	24.2	С	117		L	0.42	24.2	С	117	
		TR	0.85	37.6	D	826	TR	0.89	40.7	D	898		TR	0.89	40.7	D	898	ш
	Northbound	LTR Interse	0.47	39.4 28.0	D C	202	LTR Inters	0.50	40.2 30.2	D C	215		LTR Interse	0.50	40.2 30.2	D C	215	ullet
	Victory Boulevard			28.0	C	<u> </u>	mers	ection	30.2	U	<u> </u>		mers	ection	30.2	C		Н
	Eastbound	IIIU CEDIA	0.30	31.8	С	43		0.31	32.7	С	43			0.31	32.7	С	43	Н
		TR	0.76	42.7	D	240	TR	0.76	42.7	D	240		TR	0.76	42.7	D	240	М
35	Westbound	L	0.69	51.5	D	120	L	0.69	51.0	D	119		L	0.69	51.0	D	119	
35		TR	0.73	40.2	D	262	TR	0.76	42.2	D	291		TR	0.76	42.2	D	291	
	Northbound	LTR	0.90	35.4	D	616	LTR	1.00	52.7	D	721	+	LTR	1.00	52.6	D	721	+
	Southbound	LTR	1.17	105.3	F	579	LTR	1.35	181.5	F	611	+	LTR	1.35	181.5	F	611	+
	Vietem Beuleum I	Interse		62.9	E	<u> </u>	Inters	ection	97.3	F	l		Interse	ection	97.3	F		ш
	Victory Boulevard a Eastbound	and Jerse	0.78	43.6	D	36		1.42	235.8	F	98	+		1.42	235.8	F	98	+
	Lasibound	T	0.78	39.7	D	485	T	1.42	68.2	F	493	+	T	1.42	68.3	E	493	+
36	Westbound	÷	1.05	70.0	E	700	÷	1.14	103.6	F	796	+	Ė	1.14	103.9	F	796	+
	TT COLDOURIG	R	0.19	13.8	В	67	R	0.34	16.8	В	95		R	0.34	16.9	В	95	
	Southbound	LR	0.50	28.3	С	146	LR	0.93	67.5	Е	263	+	LR	0.93	67.5	E	263	+
		Interse		50.1	D		Inters	ection	88.2	F			Interse		88.4	F		
	Victory Boulevard																	
	Eastbound	LR	0.45	27.5	С	138	LR	0.48	27.9	С	146		LR	0.54	31.2	С	154	$ldsymbol{\sqcup}$
20	Northbound	L	0.78	52.2	D	171	L	0.99	103.9	F	192	+	L	0.79	51.6	D	171	ш
38	Canalita i i	Ţ	0.69	22.1	С	366	T	0.76	25.1	C F	424	H.,	T	0.71	21.0	С	391	Н
	Southbound	T R	0.83	75.8 2.9	E A	349 10	R	0.90 0.41	80.3 3.0	A	474 11	+	R R	0.85	74.1 2.6	E A	378 9	Н
		Interse		39.2	D D	10	Inters		44.5	D	- 11		Interse		38.9	D	J	Н
-		11110130	COUCH	JJ.Z	U		1111015	COLIOIT	44.5	U			1111013	COHOLI	JU.3	U		

Table 21-<u>7</u>: Signalized Level of Service Analysis – Weekday MD Peak Hour No-Action vs. With-Action vs. Mitigated Conditions (con't)

			No-Act	ion Cond	itions			With-Ac	tion Cond	ditions			With-A	ction Wit	h Mitigati	on Con	ditions	I
Int#	Intersection & Approach	Lane Group	v/c Ratio	Delay (sec)	LOS	Queue Length (ft)	Lane Group	v/c Ratio	Delay (sec)	LOS	Queue Length (ft)		Lane Group	v/c Ratio	Delay (sec)	LOS	Queue Length (ft)	
	Broad Street and C	anal Stree																Ţ
	Eastbound	L	0.31	10.4	В	65	L	0.31	11.4	В	73		L	0.31	11.4	В	73	4
		TR	0.34	9.8	Α	95	TR	0.39	11.3	В	136		TR	0.39	11.3	В	136	4
41	Westbound	LTR	0.30	20.0	С	144	LTR	0.34	22.0	С	173		LTR	0.38	22.0	С	176	4
	Northbound	L	0.49	33.0	С	98	L	0.47	31.8	С	97		L	0.47	31.8	С	97	+
	Caudhhaina	TR LT	0.63	33.6	C	211	TR LT	0.62	32.9	C	207	$\vdash$	TR LT	0.62	32.9	C	207	+
	Southbound	Interse	0.37	26.2 22.6	C	136	Inters	0.35	25.8 22.5	C	130	-	Interse	0.35	25.8 22.5	C	130	+
	Broad Street and V			22.0	C		IIILEIS	ection	22.5	U		$\vdash$	IIILEIS	ECLIOIT	22.5	C		+
	Westbound	ali Duzei .	0.78	56.0	Е	168		0.82	54.3	D	196		L	0.82	54.3	D	196	+
42	Southbound	L	0.78	8.9	A	76	-	0.02	9.5	A	76		L	0.19	9.5	A	76	+
	Southboaria	Ť	0.60	14.3	В	314	Ť	0.64	16.0	В	327		Ť	0.64	16.0	В	327	t
		Interse		25.0	C	014	Inters		26.3	C	021		Interse		26.3	C	OZ1	+
	Broad Street and Ta				Ŭ				_0.0	Ŭ		$\vdash$	510					t
	Eastbound	TR	0.33	29.8	С	155	TR	0.34	29.7	С	156	П	TR	0.34	29.7	С	156	1
	Westbound	TR	0.58	29.9	Č	227	TR	0.65	32.0	Č	262		TR	0.65	31.9	Č	262	†
43	Northbound	LT	0.77	24.7	C	355	LT	0.79	26.0	C	373		LT	0.79	26.0	C	373	1
		R	0.40	14.3	В	113	R	0.48	15.8	В	139		R	0.48	15.8	В	139	1
		Interse	ection	24.6	С		Inters	ection	25.8	С			Interse	ection	25.8	С		1
	Vanderbilt Avenue	and Tomp	kins Ave	nue														T
	Eastbound	LTR	1.00	63.3	E	552	LTR	1.06	79.5	E	603	+	LTR	1.06	79.5	E	603	T
44	Westbound	LTR	0.78	9.9	Α	71	LTR	0.92	14.3	В	243		LTR	0.92	25.4	C	307	I
	Northbound	LTR	1.25	162.3	F	463	LTR	1.29	177.3	F	489	+	LTR	1.29	177.3	F	489	I
	Southbound	LTR	0.99	69.1	Е	497	LTR	0.98	67.3	Е	489		LTR	0.98	67.3	Е	489	1
		Interse		72.3	Е		Inters	ection	79.9	Е			Interse	ection	82.8	F		
	Bay Street and Van	derbilt Av																1
	Eastbound	L	0.48	27.1	С	106	L	0.61	28.9	С	134		L	0.69	32.7	С	143	ļ
		R	0.21	24.2	С	36	R	0.21	24.1	С	35		R	0.24	27.2	С	37	4
45	Northbound	LT	5.20	1912.8	F	1176	LT	8.44	3368.1	F	1266	+	LT	3.68	1225.0	F	1147	4
	Southbound	T	1.20	105.3	F	458	Т	1.25	128.1	F	366	+	T	1.14	80.3	F	360	4
		R	0.37	1.5	A	10	R	0.46	1.8	A	12		R	0.42	1.4	A	11	4
	D 04 1 E I	Interse		730.2	F		Inters	ection	1216.8	F			Interse	ection	458.4	F		4
	Bay Street and Edg Westbound			23.2	С	124	LR	0.40	04.4	С	150		I D	0.40	24.1	С	450	4
	Northbound	LR TR	0.36	16.9	В	74	TR	0.42	24.1 17.6	В	73		LR TR	0.42	17.6	В	150 73	+
47	Southbound	T	0.96	28.7	С	328	T	1.00	33.6	С	326	-	T	1.00	34.1	С	372	+
	Northwestbound	R	0.25	0.6	A	0	R	0.27	0.8	A	0	-	R	0.27	0.8	A	0	t
	Northwestboard	Interse		20.8	Ĉ	- 0	Inters		23.0	Ĉ	- 0		Interse		23.2	Ĉ		t
	Bay Street and Hyla			20.0	U		ii itoro	0011011	20.0	U			ii koro.	0011011	20.2	U		t
	Eastbound	LTR	1.03	81.1	F	534	LTR	1.12	110.0	F	594	+	LTR	1.12	110.0	F	594	1
	Westbound	LTR	0.90	66.8	Ē	300	LTR	0.92	69.9	E	302		LTR	0.92	69.9	E	302	1
48	Northbound	LTR	4.89	1762.1	F	751	LTR	6.45	2463.6	F	774	+	LTR	6.45	2463.6	F	849	1
	Southbound	Т	1.12	97.0	F	572	T	1.21	134.6	F	642	+	T	1.21	134.7	F	642	j
		R	0.58	18.0	В	170	R	0.64	18.7	В	190		R	0.64	18.7	В	190	
		Interse	ection	587.6	F		Inters	ection	821.6	F			Interse	ection	821.6	F		J
	Bay Street and Sch	ool Road																J
	Eastbound	L	1.35	195.2	F	786	L	1.48	252.6	F	881	+	L	1.34	189.8	F	846	1
		TR	0.12	12.1	В	39	TR	0.12	12.1	В	39		TR	0.10	10.2	В	35	1
49	Westbound	LTR	0.01	15.2	В	8	LTR	0.01	15.2	В	8		LTR	0.01	13.0	В	7	1
-13	Northbound	LTR	0.22	15.2	В	83	LTR	0.22	15.2	В	83		LTR	0.24	17.9	В	91	1
	Southbound	LTR	0.08	16.7	В	23	LTR	0.08	17.0	В	21		LTR	0.09	17.7	В	22	1
		R	0.71	6.7	Α	325	R	0.71	7.0	Α	325		R	0.71	7.0	Α	325	J
		Interse	ection	82.1	F		Inters	ection	107.0	F			Interse	ection	81.9	F		Т

Table 21- $\underline{8}$ : Signalized Level of Service Analysis – Weekday PM Peak Hour No-Action vs. With-Action vs. Mitigated Conditions

VVILL	i-Action vs	. 1411113	gatet	CUII	uitit	7115												
			No-Act	ion Cond	itions			With-Ac	tion Con	ditions			With-A	ction Wit	h Mitigati	ion Con	ditions	
Int #	Intersection & Approach	Lane Group	v/c Ratio	Delay (sec)	LOS	Queue Length (ft)	Lane Group	v/c Ratio	Delay (sec)	LOS	Queue Length (ft)		Lane Group	v/c Ratio	Delay (sec)	LOS	Queue Length (ft)	
	Richmond Terrace	and Frank	din Aven	ue						•				•	•			M
	Eastbound	TR	0.75	28.8	С	738	TR	0.84	34.6	С	837		TR	0.77	21.6	С	713	
1	Westbound	LT	1.14	81.4	F	278	LT	1.52	253.0	F	689	+	LT	1.12	73.8	Е	1138	
	Northbound	LR	0.14	35.3	D	67	LR	0.14	35.4	D	68		LR	0.19	41.6	D	74	
		Inters		56.4	Е		Inters	ection	147.0	F			Inters	ection	49.0	D		Ш
	Richmond Terrace Eastbound	and Jerse		39.2	D	106		0.81	48.3	D	92	+		0.71	33.9	С	87	<b>—</b>
	Easibound	TR	0.72	28.1	С	598	TR	0.81	36.8	D	956	+	TR	0.71	32.4	С	935	$\vdash$
	Westbound	LT	1.29	163.2	F	1186	LT	1.73	353.4	F	1134	+	- 110	0.01	OZT	Ŭ	500	
		R	0.01	11.1	В	4	R	0.01	9.8	A	3							
2													L	0.38	18.6	В	39	
													TR	0.97	77.6	Е	682	+
	Northbound	L	0.20	39.5	D	42	L	0.20	39.5	D	42		L	0.23	42.4	D	44	
		TR	0.19	37.0	D	88	TR	0.20	37.3	D	91		TR	0.21	39.0	D	93	
	Southbound		0.04	34.7	С	23	L	0.04	34.7	С	23	<b>—</b>		0.04	36.4	D	23	$\vdash$
		TR Inters	0.68	49.9	D F	255	TR Inters	0.68	49.9	D F	255	<b>—</b>	TR	0.72 ection	54.4 51.8	D D	261	<del></del>
	Richmond Terrace			85.2			mers	CCHOIT	165.5				mers	CCHOIT	ე1.გ	υ		$\vdash$
	Eastbound	TR	0.88	25.8	С	409	TR	0.98	47.9	D	456	+	TR	0.96	32.2	С	236	
3	Westbound	ĹŤ	0.78	78.1	Ē	344	LT	1.10	101.3	F	935	+	LT	1.00	80.5	F	904	
	Northbound	LR	0.52	38.5	D	223	LR	0.52	38.5	D	223		LR	0.55	41.8	D	229	
		Inters		47.6	D		Inters	ection	67.3	Е			Inters	ection	52.2	D		
	Hamilton Avenue a				_	0=1				_	0.10					-	0.10	_
5	Northbound	LT	0.87	21.5	С	371	LT	0.99	36.3	D	612		LT	0.99	36.3	D	612	_
	Southbound	TR Inters	0.48	34.0 26.8	C	331	TR Inters	0.54	33.6 35.1	C D	366		TR	0.54 ection	29.8 33.5	C	366	Н
	Wall Street and Ric			20.8	U		IIILEIS	ection	35.1	U	L		IIILEIS	ection	33.5	C		$\vdash$
	Westbound	LTR	0.66	185.5	F	312	LTR	0.66	185.5	F	312		LTR	0.66	185.5	F	312	$\vdash$
	TT COLDOURIG	L	0.62	175.4	F	273	L	0.62	177.9	F	273		L	0.62	177.9	F	273	
7	Northbound	Т	0.55	4.5	Α	38	T	0.60	5.2	Α	52		T	0.60	5.2	Α	52	
		R	0.51	5.6	Α	32	R	0.51	6.1	Α	39		R	0.51	6.1	Α	39	
	Southbound	LTR	0.61	8.3	Α	73	LTR	0.71	11.7	В	93		LTR	0.71	11.7	В	93	
		Inters		45.1	D		Inters	ection	44.1	D			Inters	ection	44.1	D		Щ
	Richmond Terrace	and Ferry	0.67	1 <b>(bus)</b> 57.7	E	174	L	0.67	57.7	E	174			0.67	F7 7	Е	174	<u> </u>
	Westbound	R	0.87	44.1	D	84	R	0.87	44.1	D	84		R	0.87	57.7 44.1	D	84	$\vdash$
8	Northbound	T	0.72	75.4	Ē	65	T	0.78	80.1	F	63	+	T	0.78	80.1	F	63	+
	Southbound	Ť	0.90	80.1	F	712	Ť	0.98	87.1	F	832	+	Ť	0.98	87.1	F	832	+
		Inters	ection	75.5	E		Inters	ection	81.0	F			Inters	ection	81.0	F		
	Richmond Terrace	and Ferry																
	Westbound	L	0.77	58.0	E	286	L	0.77	58.0	E	286		L	0.77	58.0	Е	286	
	Mantheau I	R	0.16	13.2	В	40 60F	R	0.16	13.2	В	40	<b>—</b>	R	0.16	13.2	В	40	H
9	Northbound	T R	1.38 0.26	208.0	F A	695 12	T R	1.50 0.26	260.0 3.2	F A	775 22	+	T R	1.50 0.26	261.1 3.4	F A	775 22	+
"		R	0.26	3.2	A	6	R	0.26	4.5	A	11		R	0.26	4.6	A	11	Н
	Southbound	L	4.16	1457.1	F	350	L	4.16	1451.3	F	314		L	4.16	1451.3	F	314	П
		TR	0.91	55.7	Ē	332	TR	1.00	64.5	Ē	1022	+	TR	1.00	64.5	E	1022	+
		Inters		206.2	F		Inters	ection	222.4	F			Inters	ection	222.8	F		
	Bay Street and Slo																	
	Eastbound	LR	0.20	34.4	С	80	LR	0.60	44.6	D	218		LR	0.60	44.6	D	218	ш
10	Northbound	L T	0.57	32.6 46.1	C D	89 381	L T	0.59	30.8 64.1	C E	82 402	<b>.</b>	L T	0.72 0.90	36.8 33.0	D C	80 525	lacksquare
	Southbound	TR	0.86 1.13	95.5	F	928	TR	1.20	125.6	F	1023	+	TR	1.14	97.9	F	990	$\vdash$
	Southbound	Inters		69.9	E	320		ection	91.2	F	1023	Ε-		ection	65.1	E	330	$\vdash$
	Victory Boulevard					-					•							М
	Eastbound	TR	0.39	12.6	В	157	TR	0.42	13.3	В	175		TR	0.42	13.3	В	175	
		R	0.33	11.9	В	105	R	0.42	13.2	В	133		R	0.42	13.2	В	133	
11	Westbound	Т	0.74	37.6	D	151	Т	0.91	62.5	Е	225	+	Т	0.91	59.7	Е	148	+
		L .=	0.08	3.2	A	3	L -	0.08	5.0	A	4		L	0.08	6.5	Α	5	ш
	Southbound	LT R	0.56 0.91	46.6 84.4	D F	209 263	LT R	0.58	47.3 98.1	D F	214 275	+	LT D	0.58	48.6 98.1	D F	214 275	$\vdash$
			ection	34.9	C	∠03		ection	98.1 47.1	D	2/0	+	R Inters	ection	98.1 46.0	D	2/5	$\vdash$
		1111615	COLIUIT	J4.9	J		1111615	COLIUII	47.1	U			1111613	COLIUIT	40.0	U		

Table 21-8: Signalized Level of Service Analysis – Weekday PM Peak Hour No-Action vs. With-Action vs. Mitigated Conditions (con't)

With	-Action vs	<u>. Mit</u> i	gated	l Con	<u>diti</u> d	ons (c	on't)											
	<u>-</u>		No-Act	ion Cond	itions			With-Ac	tion Cond	ditions			With-A	ction Wit	h Mitigati	on Con	ditions	П
Int #	Intersection & Approach	Lane Group	v/c Ratio	Delay (sec)	LOS	Queue Length (ft)	Lane Group	v/c Ratio	Delay (sec)	LOS	Queue Length (ft)		Lane Group	v/c Ratio	Delay (sec)	LOS	Queue Length (ft)	
	Victory Boulevard									-	0=1					-		
	Eastbound	L LT	0.84	72.0 72.9	E	320 325	L LT	0.90	83.1 95.2	F	351 363	+	L LT	0.84	85.0 91.3	F	331 343	+
	Westbound	LTR	0.75	57.8	Ē	204	LTR	2.61	756.6	F	863	+	LTR	2.19	573.1	F	828	+
12	Northbound	_	2.23	577.1	F	222	L	3.75	1255.3	F	246	+	٦	2.10	522.7	F	352	Ш
	Southbound	TR LT	0.70	16.7 14.1	B B	262 130	TR LT	0.73 1.08	17.8 55.4	B E	204 172	+	TR LT	0.77 1.36	29.1 183.6	C F	497 692	+
	Coumbound	R	0.76	11.9	В	70	R	0.89	27.9	C	108	·	R	1.16	92.5	F	457	+
		Inters		60.2	Е		Inters	ection	210.2	F			Inters	ection	193.2	F		
	Bay Street and Har Eastbound	LTR	0.11	30.5	С	64	LTR	0.11	30.7	С	64		LTR	0.09	25.0	С	57	
	Westbound	LTR	0.88	58.9	Ĕ	529	LTR	1.13	122.3	F	683	+	LTR	0.90	55.5	Ë	586	
	Northbound	LTR	1.18	118.7	F	740	LTR	1.39	208.7	F	866	+	-	0.57	40.0	D	400	
13													TR	0.57	42.8 89.5	F	102 618	$\vdash$
	Southbound	١	2.51	711.6	F	666	١	4.09	1404.1	F	698	+	L	2.43	667.8	F	501	
		T R	0.55	24.3	C	374	T	0.66	22.3	С	331		T	1.01	44.4	D	403	ш
		Inters	0.29 ection	7.6 141.5	A F	67	R Inters	0.38 ection	10.8 281.9	B F	69		R Interse	0.62 ection	17.4 141.2	B F	96	Н
	Front Street and Ha	annah Stre	eet															
14	Eastbound Westbound	TR LT	0.45	3.7 13.3	A B	67 47	TR LT	0.55 0.10	4.0 13.4	A B	72 47		TR LT	0.55	4.0 13.4	A B	72 47	Н
1.4	Northbound	LR	0.10	25.2	C	289	LR	0.10	37.5	D	424		LR	0.83	37.5	D	424	H
		Inters		13.8	В		Inters	ection	18.4	В			Inters	ection	18.4	В		
	Bay Street and Swa Eastbound	an Street/\	/an Duze 0.63	70.6	Е	192	L	0.68	114.9	F	202	+		0.68	115.7	F	202	+
	Ladiboaria	LTR	0.61	65.9	Ē	215	LTR	0.67	115.4	F	228	+	LTR	0.67	116.1	F	228	+
15	Westbound	LTR	0.00	0.0	0.0	0	LTR	0.00	0.0	0.0	0		LTR	0.00	0.0	0.0	0	
	Northbound Southbound	LTR LTR	0.55 0.67	20.5 5.9	C A	262 41	LTR LTR	0.61 0.81	21.9 8.2	C A	318 42		LTR LTR	0.61	15.4 22.3	B C	200 90	
		Inters		20.8	C			ection	27.8	C			Inters		32.6	C		
	Bay Street and Gra	nt Street											LTD	0.24	40.0	_	440	
	Eastbound Westbound												LTR R	0.31	40.8 38.1	D D	110 73	Н
18	Northbound		Ur	nsignalize	d			Un	signalize	d			TR	0.46	6.1	Α	89	
	Southbound												T Inters	1.45	231.6 132.5	F	1754	+
	Van Duzer Street a	nd Clintor	Street										IIICIO	COLIOTI	102.0			
19	Westbound	TR	0.28	37.4	D	79	TR	0.32	38.3	D	86		TR	0.32	41.1	D	88	
	Northbound	LT Inters	0.39 ection	9.2 15.1	A B	146	LT Inters	0.40 ection	9.3 15.8	A B	150		Inters	0.40 ection	9.3 16.5	A B	150	H
	Bay Street and Clir	ton Stree	1								•							
	Westbound Northbound	LTR	0.39	117.0 11.4	F B	153 5	LTR L	0.41	710.4 10.2	F B	154 5	+	LTR	0.83	84.3 12.0	F B	212	Н
20	Northbourid	TR	0.53	5.7	A	113	TR	0.40	5.8	A	100		TR	0.52	3.9	A	42	Н
	Southbound	L	0.31	9.7	Α	20	L	0.40	11.1	В	15		L	0.28	4.9	Α	9	
		TR Inters	1.14	89.3 54.8	F D	1319	TR Inters	1.38 ection	193.5 144.6	F F	1725	+	TR Inters	1.15	79.3 47.0	E D	160	
	Bay Street and Bal		cotion	34.0			inters	COLIOTI	144.0				intero	oction	47.0			
	Eastbound												LTR	0.16	44.2	D	37	
21	Westbound Northbound		Ur	nsignalize	d			Un	signalize	d			LTR TR	0.01	39.5 37.4	D D	9 53	$\blacksquare$
	Southbound												LT	1.27	136.5	F	1202	+
	Bay Street and Way	io Stroot											Inters	ection	92.6	F		Н
	Westbound	LTR	0.40	37.1	D	74	LTR	0.41	35.2	D	54							
													L	0.29	51.0	D	55	+
24	Northbound	LT	1.11	84.0	F	944	LT	1.42	215.9	F	1267	+	TR LT	0.46 1.26	59.3 142.8	E F	83 1183	+
	rtoranboaria	R	0.06	7.7	A	16	R	0.07	7.9	A	16		R	0.06	4.3	A	11	
	Southbound	L	0.30	17.7	В	28	L	1.08	99.4	F	33	+	L	0.44	10.8	В	15	Ш
		TR Interse	1.17 ection	110.2 93.9	F F	1011	TR Inters	1.39 ection	207.1	F F	1029	+	TR Inters	1.25 ection	132.8 130.6	F	431	+
	Front Street and W	ave Street			•													
25	Eastbound	LR	0.22	16.0	В	41	LR	0.25	17.5	В	33		LR	0.38	36.2	D	66	Щ
25	Northbound Southbound	LT TR	0.82	7.3 11.6	A B	21 161	LT TR	1.09 0.64	59.5 14.4	E B	20 233	+	LT TR	0.80	13.0 9.8	B A	226	Н
		Inters	ection	9.6	A			ection	38.3	D			Inters		12.8	В		
	Front Street and Pr			20.0		04	LTD	0.54	20.0		00		LTD	0.50	42.0	Г	140	П
	Eastbound Westbound	LTR LTR	0.53	28.6 24.6	C	81 90	LTR LTR	0.54	28.9 24.8	C	80 90		LTR LTR	0.59	43.8 41.9	D D	140 134	Н
26	Northbound	TR	1.34	194.0	F	889	TR	1.64	322.2	F	1058	+	TR	1.12	92.4	F	661	
	Southbound	LT Inters	7.14 ection	2797.4 1048.1	F F	906	LT Inters	9.60 ection	3902.7 1588.3	F F	1149	+	LT Inters	3.78	1277.9 520.0	F	849	Н
-		1111015	COUCH	1040. l			1111615	COLIOTI	1000.3		<u> </u>		111615	JULIUIT	J2U.U	Г		ш

Table 21-8: Signalized Level of Service Analysis – Weekday PM Peak Hour No-Action vs. With-Action vs. Mitigated Conditions (con't)

v ILI	1-Action vs	. 171111		tion Cond		טן פווע	on tj	With-Ac	tion Cond	ditions			With-A	ction Wit	h Mitigati	on Con	ditions	Τ
Int #	Intersection & Approach	Lane Group	v/c Ratio	Delay (sec)	LOS	Queue Length (ft)	Lane Group	v/c Ratio	Delay (sec)	LOS	Queue Length (ft)		Lane Group	v/c Ratio	Delay (sec)	LOS	Queue Length (ft)	
	Van Duzer Street a																	
	Eastbound	LT	0.77	49.3	D	286	LT	0.97	80.1	F	394	+	LT	0.82	50.1	D	344	┺
27	Westbound	TR	0.46	33.0	C	195	TR	0.47	33.4	C	202		TR	0.42	28.8	C	188	┺
	Northbound	L TR	0.42	17.1	В	208	L TR	0.43	17.2	В	211		L TR	0.46	20.7	С	233	+
		Inters	0.58	20.9	C	316		0.59 ection	21.3 35.6	C D	326			0.64 ection	25.8 30.5	C	361	╂
	Bay Street and Wat		COLIOIT	21.5	U		Inters	COLIOIT	55.0	D			IIICIO	COLIOIT	50.5	U	-	十
	Westbound	LTR	0.28	79.6	Е	109	LTR	0.28	74.9	Е	109		LTR	0.28	49.5	D	109	1
28	Northbound	L	3.00	921.0	F	177	L	3.11	971.4	F	139	+	L	3.11	970.3	F	129	T
20		T	1.01	74.3	Е	737	T	1.25	143.6	F	761	+	T	1.25	135.5	F	762	Ė
	Southbound	TR	1.31	174.3	F	1338	TR	1.55	277.2	F	1611	+	TR	1.55	275.1	F	1705	Ŀ
		Inters	ection	176.8	F		Inters	ection	253.2	F			Inters	ection	248.0	F		┸
	Bay Street and Car	al Street	0.00	00.7	F	000		0.00	70.0	-	000			0.00	00.0	F	000	╄
	Eastbound	TR	0.89	82.7 33.8	C	268 91	L TR	0.88	79.9 33.8	E C	263 91		L TR	0.88	80.9 35.3	D D	263 121	╆
29	Westbound	LTR	0.25	40.6	D	66	LTR	0.25	43.5	D	76		LTR	0.34	38.3	D	85	╆
	Northbound	TR	1.13	84.1	F	140	TR	1.43	217.2	F	153	+	TR	1.43	214.8	F	99	t
	Southbound	LT	3.86	1303.9	F	1227	LT	4.64	1652.0	F	1266	+	T	1.50	250.3	F	296	1
		Inters		627.9	F		Inters	ection	841.9	F			Inters	ection	213.4	F		T
	Front Street and Ca																	Ι
	Eastbound	LR	0.59	18.6	В	65	LR	0.70	21.2	С	71		LR	0.60	31.8	С	173	L
30	Northbound	LT	0.76	19.7	В	303	LT	0.88	28.9	С	414		LT	0.85	30.6	С	555	┸
	Southbound	TR	0.46	10.9	В	36	TR	0.61	11.9	В	36		TR	0.59	13.5	В	60	╄
	Day Ctreat and Dre	Inters	ection	16.5	В		Inters	ection	21.4	С			Inters	ection	24.4	С		+
	Bay Street and Bro	LR	0.29	37.5	D	150	LR	0.42	114.0	F	210							٠
	Eastbound	LK	0.29	37.5	D	150	LK	0.42	114.0	F	210	+	_	0.44	43.8	D	192	╄
													R	0.14	40.2	D	58	
31	Northbound	LT	3.39	1091.2	F	763	LT	5.12	1867.4	F	827	+	LT	4.59	1632.7	F	835	t
	Southbound	T	1.07	62.0	E	45	T	1.25	133.8	F	46	+	T	1.15	87.7	F	213	t
		R	0.17	0.8	Α	0	R	0.24	1.0	Α	0		R	0.22	3.5	Α	8	Τ
		Inters		483.8	F		Inters	ection	845.5	F			Inters	ection	722.4	F		Ι
	Richmond Terrace	and Clove																L
	Eastbound	LT	0.74	17.1	В	647	LT	0.83	22.8	С	778		LT	0.83	22.8	С	778	┺
20	\\/ = = + b = = -l	R I	0.17 0.43	3.1	A	27	R	0.17	3.6	A	32		R	0.17 0.64	3.6	A	32	╄
32	Westbound	TR	0.43	14.3 19.3	B B	85 708	TR	0.64 0.81	29.1 22.6	CC	157 791		TR	0.64	29.1 22.6	OO	157 791	╀
	Northbound	LTR	0.75	36.2	D	157	LTR	0.36	36.5	D	165		LTR	0.36	36.5	D	165	╁
	Hortibound	Inters		18.3	В	101		ection	22.8	C	100			ection	22.8	C	100	t
	Victory Boulevard			10.0					EE.O	Ŭ					EE.O	Ü		t
	Eastbound	L	0.99	150.8	F	129	L	1.13	197.4	F	137	+	L	1.13	197.4	F	137	1
		TR	0.72	54.2	D	252	TR	0.72	54.2	D	252		TR	0.72	54.2	D	252	Ι
	Westbound	L	0.70	68.4	Е	160	L	0.73	72.2	Е	170		L	0.73	72.2	Е	170	
35		TR	0.93	76.6	Е	407	TR	0.98	87.0	F	434	+	TR	0.98	87.0	F	434	ł
	Northbound	LTR	0.91	40.8	D	851	LTR	1.34	191.0	F	1180	+	LTR	1.34	191.2	F	1180	╀
	Southbound	LT	1.05	47.0	D	1036	LT	1.22	113.6	F	1089	+	LT	1.22	113.6	F	1089	Ļ
		R Inters	0.04	3.7 52.8	A D	4	R	0.04 ection	3.6 127.5	A F	4	<del>     </del>	R Inters	0.04	3.6 127.5	A F	4	╁
	Victory Boulevard			JZ.0	U		1111015	COLIOIT	121.3				1111015	COMOTI	121.3			t
	Eastbound	L	0.94	66.3	Е	63	L	2.74	807.5	F	125	+	L	2.74	807.5	F	125	t
	200,000110	Ť	0.90	27.6	C	445	T	0.96	27.9	С	299		Ť	0.96	27.8	С	299	t
36	Westbound	Т	0.91	79.3	Ē	986	Т	1.04	93.0	F	1208	+	Т	1.04	92.7	F	1208	Ι
		R	0.10	7.4	Α	40	R	0.18	8.2	Α	68		R	0.18	8.3	Α	68	Ι
	Southbound	LR	0.53	43.3	D	176	LR	0.87	70.5	Е	284	+	LR	0.87	70.5	E	284	I
		Inters		54.6	D		Inters	ection	103.2	F			Inters	ection	103.1	F		Ţ
	Victory Boulevard			46.0	_	40.		0 ==	46.1	_	40=			0	44.0	_	40-	Ļ
	Eastbound	LR I	0.51	42.2	D	181	LR I	0.55	43.1	D F	195	<b>.</b>	LR I	0.57	44.3	ΔШ	197	+
38	Northbound		0.59 0.52	30.4 16.1	В	131 324	T	0.91 0.58	86.4 17.4	В	197 373	+	T T	0.84 0.57	69.7 16.7	B	190 364	╀
		T	0.52	74.1	E	453	T	0.58	79.8	E	664	+	+	0.57	78.1	E	634	t
30	Southhound							0.02			700	T		0.00	, 0.1		UUT	
30	Southbound	R	0.37	7.0	Α	61	R	0.42	8.2	Α	81		R	0.41	7.7	Α	76	т

Table 21-8: Signalized Level of Service Analysis – Weekday PM Peak Hour No-Action vs. With-Action vs. Mitigated Conditions (con't)

			No-Act	ion Cond	itions			With-Ac	tion Cond	ditions			With-A	ction Wit	h Mitigati	on Con	ditions	
nt #	Intersection & Approach	Lane Group	v/c Ratio	Delay (sec)	LOS	Queue Length (ft)	Lane Group	v/c Ratio	Delay (sec)	LOS	Queue Length (ft)		Lane Group	v/c Ratio	Delay (sec)	LOS	Queue Length (ft)	
	Broad Street and C	anal Stree	et															Ι
	Eastbound	L	0.22	8.3	Α	50	L	0.24	12.6	В	76		L	0.24	12.6	В	76	1
		TR	0.22	7.8	Α	70	TR	0.29	12.0	В	137		TR	0.29	12.0	В	137	1
41	Westbound	LTR	0.27	16.7	В	113	LTR	0.37	17.5	В	150		LTR	0.42	19.5	В	172	4
	Northbound	L	0.44	43.1	D	101	L	0.43	42.8	D	101		L	0.43	42.8	D	101	4
		TR	0.61	44.0	D	223	TR	0.65	45.6	D	237		TR	0.65	45.6	D	237	4
	Southbound	LT	0.45	38.4	D	177	LT	0.44	38.3	D	175		LT	0.44	38.3	D C	175	4
	Broad Ctroot and V	Interse		27.4	С		Inters	ection	27.5	С			Interse	ection	27.9	С		4
	Broad Street and V Westbound	an Duzer	0.75	77.9	Е	175	_	0.80	66.9	Е	179			0.80	67.1	Е	180	4
42	Southbound	-	0.73	6.0	A	55	-	0.60	7.8	A	64	-	-	0.80	7.8	A	64	4
72	Southbound	T	0.12	8.5	A	284	T	0.13	11.4	В	351		T	0.13	11.4	В	351	4
		Interse		25.0	C	204	Inters		26.7	C	001		Interse		26.8	C	001	1
	Broad Street and T											H						1
	Eastbound	LT	0.22	44.9	D	163	LT	0.23	44.5	D	162	П	LT	0.23	44.5	D	162	1
,	Westbound	TR	0.39	28.7	C	192	TR	0.50	35.1	D	270		TR	0.50	37.5	D	273	1
13	Northbound	LT	0.65	22.8	С	403	LT	0.65	23.1	С	412		LT	0.65	23.1	С	412	٦
		R	0.26	15.0	В	96	R	0.38	17.0	В	144		R	0.38	17.0	В	144	
		Interse	ection	25.3	С		Inters	ection	26.8	С			Interse	ection	27.4	С		
	Vanderbilt Avenue	and Tomp	kins Ave	nue														
	Eastbound	LTR	0.74	31.8	С	433	LTR	0.85	40.0	D	587		LTR	0.85	40.0	D	587	
14	Westbound	LTR	0.74	37.2	D	384	LTR	0.94	50.7	D	488	+	LTR	0.94	50.3	D	499	
	Northbound	LTR	0.99	79.9	Е	485	LTR	1.02	87.8	F	517	+	LTR	1.02	87.8	F	517	
	Southbound	LTR	0.65	39.0	D	337	LTR	0.65	38.8	D	333		LTR	0.65	38.8	D	333	
		Interse		45.9	D		Inters	ection	53.7	D			Interse	ection	53.6	D		_
	Bay Street and Van	derbilt Av			_				44.0	_					10.0	_		4
	Eastbound	L	0.58	39.1	D	236		0.76	41.9	D	295	-	L	0.78	43.8	D	301	4
15	Nanthhaire	R LT	0.21 2.07	30.2 508.0	C F	63 1327	R LT	0.21 3.17	27.4 997.9	C F	54 1667	Ь.	R LT	0.22 2.95	28.3	C	55 1645	4
	Northbound Southbound	T	0.91	9.7	A	110	T	1.00	23.1	C	101	+	T	0.99	901.9 22.6	F C	147	4
	Southbound	R	0.34	2.2	A	10	R	0.45	2.5	A	12		R	0.99	4.2	A	31	4
		Interse		197.5	F	10	Inters		384.6	F	12		Interse		349.2	F	31	4
	Bay Street and Edg			107.0				0011011	004.0					3011011	040.2			٦
	Westbound	LR	0.40	34.1	С	174	LR	0.51	36.2	D	227		LR	0.51	36.2	D	227	٦
17	Northbound	TR	0.56	8.5	Ā	54	TR	0.70	9.7	A	56		TR	0.70	9.7	Ā	56	1
• /	Southbound	T	0.77	12.1	В	178	T	0.84	13.5	В	171		T	0.84	14.0	В	182	1
	Northwestbound	R	0.59	12.9	В	111	R	0.63	18.4	В	160		R	0.63	18.4	В	160	1
		Interse		14.0	В		Inters	ection	16.2	В			Interse	ection	16.3	В		
	Bay Street and Hyla																	_
	Eastbound	LTR	1.09	95.8	F	734	LTR	1.28	169.4	F	899	+	LTR	1.28	169.4	F	899	_
.	Westbound	LTR	0.98	89.2	F	441	LTR	0.99	92.4	F	444	+	LTR	0.99	92.4	F	444	4
18	Northbound	LTR	3.91	1326.7	F	946	LTR	5.13	1869.2	F	981	+	LTR	5.13	1867.8	F	890	4
	Southbound	1	1.08 0.51	85.3	F	964	I	1.23	143.6	F	1166	+	T R	1.23 0.61	143.0	F B	1166	4
		R Interse		15.4 471.8	B F	188	R Inters	0.61	17.6 687.2	B	241	H	Interse		17.4 686.5	F	241	4
_	Bay Street and Sch		BULLUIT	4/1.8		-	mers	BUILDE	001.2			$\vdash$	interse	octioi I	0.000.5			4
	Eastbound	UUI KUAU	1.44	233.4	F	1331		1.69	341.1	F	1621	+		1.61	306.5	F	1594	4
	Lasibullu	TR	0.11	2.0	A	17	TR	0.11	2.0	A	17	H	TR	0.11	1.8	A	16	+
	Westbound	LTR	0.11	13.8	В	7	LTR	0.01	13.8	В	7	$\vdash$	LTR	0.01	12.2	В	7	1
19	Northbound	LTR	0.16	24.7	С	86	LTR	0.17	24.9	С	86	$\vdash$	LTR	0.19	27.1	С	91	1
	Southbound	LTR	0.32	30.3	C	82	LTR	0.50	32.8	C	113	$\Box$	LTR	0.54	15.7	В	95	1
	222	R	1.00	29.6	Č	190	R	1.03	38.9	D	166	$\Box$	R	1.05	43.9	D	418	1
			ection	125.7	F			ection	185.1	F				ection	168.0	F		-

Table 21-9: Signalized Level of Service Analysis – Saturday MD Peak Hour No-Action vs. With-

			No-Act	ion Cond	itions			With-Ac	tion Cond	ditions			With-A	ction Wit	h Mitigati	on Con	ditions
Int #	Intersection & Approach	Lane Group	v/c Ratio	Delay (sec)	LOS	Queue Length (ft)	Lane Group	v/c Ratio	Delay (sec)	LOS	Queue Length (ft)		Lane Group	v/c Ratio	Delay (sec)	LOS	Queue Length (ft)
	Richmond Terrace	and Frank	din Aven	ue													
	Eastbound	TR	0.71	18.4	В	506	TR	0.76	20.6	С	552		TR	0.76	20.6	С	552
1	Westbound	L	0.86	18.0	В	382	LT	1.02	32.3	C	479		LT	1.02	44.6	D	602
	Northbound	LR	0.11	22.8	C	48	LR	0.11	22.9	C	49		LR	0.11	22.9	С	49
		Inters		18.4	В		Inters	ection	26.4	С			Inters	ection	32.4	С	
	Richmond Terrace																
	Eastbound	L	0.58	33.7	С	77	L	0.58	32.9	С	70		L	0.58	32.9	С	70
	10/	TR	0.75	6.9	A	52	TR	0.81	9.5	A	60		TR	0.81	9.5	Α	60
	Westbound	LT	1.10	78.1	E	687	LT	1.19	113.9	F	670	+					
		R	0.03	9.9	Α	6	R	0.03	12.4	В	5		_	0.00	40.0	Г	44
2													L	0.23	13.8	В	14
	Northbound		0.21	27.7	_	40		0.21	27.7		40		TR	1.00	44.4	D	565
	Northbound	L TR	0.21	27.7 27.1	C	49 73	TR	0.21	27.7 27.3	C	49		L TR	0.21	27.7 27.3	C	49 75
	Southbound	I I	0.24	24.1	C	16	I I	0.25	24.1	C	75 16		I I	0.25	24.1	C	16
	Southbound	TR	0.03	30.4	C	139	TR	0.03	30.4	C	139		TR	0.03	30.4	C	139
		Inters	0.11	39.3	D	139	Inters		53.7	D	138		Inters		27.2	C	139
	Richmond Terrace						IIICIO	COLIOIT	55.1	U			IIItoro	COLIOIT	21.2	U	
	Eastbound	TR	0.79	16.2	В	270	TR	0.87	21.2	С	609		TR	0.87	21.2	С	609
3	Westbound	LT	0.74	19.2	В	495	LT	0.89	31.6	Č	613		LT	0.89	41.4	Ď	612
	Northbound	LR	0.21	21.4	С	89	LR	0.22	21.5	С	90		LR	0.22	21.5	С	90
		Inters	ection	17.9	В		Inters	ection	25.8	С			Inters	ection	30.1	С	
	Hamilton Avenue a	nd Richm	ond Terra	ace													
5	Northbound	LT	0.95	31.4	C	376	LT	1.03	53.2	D	425	+	LT	1.00	43.6	D	415
٠ ا	Southbound	TR	0.53	24.8	С	244	TR	0.57	25.2	С	266		TR	0.56	24.6	С	263
		Inters	ection	28.5	С		Inters	ection	40.7	D			Inters	ection	35.1	D	
	Wall Street and Ric	hmond Te	errace														
	Westbound	LTR	0.80	94.2	F	383	LTR	0.80	94.2	F	383		LTR	0.80	94.2	F	383
		L	0.80	93.1	F	304	L	0.80	93.1	F	304		L	0.80	93.1	F	304
7	Northbound	Т	0.50	5.5	Α	133	Т	0.54	6.8	Α	190		T	0.54	6.8	Α	190
		R	0.80	23.9	С	424	R	0.80	24.6	С	424		R	0.80	24.6	С	424
	Southbound	LTR	0.67	60.0	Е	73	LTR	0.75	62.2	Е	171		LTR	0.75	62.4	Е	88
		Inters		49.0	D		Inters	ection	49.5	D			Inters	ection	49.6	D	
	Richmond Terrace	and Ferry			-				10=0	-	222					_	
	Westbound		1.24	195.9	F	206	L	1.24	195.9	F	206		L	1.24	195.9	F	206
8	Newthern	R T	0.44	48.3	D	63	R T	0.44	48.3	D	63		R T	0.44	48.3	D	63
	Northbound	T	0.67	25.0	C	48	÷	0.71	42.6	р	48	_	T	0.71	42.6	D	48
	Southbound	_	0.77	27.3	O D	193			46.0	ם	208	+		0.81	46.1	ם	208
	Richmond Terrace	Inters		37.2			Inters	ection	53.4	D			Inters	ection	53.5	D	
	Westbound	and Ferry	0.64	54.3	D D	111		0.64	54.3	D	111			0.64	54.3	D	111
	Westbourid	R	0.04	15.5	В	23	R	0.13	16.3	В	23		R	0.04	16.3	В	23
		T	1.03	70.9	E	398	T	1.09	77.3	E	440	+	T	1.09	77.3	E	440
	Northhound			10.5		JJ0		1.05	11.0		<del>++</del> 0		R	0.21	2.8	A	6
9	Northbound		0.21	2.5	Α	5	R	0.21	2.8	Α	6						
9	Northbound	R	0.21	2.5 3.2	A	5 3	R R	0.21	2.8 3.5	A A	6			0.29	3.5		3
9			0.29	3.2	Α	3	R R L	0.29	3.5	Α	3		R		3.5	Α	3
9	Northbound Southbound	R R					R					+	R	0.29 1.69 1.31			
9		R R L	0.29 1.71 1.24	3.2 386.7	A F	3 147	R L	0.29 1.69 1.31	3.5 374.4	A F	3 138	+	R L	1.69 1.31	3.5 374.4	A F	3 138
9		R R L TR Inters	0.29 1.71 1.24 ection	3.2 386.7 130.3	A F F	3 147	R L TR	0.29 1.69 1.31	3.5 374.4 158.4	A F F	3 138	+	R L TR	1.69 1.31	3.5 374.4 158.4	A F F	3 138
9	Southbound	R R L TR Inters	0.29 1.71 1.24 ection	3.2 386.7 130.3	A F F	3 147	R L TR	0.29 1.69 1.31	3.5 374.4 158.4	A F F	3 138	+	R L TR	1.69 1.31	3.5 374.4 158.4	A F F	3 138
	Southbound  Bay Street and Slos	R R L TR Intersesson Terra	0.29 1.71 1.24 ection	3.2 386.7 130.3 102.5	A F F	3 147 1108	R L TR Inters	0.29 1.69 1.31 ection	3.5 374.4 158.4 116.8	A F F	3 138 1194	+	R L TR Inters	1.69 1.31 ection	3.5 374.4 158.4 116.8	A F F F	3 138 1194
	Southbound  Bay Street and Slos  Eastbound	R R L TR Inters	0.29 1.71 1.24 ection ace 0.09 0.34 0.81	3.2 386.7 130.3 102.5 23.6 14.3 13.4	A F F C B	3 147 1108 35 25 188	R L TR Inters	0.29 1.69 1.31 ection	3.5 374.4 158.4 116.8 24.3 16.1 14.0	A F F C B	3 138 1194 49 27 198	+	R L TR Interso	1.69 1.31 ection 0.16	3.5 374.4 158.4 116.8	A F F C B	3 138 1194 50
	Southbound  Bay Street and Slos  Eastbound	R R L TR Interso sson Terro LR L T TR	0.29 1.71 1.24 ection ace 0.09 0.34 0.81 1.26	3.2 386.7 130.3 102.5 23.6 14.3 13.4 142.3	A F F C B B	3 147 1108 35 25	R L TR Inters	0.29 1.69 1.31 ection 0.14 0.39 0.84 1.30	3.5 374.4 158.4 116.8 24.3 16.1 14.0	A F F C B B	3 138 1194 49 27	+	R L TR Interse	1.69 1.31 ection 0.16 0.39 0.81 1.24	3.5 374.4 158.4 116.8 26.0 16.3 25.5 135.3	A F F C B C	3 138 1194 50 43
	Southbound  Bay Street and Slos  Eastbound  Northbound  Southbound	R R R L TR Interse sson Terre LR L T TR Interse	0.29 1.71 1.24 ection ace 0.09 0.34 0.81 1.26 ection	3.2 386.7 130.3 102.5 23.6 14.3 13.4 142.3 82.1	A F F C B B F	3 147 1108 35 25 188	R L TR Inters	0.29 1.69 1.31 ection 0.14 0.39 0.84 1.30	3.5 374.4 158.4 116.8 24.3 16.1 14.0	A F F C B	3 138 1194 49 27 198		R L TR Interso	1.69 1.31 ection 0.16 0.39 0.81 1.24	3.5 374.4 158.4 116.8 26.0 16.3 25.5	A F F C B	3 138 1194 50 43 486
	Southbound  Bay Street and Slos Eastbound Northbound Southbound Victory Boulevard a	R R R L TR Interse sson Terre LR L T TR Interse	0.29 1.71 1.24 ection ace 0.09 0.34 0.81 1.26 ection treet/St. I	3.2 386.7 130.3 102.5 23.6 14.3 13.4 142.3 82.1	A F F C B B F	3 147 1108 35 25 188 822	R L TR Inters	0.29 1.69 1.31 ection 0.14 0.39 0.84 1.30 ection	3.5 374.4 158.4 116.8 24.3 16.1 14.0 162.7 92.6	A F F C B B	3 138 1194 49 27 198 865		R L TR Interso	1.69 1.31 ection 0.16 0.39 0.81 1.24 ection	3.5 374.4 158.4 116.8 26.0 16.3 25.5 135.3 83.2	A F F C B C	3 138 1194 50 43 486 842
	Southbound  Bay Street and Slos  Eastbound  Northbound  Southbound	R R R L TR Inters: sson Terr: LR L T TR Inters: and Bay S	0.29 1.71 1.24 ection ace 0.09 0.34 0.81 1.26 ection treet/St. I	3.2 386.7 130.3 102.5 23.6 14.3 13.4 142.3 82.1 Warks Pla	A F F C B B F F C C C B	3 147 1108 35 25 188 822 206	R L TR Inters LR L T T TR Inters	0.29 1.69 1.31 ection 0.14 0.39 0.84 1.30 ection	3.5 374.4 158.4 116.8 24.3 16.1 14.0 162.7 92.6	A F F C B B F	3 138 1194 49 27 198 865		R L TR Inters LR L T T TR Inters	1.69 1.31 ection 0.16 0.39 0.81 1.24 ection	3.5 374.4 158.4 116.8 26.0 16.3 25.5 135.3 83.2	A F F C B C F F	3 138 1194 50 43 486 842
	Southbound  Bay Street and Slos  Eastbound  Northbound  Southbound  Victory Boulevard a  Eastbound	R R R L TR Interse sson Terra LR L T T TR Interse and Bay S R	0.29 1.71 1.24 ection ace 0.09 0.34 0.81 1.26 ection treet/St. I 0.48 0.43	3.2 386.7 130.3 102.5 23.6 14.3 13.4 142.3 82.1 Warks Pla 13.7 12.7	A F F C B B F F C C B B B B	3 147 1108 35 25 188 822 206 151	R L TR Inters LR L T T TR Inters	0.29 1.69 1.31 ection 0.14 0.39 0.84 1.30 ection 0.52 0.50	3.5 374.4 158.4 116.8 24.3 16.1 14.0 162.7 92.6	A F F F B B B	3 138 1194 49 27 198 865 243 185		R L TR Inters LR L T T TR Inters	1.69 1.31 ection 0.16 0.39 0.81 1.24 ection 0.52 0.50	3.5 374.4 158.4 116.8 26.0 16.3 25.5 135.3 83.2	A F F F C C B C F F B B B	3 138 1194 50 43 486 842 244 185
10	Southbound  Bay Street and Slos Eastbound Northbound Southbound Victory Boulevard a	R R R L TR Interse sson Terra LR L T T TR Interse and Bay S T R R T	0.29 1.71 1.24 ection ace 0.09 0.34 0.81 1.26 ection treet/\$t. 0.48 0.43 0.84	3.2 386.7 130.3 102.5 23.6 14.3 13.4 142.3 82.1 <b>Marks Pla</b> 13.7 12.7 74.7	A F F F B B F F Ce B B E	3 147 1108 35 25 188 822 206 151 365	R L TR Inters LR L T T T T T R Inters	0.29 1.69 1.31 ection 0.14 0.39 0.84 1.30 ection 0.52 0.50	3.5 374.4 158.4 116.8 24.3 16.1 14.0 162.7 92.6 16.1 15.2 77.5	A F F F B B B E	3 138 1194 49 27 198 865 243 185 401		R L TR Interso LR L T T T T R Interso	1.69 1.31 ection  0.16 0.39 0.81 1.24 ection  0.52 0.50 0.92	3.5 374.4 158.4 116.8 26.0 16.3 25.5 135.3 83.2 16.1 15.2 63.7	A F F C B C F F	3 138 1194 50 43 486 842 244 185 435
10	Southbound  Bay Street and Slos Eastbound Northbound Southbound Victory Boulevard a Eastbound Westbound	R R R L TR Interse SSON TETRS LR L T TR Interse SSON TETRS TR Interse SSON TR R R T L L T T TR INTERSE SSON TR R R T L L L L T T L L SSON TR R R R R T L L L SSON TR R R R T L L L L L L L L L L L L L L	0.29 1.71 1.24 ection ace 0.09 0.34 0.81 1.26 ection treet/St. I 0.48 0.43 0.84	3.2 386.7 130.3 102.5 23.6 14.3 13.4 142.3 82.1 Warks Pla 13.7 12.7 74.7	A F F F C B B F F C C B B B B B B B B B B	3 147 1108 35 25 188 822 206 151 365 22	R L TR Inters  LR L T T TR Inters	0.29 1.69 1.31 ection 0.14 0.39 0.84 1.30 ection 0.52 0.50 0.92	3.5 374.4 158.4 116.8 24.3 16.1 14.0 162.7 92.6 16.1 15.2 77.5 16.2	A F F F B B B B B B B B B B B B B B B B	3 138 1194 49 27 198 865 243 185 401 19		R L TR Interse LR L T T T T T R Interse	1.69 1.31 ection 0.16 0.39 0.81 1.24 ection 0.52 0.50 0.92	3.5 374.4 158.4 116.8 26.0 16.3 25.5 135.3 83.2 16.1 15.2 63.7 7.4	A F F C B C F F A	3 138 1194 50 43 486 842 244 185 435 8
10	Southbound  Bay Street and Slos  Eastbound  Northbound  Southbound  Victory Boulevard a  Eastbound	R R R L TR Interse sson Terra LR L T T TR Interse and Bay S T R R T	0.29 1.71 1.24 ection ace 0.09 0.34 0.81 1.26 ection treet/\$t. 0.48 0.43 0.84	3.2 386.7 130.3 102.5 23.6 14.3 13.4 142.3 82.1 <b>Marks Pla</b> 13.7 12.7 74.7	A F F F B B F F Ce B B E	3 147 1108 35 25 188 822 206 151 365	R L TR Inters LR L T T T T T R Inters	0.29 1.69 1.31 ection 0.14 0.39 0.84 1.30 ection 0.52 0.50	3.5 374.4 158.4 116.8 24.3 16.1 14.0 162.7 92.6 16.1 15.2 77.5	A F F F B B B E	3 138 1194 49 27 198 865 243 185 401		R L TR Interso LR L T T T T R Interso	1.69 1.31 ection  0.16 0.39 0.81 1.24 ection  0.52 0.50 0.92	3.5 374.4 158.4 116.8 26.0 16.3 25.5 135.3 83.2 16.1 15.2 63.7	A F F C B C F F	3 138 1194 50 43 486 842 244 185 435

Table 21-9: Signalized Level of Service Analysis – Saturday MD Peak Hour No-Action vs. With-Action vs. Mitigated Conditions (con't)

	on vs. Mitig	,		ion Cond				With-Ac	tion Con	ditions			With-A	ction Wit	th Mitigati	on Con	ditions
Int#	Intersection & Approach	Lane Group	v/c Ratio	Delay (sec)	LOS	Queue Length (ft)	Lane Group	v/c Ratio	Delay (sec)	LOS	Queue Length (ft)		Lane Group	v/c Ratio	Delay (sec)	LOS	Queue Length (ft)
	Victory Boulevard	and Bay S															
	Eastbound	L LT	0.62	18.2 18.9	B B	54 55	L LT	0.81	34.5 30.6	C	250 248		L LT	0.75 0.73	41.8 40.0	D D	260 258
	Westbound	LTR	0.63	24.2	С	72	LTR	0.79	49.2	D	194	+	LTR	0.73	37.3	D	171
12	Northbound	L	3.55	1171.5	F	247	L	4.38	1549.4	F	254	+	L	1.77	377.0	F	261
		TR	0.74	24.2	С	185	TR	0.76	23.8	С	171		TR	0.80	22.9	С	383
	Southbound	LT	0.93	43.6	D	315	LT	1.06	72.4	E	322	+	LT	1.47	231.9	F	401
		R Interse	0.57	13.6 119.1	B F	68	R Inters	0.65	23.1 163.9	C F	103		R Inters	0.77	11.6 123.2	B F	3
_	Bay Street and Har			119.1			inters	ection	103.9				inters	ection	123.2		
	Eastbound	LTR	0.04	17.4	В	26	LTR	0.04	17.4	В	26		LTR	0.04	18.7	В	27
	Westbound	LTR	0.60	10.3	В	52	LTR	0.76	14.9	В	90		LTR	0.81	25.2	С	370
	Northbound	LTR	1.43	217.9	F	666	LTR	1.59	290.2	F	719	+	L	0.55	28.4	С	32
13													TR	0.55	58.7	E	476
	Southbound	L	3.30	1064.7	F	410	L	4.86	1760.5	F	461	+	L	2.12	529.8	F	296
		T	0.72	11.2	В	141	T	0.77	13.6	В	153		T	0.96	29.9	С	334
		R	0.17	3.1	A	0	R	0.20	3.6	A	4		R	0.26	8.6	A	29
	Front Street and Ha	Interse		194.8	F	<b>-</b>	Inters	ection	306.4	F	<b>-</b>		inters	ection	93.2	F	
	Eastbound	TR	0.38	10.5	В	0	TR	0.43	10.4	В	0		TR	0.43	12.0	В	6
14	Westbound	LT	0.05	12.9	В	30	LT	0.05	12.9	В	30		LT	0.05	12.9	В	30
	Northbound	LR	0.52	23.1	С	242	LR	0.74	32.0	С	326		LR	0.74	32.0	С	326
	Bay Street and Swa	Interse		16.5	В	l	Inters	ection	20.6	С	l		Inters	ection	21.4	С	
	Eastbound	in Street/\	0.66	33.6	С	178	L	0.71	36.6	D	188		L	0.71	37.8	D	188
	Lasibouria	LTR	0.17	19.9	В	66	LTR	0.19	20.2	C	69		LTR	0.19	20.2	C	69
15	Westbound	LTR	0.00	0.0	0.0	0	LTR	0.00	0.0	0.0	0		LTR	0.00	0.0	0.0	0
	Northbound	LTR	0.68	62.1	Е	273	LTR	0.73	63.1	Е	336		LTR	0.73	26.3	С	345
	Southbound	LTR Interse	0.90	21.4	С	480	LTR Inters	0.96	26.9 41.4	С	528		LTR	0.96 ection	27.7	C	85
	Bay Street and Gra		SCHOIL	37.8	D	!	IIILEIS	ection	41.4	D	!		IIILEIS	ection	27.9	С	
	Eastbound	nt otroct											LTR	0.24	29.8	С	74
18	Westbound												R	0.21	29.1	С	64
	Northbound		Ur	nsignalize	d			Un	signalize	d			TR	0.46	10.8	В	195
	Southbound												T	1.47 ection	233.0 134.1	F	1233
	Van Duzer Street a	nd Clinton	Street										inters	ection	134.1		
19	Westbound	TR	0.27	33.1	С	53	TR	0.29	33.5	С	56		TR	0.29	32.9	С	60
19	Northbound	LT	0.33	7.1	Α	95	LT	0.34	7.2	Α	98		LT	0.34	7.2	Α	98
	Bay Street and Clin	Interse		12.6	В		Inters	ection	13.0	В			Inters	ection	12.9	В	
	Westbound	LTR	0.30	23.6	С	100	LTR	0.31	23.9	С	101		LTR	0.37	29.3	С	109
	Northbound	L	0.34	19.0	В	10	L	0.38	19.6	В	10		L	0.39	18.9	В	9
20		TR	0.63	17.4	В	147	TR	0.69	18.2	В	144		TR	0.64	13.5	В	156
	Southbound	L	0.54	14.2	В	25	L	0.65	21.4	C	32		L	0.55	8.0	A	9
		TR Interse	1.45	222.8 118.3	F	1228	TR Inters	1.56 ection	273.7 143.6	F	1256	+	TR	1.44 ection	218.2 114.4	F F	610
	Bay Street and Bal		otion	110.5			Inters	COLIOIT	145.0				IIICIO	COLIOTI	117.7	-	
	Eastbound												LTR	0.21	38.7	D	35
21	Westbound												LTR	0.05	33.8	С	13
			Ur	nsignalize	d			Un	signalize	d			TR LT	0.85 1.18	7.9 96.4	A F	133 39
ì	Northbound												LI			E	39
	Southbound												Inters	ection	56.2		
													Inters	ection	56.2	E	
	Southbound		0.34	26.2	С	87	LTR	0.34	25.9	С	87		Inters				
	Southbound  Bay Street and Way			26.2	С	87	LTR	0.34	25.9	С	87		L	0.28	36.6	D	39
24	Southbound  Bay Street and Wa  Westbound	LTR	0.34										L TR	0.28 0.45	36.6 42.0	D D	67
24	Southbound  Bay Street and Way			26.2 141.6 12.9	C F B	87 820 22	LTR LT R	0.34 1.41 0.10	25.9 214.7 12.7	C F B	949 23	+	L	0.28	36.6	D	
24	Southbound  Bay Street and Wa  Westbound	LTR LT R L	0.34 1.24 0.10 0.81	141.6 12.9 38.7	F B D	820 22 16	LT R L	1.41	214.7 12.7 37.6	F B D	949 23 15	+	L TR LT R L	0.28 0.45 1.10 0.08 0.67	36.6 42.0 75.8 5.7 20.9	D D E A	67 857 14 11
24	Southbound  Bay Street and Wa  Westbound  Northbound	LTR LT R L TR	0.34 1.24 0.10 0.81 1.54	141.6 12.9 38.7 268.3	F B D	820 22	LT R L TR	1.41 0.10 0.79 1.67	214.7 12.7 37.6 323.9	F B D	949 23	+	L TR LT R L	0.28 0.45 1.10 0.08 0.67 1.34	36.6 42.0 75.8 5.7 20.9	D D E A C	67 857 14
24	Southbound  Bay Street and War  Westbound  Northbound  Southbound	LTR LT R L TR Interse	0.34 1.24 0.10 0.81 1.54 ection	141.6 12.9 38.7	F B D	820 22 16	LT R L TR	1.41 0.10 0.79	214.7 12.7 37.6	F B D	949 23 15		L TR LT R L	0.28 0.45 1.10 0.08 0.67	36.6 42.0 75.8 5.7 20.9	D D E A	67 857 14 11
24	Southbound  Bay Street and Way  Westbound  Northbound  Southbound  Front Street and W	LTR LT R L TR Interse	0.34 1.24 0.10 0.81 1.54 ection	141.6 12.9 38.7 268.3 201.4	F B D F	820 22 16 707	LT R L TR Inters	1.41 0.10 0.79 1.67 ection	214.7 12.7 37.6 323.9 259.9	F B D F	949 23 15 722		L TR LT R L TR	0.28 0.45 1.10 0.08 0.67 1.34 ection	36.6 42.0 75.8 5.7 20.9 171.8 123.6	D D E A C F	67 857 14 11 874
	Southbound  Bay Street and Wa Westbound  Northbound  Southbound  Front Street and W Eastbound	LTR  LT  R  L  TR  Interse	0.34 1.24 0.10 0.81 1.54 ection	141.6 12.9 38.7 268.3 201.4	F B D F F	820 22 16 707	LT R L TR Inters	1.41 0.10 0.79 1.67 ection	214.7 12.7 37.6 323.9 259.9	F B D F F	949 23 15 722		L TR LT R L	0.28 0.45 1.10 0.08 0.67 1.34 ection	36.6 42.0 75.8 5.7 20.9 171.8 123.6	D D E A C F F	67 857 14 11 874
	Southbound  Bay Street and Way  Westbound  Northbound  Southbound  Front Street and W	LTR LT R L TR Interse	0.34 1.24 0.10 0.81 1.54 ection	141.6 12.9 38.7 268.3 201.4	F B D F	820 22 16 707	LT R L TR Inters	1.41 0.10 0.79 1.67 ection	214.7 12.7 37.6 323.9 259.9	F B D F	949 23 15 722		L TR LT R L TR Interse	0.28 0.45 1.10 0.08 0.67 1.34 ection	36.6 42.0 75.8 5.7 20.9 171.8 123.6	D D E A C F	67 857 14 11 874
	Southbound  Bay Street and Wa Westbound  Northbound  Southbound  Front Street and W Eastbound Northbound Southbound	LTR  LT  R  L  TR  Interse  ave Street  LR  LT  TR  Interse	0.34 1.24 0.10 0.81 1.54 ection 0.25 0.74 0.39 ection	141.6 12.9 38.7 268.3 201.4 17.9 8.5	F B D F F	820 22 16 707 43 29	LT R L TR Inters LR LT	1.41 0.10 0.79 1.67 ection 0.27 0.87 0.48	214.7 12.7 37.6 323.9 259.9	F B D F F	949 23 15 722 44 24		L TR LT R L TR Inters	0.28 0.45 1.10 0.08 0.67 1.34 ection 0.30 0.75 0.41	36.6 42.0 75.8 5.7 20.9 171.8 123.6	D D E A C C F F	67 857 14 11 874 62 65
	Southbound  Bay Street and Wa Westbound  Northbound  Southbound  Front Street and W Eastbound Northbound Southbound Front Street and W	LTR  LT  R  L  TR  Interse ave Street  LR  LT  TR  Interse cospect St	0.34  1.24 0.10 0.81 1.54 ection  0.25 0.74 0.39 ection reet	141.6 12.9 38.7 268.3 201.4 17.9 8.5 10.4 10.0	F B D F F F B A B	820 22 16 707 43 29 125	LT R L TR Inters LR LT TR LIT TR Inters	1.41 0.10 0.79 1.67 ection 0.27 0.87 0.48 ection	214.7 12.7 37.6 323.9 259.9 18.4 11.4 11.5 11.9	F B D F F B B	949 23 15 722 44 24 156		L TR LT R L TR Interse	0.28 0.45 1.10 0.08 0.67 1.34 ection 0.30 0.75 0.41 ection	36.6 42.0 75.8 5.7 20.9 171.8 123.6 26.0 9.9 11.0	D D E A C F F C A B B	67 857 14 11 874 62 65 183
25	Southbound  Bay Street and Wa Westbound  Northbound  Southbound  Front Street and W Eastbound  Northbound  Southbound  Front Street and P Eastbound	LTR  LT R L TR Interso ave Street LR LT TR Interso ospect St LTR	0.34  1.24 0.10 0.81 1.54 ection  0.25 0.74 0.39 ection reet 0.62	141.6 12.9 38.7 268.3 201.4 17.9 8.5 10.4 10.0	F B D F F A B B	820 22 16 707 43 29 125	LT R L TR Inters LR LT TR Inters LT TR LT TR LT	1.41 0.10 0.79 1.67 ection 0.27 0.87 0.48 ection	214.7 12.7 37.6 323.9 259.9 18.4 11.4 11.5 11.9	F B D F F B B B	949 23 15 722 44 24 156		L TR LT R L TR L TR Interse	0.28 0.45 1.10 0.08 0.67 1.34 ection 0.30 0.75 0.41 ection	36.6 42.0 75.8 5.7 20.9 171.8 123.6 26.0 9.9 11.0 11.4	D D E A C C F F C A B B B	67 857 14 11 874 62 65 183
25	Southbound  Bay Street and Wa Westbound  Northbound  Southbound  Front Street and W Eastbound Northbound Southbound Front Street and P Eastbound Westbound	LTR  LT R L TR Intersor ave Street LR LT TR LIT TR LIT LT TR LTR LTR	0.34  1.24 0.10 0.81 1.54 ection  0.25 0.74 0.39 ection reet 0.62 0.53	141.6 12.9 38.7 268.3 201.4 17.9 8.5 10.4 10.0	F B D F F F B A B	820 22 16 707 43 29 125	LT R L TR Inters LR LT TR Inters LT TR LT TR Inters	1.41 0.10 0.79 1.67 ection 0.27 0.87 0.48 ection	214.7 12.7 37.6 323.9 259.9 18.4 11.4 11.5 11.9	F B D F F B B	949 23 15 722 44 24 156	+	L TR LT R LT TR Interse LR LT TR Interse LT TR LTT TR LTT TR LTT TR LTT LTT LTT	0.28 0.45 1.10 0.08 0.67 1.34 ection 0.30 0.75 0.41 ection 0.61 0.59	36.6 42.0 75.8 5.7 20.9 171.8 123.6 26.0 9.9 11.0 11.4	D D E A C F F D D D D D D D D D	67 857 14 11 874 62 65 183
24 25 26	Southbound  Bay Street and Wa Westbound  Northbound  Southbound  Front Street and W Eastbound  Northbound  Southbound  Front Street and P Eastbound	LTR  LT R L TR Interso ave Street LR LT TR Interso ospect St LTR	0.34  1.24 0.10 0.81 1.54 ection  0.25 0.74 0.39 ection reet 0.62	141.6 12.9 38.7 268.3 201.4 17.9 8.5 10.4 10.0	F B D F F B A B B C C C	820 22 16 707 43 29 125	LT R L TR Inters LR LT TR Inters LT TR LT TR LT	1.41 0.10 0.79 1.67 ection 0.27 0.87 0.48 ection	214.7 12.7 37.6 323.9 259.9 18.4 11.4 11.5 11.9	F B B B B C C	949 23 15 722 44 24 156		L TR LT R L TR L TR Interse	0.28 0.45 1.10 0.08 0.67 1.34 ection 0.30 0.75 0.41 ection	36.6 42.0 75.8 5.7 20.9 171.8 123.6 26.0 9.9 11.0 11.4	D D E A C C F F C A B B B	67 857 14 11 874 62 65 183

Table 21-9: Signalized Level of Service Analysis – Saturday MD Peak Hour No-Action vs. With-Action vs. Mitigated Conditions (con't)

			No-Act	ion Cond	itions			With-Ac	tion Cond	ditions			With-A	ction Wit	h Mitigati	on Con	ditions
nt#	Intersection & Approach	Lane Group	v/c Ratio	Delay (sec)	LOS	Queue Length (ft)	Lane Group	v/c Ratio	Delay (sec)	LOS	Queue Length (ft)		Lane Group	v/c Ratio	Delay (sec)	LOS	Queue Length (ft)
	Van Duzer Street a																
	Eastbound	LT	0.65	33.9	С	212	LT	0.71	37.2	D	252		LT	0.71	37.2	D	252
27	Westbound	TR	0.31	23.9	С	99	TR	0.33	24.1	С	103		TR	0.33	24.1	С	103
	Northbound	L	0.29	12.1	В	121	L	0.29	12.2	В	124		L	0.29	12.2	В	124
		TR	0.44	14.3	В	184	TR	0.45	14.5	В	190		TR	0.45	14.5	В	190
	D 0 ( ( 1 W -	Inters	ection	20.1	С	l .	Inters	ection	21.3	С			Inters	ection	21.3	С	
	Bay Street and Wat		0.04	27.3	_	0.4	LTD	0.04	07.0	_	0.4		LTD	0.44	247	_	00
	Westbound Northbound	LTR L	0.31 1.74	359.2	C F	84 107	LTR I	0.31 1.80	27.3 383.0	C F	93	+	LTR	0.41 1.75	34.7 362.6	C F	93 102
28	Northbourid	÷	1.74	61.3	E	200	+	1.20	107.5	F	190	+	+	1.73	63.4	E	309
	Southbound	TR	1.46	240.6	F	1067	TR	1.57	290.6	F	1182	+	TR	1.06	211.8	F	1219
	Southbound	Inters		169.3	F	1007	Inters		212.9	F	1102	-	Inters		153.6	F	1219
	Bay Street and Can		COLIOIT	103.5			IIItoro	Journ	212.0				IIItoro	COLIOIT	155.0		
	Eastbound	L	0.62	145.5	F	163	L	0.62	145.2	F	161		L	0.93	144.8	F	231
	200,000110	TR	0.25	20.8	C	85	TR	0.25	20.7	Ċ	84		TR	0.40	30.3	Ċ	120
29	Westbound	LTR	0.20	134.0	F	52	LTR	0.25	134.8	F	64		LTR	0.38	86.2	F	88
	Northbound	TR	1.17	97.7	F	77	TR	1.35	179.2	F	86	+	TR	1.12	72.3	E	83
	Southbound	LT	3.56	1167.3	F	664	LT	3.88	1309.0	F	677	+	Т	1.32	162.6	F	609
		Inters	ection	606.5	F		Inters	ection	697.8	F			Inters	ection	116.9	F	
	Front Street and Ca	anal Stree															
	Eastbound	LR	0.65	30.2	С	110	LR	0.73	35.1	D	141		LR	0.56	29.5	С	123
30	Northbound	LT	0.53	12.8	В	165	LT	0.61	14.4	В	200		LT	0.63	21.1	С	300
	Southbound	TR	0.44	10.4	В	63	TR	0.52	11.1	В	55		TR	0.54	14.8	В	109
		Inters	ection	15.3	В		Inters	ection	17.1	В			Inters	ection	20.2	С	
	Bay Street and Bro				_				0= 4	_	150						
	Eastbound	LR	0.30	25.2	С	127	LR	0.38	25.1	С	156			0.44	00.0		454
										_			R	0.44	33.2 29.7	C	151 56
31	Northbound	LT	3.24	1024.5	F	244	LT	3.94	1339.0	F	189	+	LT	0.19 3.17	995.2	F	140
	Southbound	T	1.35	180.6	F	108	T	1.46	229.5	F	111		T	1.24	128.4	F	246
	Codtribodria	R	0.20	6.3	A	0	R	0.24	6.6	A	0		R	0.21	3.4	A	8
		Inters		482.3	F	Ŭ	Inters		627.8	F				ection	447.8	F	
	Richmond Terrace	and Clove	Road			•											
	Eastbound	LT	0.76	19.4	В	333	LT	0.81	21.9	С	366		LT	0.81	21.9	С	366
		R	0.13	6.8	Α	38	R	0.13	7.0	Α	39		R	0.13	7.0	Α	39
32	Westbound	L	0.47	15.6	В	37	L	0.60	25.3	С	120		L	0.60	25.3	С	120
		TR	0.69	12.3	В	177	TR	0.73	13.8	В	198		TR	0.73	13.8	В	198
	Northbound	LTR	0.27	22.7	С	31	LTR	0.28	22.9	С	32		LTR	0.28	22.9	С	32
		Inters		16.0	В		Inters	ection	18.2	В			Inters	ection	18.2	В	
	Victory Boulevard	and Cebra															
	Eastbound	L	0.27	29.4	С	47	L	0.28	29.9	С	48	<b>—</b>	L	0.34	35.4	D	51
	Mooths:::=d	TR L	0.50	31.2	C	153	TR L	0.50	31.2	C	153		TR L	0.57	35.7	ם ם	161
35	Westbound	TR	0.32	29.5 32.1	C	68 176	TR	0.35	30.2	C	73 185		TR	0.42	35.2 38.6	D	78 195
	Northbound	LTR	0.92	37.7	D	663	LTR	0.56	50.5	D	739	+	LTR	0.88	36.5	D	705
	Southbound	LTR	1.07	65.3	E	561	LTR	1.17	103.8	F	601	+	LTR	1.09	67.5	E	565
	Souribound	Inters		46.3	D	- 551	Inters		65.7	Ė				ection	48.3	D	
	Victory Boulevard					•											
	Eastbound	L	0.74	36.0	D	40	L	1.05	91.7	F	91	+	L	1.05	96.8	F	98
		Т	1.00	42.9	D	509	Т	1.06	58.0	Е	502	+	T	1.06	59.9	Е	556
6	Westbound	Т	1.00	50.2	D	664	Т	1.05	64.2	E	712	+	T	1.05	64.2	E	712
		R	0.12	6.4	Α	24	R	0.21	7.1	Α	35		R	0.21	7.1	Α	35
	Southbound	LR	0.38	25.4	С	112	LR	0.59	31.6	С	156		LR	0.59	31.6	С	156
		Inters		42.6	D		Inters	ection	57.1	E			Inters	ection	58.1	Е	
	Victory Boulevard																
	Eastbound	LR	0.57	29.4	С	162	LR	0.59	29.9	С	169		LR	0.64	32.5	С	175
20	Northbound	L	0.92	67.8	E	238	L	1.03	100.8	F	253	+	L	0.90	63.9	E	236
38	0. (1.1	T	0.63	19.8	В	326	T	0.67	21.1	C	360		T	0.64	18.9	В	341
	Southbound	Т	0.78	64.8	Е	448		0.82	78.7	Е	541	+	Т	0.79	67.7	Е	465
		R	0.33	3.0	Α	37	R	0.34	3.1	Α	38		R	0.33	2.9	Α	36

Table 21-<u>9</u>: Signalized Level of Service Analysis – Saturday MD Peak Hour No-Action vs. With-Action vs. Mitigated Conditions (con't)

	on vs. Mitig I			ion Cond				With Ac	tion Cond	litions			With A	ction Wit	h Mitigati	on Con	ditions
					itions	Queue				illions	Queue					on con	Queue
nt #	Intersection & Approach	Lane Group	v/c Ratio	Delay (sec)	LOS	Length (ft)	Lane Group	v/c Ratio	Delay (sec)	LOS	Length (ft)		Lane Group	v/c Ratio	Delay (sec)	LOS	Length (ft)
	Broad Street and C	anal Stree															
	Eastbound	L	0.27	9.5	A	65	L	0.28	9.7	A	64		L	0.28	9.7	A	64
	107	TR	0.25	8.6	A	70	TR	0.29	9.2	A	89		TR	0.29	9.2	A	89
41	Westbound	LTR	0.28	13.4	В	120	LTR	0.33	14.2	B C	143	-	LTR	0.37	12.7	В	138
	Northbound	L TR	0.28	25.8 26.9	CC	68 158	L TR	0.28	25.8 27.0	C	68		L TR	0.28	25.8	C	68
	Southbound	LT	0.41	26.9	C	113	LT	0.42	24.9	C	160 117	$\vdash$	IT	0.42	27.0 24.9	C	160 117
	Southbound	Interse		17.8	В	113	Inters		17.7	В	117	$\vdash$	Interse		17.4	В	117
	Broad Street and V			17.0	Ь		inters	ection	17.7	В			IIICISC	BOLIOIT	17.4	Ь	
	Westbound	an Duzer	0.66	68.3	Е	173		0.70	66.6	Е	178			0.70	66.7	Е	177
12	Southbound	Ŀ	0.11	5.1	Ā	45	- i	0.11	5.9	A	49		i i	0.11	5.9	A	49
-	Coulibouria	Ť	0.34	6.5	A	144	Ť	0.36	7.5	A	161		Ť	0.36	7.5	A	161
		Interse		22.4	C		Inters		24.5	C			Interse		24.5	C	
	Broad Street and T				_												
	Eastbound	LT	0.22	30.9	С	119	LT	0.22	30.2	С	120		LT	0.22	30.2	С	120
42	Westbound	TR	0.37	23.3	С	137	TR	0.43	24.6	С	163		TR	0.43	24.2	С	163
43	Northbound	LT	0.58	16.8	В	265	LT	0.58	17.0	В	270		LT	0.58	17.0	В	270
		R	0.27	12.0	В	89	R	0.33	12.8	В	111		R	0.33	12.8	В	111
		Interse	ection	19.0	В		Inters	ection	19.3	В			Interse	ection	19.2	В	
	Vanderbilt Avenue	and Tomp	kins Ave	nue													
	Eastbound	LTR	0.81	32.3	С	445	LTR	0.88	38.4	D	501		LTR	0.88	38.4	D	501
4	Westbound	LTR	0.53	4.4	Α	33	LTR	0.60	4.5	Α	35		LTR	0.60	8.3	Α	58
-	Northbound	LTR	0.83	44.8	D	273	LTR	0.87	48.4	D	305		LTR	0.87	48.4	D	305
	Southbound	LTR	0.61	29.6	С	248	LTR	0.61	29.7	С	248		LTR	0.61	29.7	С	248
		Interse		27.9	С		Inters	ection	30.4	С			Interse	ection	31.3	С	
	Bay Street and Van																
	Eastbound	L	0.38	28.7	C	124	L	0.47	30.3	С	149		L	0.52	33.3	С	155
45	Ni. at Land	R	0.20	26.6	С	51	R	0.20	26.6	C	48		R	0.22	29.0	C	50
io	Northbound	LT T	8.16	3246.2	F	1218	LT T	8.95	3598.7	F	1302	+	LT T	7.95	3147.0	F	1272
	Southbound	R	1.28 0.35	145.4	A	483 9	R	1.36 0.40	180.4 1.7	A	475 10	+	R	1.28 0.38	139.9 1.4	A	569 10
		Interse		1.5 1195.9	F	9	Inters		1322.7	F	10		Interse		1150.4	F	10
	Bay Street and Edg			1195.9	F		IIILEIS	ection	1322.7	F		$\vdash$	IIILEIS	ECLIOIT	1130.4	_ F	
	Westbound	LR	0.30	22.5	С	105	LR	0.35	23.0	С	121		LR	0.37	24.7	С	126
	Northbound	TR	0.60	16.8	В	84	TR	0.68	17.6	В	85		TR	0.65	15.5	В	78
47	Southbound	T	1.01	36.9	D	328	T	1.06	55.5	E	324	+	T	1.02	37.8	D	336
	Northwestbound	R	0.37	3.8	A	25	R	0.39	5.6	A	42	$\vdash$	R	0.40	6.0	A	43
		Interse		24.1	C		Inters		31.5	C			Interse		24.3	C	- 1
	Bay Street and Hyla																•
	Eastbound	LTR	1.06	77.9	Е	551	LTR	1.15	110.3	F	614	+	LTR	1.15	110.3	F	614
	Westbound	LTR	0.65	41.9	D	185	LTR	0.66	42.4	D	187		LTR	0.66	42.4	D	187
48	Northbound	LTR	4.39	1540.4	F	709	LTR	5.22	1909.6	F	718	+	LTR	5.22	1909.6	F	814
	Southbound	Т	1.10	90.6	F	529	T	1.20	128.0	F	580	+	Ť	1.20	128.3	F	613
		R	0.63	18.8	В	179	R	0.68	19.5	В	191		R	0.68	19.4	В	203
		Interse	ection	515.8	F		Inters	ection	654.4	F			Interse	ection	654.5	F	
	Bay Street and Sch																
	Eastbound	L	1.39	210.7	F	831	L	1.54	277.4	F	943	+	L	1.36	197.3	F	898
		TR	0.09	8.3	Α	28	TR	0.09	8.3	Α	28	Ш	TR	0.08	6.8	Α	25
19	Westbound	LTR	0.01	15.3	В	9	LTR	0.01	15.3	В	9		LTR	0.01	12.5	В	8
-	Northbound	LTR	0.10	13.9	В	46	LTR	0.10	13.9	В	46	Ш	LTR	0.11	16.9	В	51
	Southbound	LTR	0.19	19.9	В	65	LTR	0.20	20.3	С	63	Щ	LTR	0.23	21.0	C	65
		R	0.70	11.3	В	153	R	0.73	12.1 130.1	В	137	Щ	R	0.74	12.1	В	137
	-	Interse	ะแบบ	98.3	F	•	Inters			F				ection	94.8	F	

Table 21-<u>10</u>: Unsignalized Level of Service Analysis – Weekday AM Peak Hour No-Action vs. With-Action vs. Mitigated Conditions

			No-Acti	on Condition	ons			With-Act	ion Condit	ions			With	h-Action Wit	h Mitigatio	n Condit	ions	
#	Intersection & Approach	Lane Group	v/c Ratio	Delay (sec)	LOS	Queue Length (ft)	Lane Group	v/c Ratio	Delay (sec)	LOS	Queue Length (ft)		Lane Group	v/c Ratio	Delay (sec)	LOS	Queue Length (ft)	
4	Hamilton Avenu	e and Stuy	vesant Place	)						•				•		•		$\overline{}$
4	Southbound	TR	0.54	21.2	С	78	TR	0.58	22.9	С	89		TR	0.58	22.9	С	89	Π
	Wall Street and	Stuyvesant	Place															Ξ
6	Eastbound	R	0.44	18.6	С	56	R	0.45	19.0	С	57		R	0.45	19.0	С	57	
	Southbound	L	0.35	42.9	Е	36	L	0.36	44.5	Е	37		L	0.36	44.5	Е	37	Ĺ
16	Van Duzer Stree																	
10	Westbound	R	0.03	15.7	С	2	R	0.03	16.4	С	2		R	0.03	16.4	С	2	Ē
	Bay Street and																	Ē
17	Eastbound	LTR	0.14	16.4	С	12	LTR	0.12	15.1	С	10		LTR	0.13	15.3	С	11	_
••	Westbound	LTR	0.02	10.3	В	2	LTR	0.02	9.9	Α	2		LTR	0.02	10.3	В	2	_
	Northbound	LTR	0.01	0.4	Α	1	LTR	0.01	0.4	Α	1		LTR	0.01	0.4	Α	1	
	Bay Street and																	_
18	Eastbound	LTR	0.62	56.1	F	86	LTR	0.69	70.3	F	100	+		s	ignalized			
	Westbound	R	0.02	9.6	Α	2	R	0.02	9.4	Α	1				igitalizea			_
	Bay Street and I	Baltic Stree																ī
21	Eastbound	LTR	0.45	58.9	F	49	LTR	0.91	210.3	F	104							_
	Westbound	LTR	0.06	68.3	F	5	LTR	0.20	239.2	F	14			S	ignalized			_
	Southbound	LT	0.00	0.0		0	LT	0.00	0.0		0							Ĺ
	Bay Street and																	ī
22	Eastbound	LR	0.58	48.6	Е	77	LR	0.95	138.8	F	152	+	LR	1.45	353.7	F	224	т
	Northbound	LT	0.01	0.4	Α	1	LT	0.02	0.7	Α	2		LT	0.02	0.8	Α	2	_
	Bay Street and																	L
23	Eastbound	LR	0.04	23.2	С	3	LR	0.07	42.2	E	6		LR	0.11	62.7	F	9	_
	Northbound	LT	0.01	0.3	Α	1	LT	0.02	0.9	Α	2		LT	0.02	1.0	Α	2	Ĺ
	Jersey Street ar																	Ξ
33	Westbound	LR	0.16	11.4	В	14	LR	0.17	12.0	В	16		LR	0.17	12.0	В	16	ī
	Southbound	LT	0.12	4.8	Α	11	LT	0.13	4.7	Α	11		LT	0.13	4.7	Α	11	Ξ
34	Pike Street and																	Ξ
04	Westbound	LT	0.02	1.6	Α	2	LT	0.02	1.6	Α	2		LT	0.02	1.6	Α	2	_
37	Pike Street and																	_
•	Southbound	LR	0.14	20.6	С	12	LR	0.22	32.4	D	20		LR	0.22	33.4	D	20	_
	Hudson Street a																	Ĺ
	Eastbound	LTR	0.03	10.4	В	3	LTR	0.03	10.4	В	3		LTR	0.03	10.4	В	3	_
39	Westbound	LTR	0.00	11.0	В	0	LTR	0.00	11.0	В	0		LTR	0.00	11.0	В	0	_
	Northbound	LTR	0.01	1.0	Α	1	LTR	0.01	1.0	Α	1		LTR	0.01	1.0	Α	1	_
	Southbound	LTR	0.00	0.0		0	LTR	0.00	0.0		0		LTR	0.00	0.0		0	_
	Broad Street an																	_
	Eastbound	LTR	0.05	1.4	Α	4	LTR	0.05	1.4	Α	4		LTR	0.05	1.4	Α	4	_
40	Westbound	LT	0.00	0.1	Α	0	LT	0.00	0.1	Α	0		LT	0.00	0.1	Α	0	_
	Northbound	LTR	0.00	0.0	Α	0	LTR	0.00	0.0	Α	0		LTR	0.00	0.0	Α	0	_
	Southbound	LR	0.46	33.0	D	55	LR	0.52	40.9	Е	67		LTR	0.52	40.9	Е	67	

Notes: Le Left Turn, T= Through, R= Right Turn, DEL = Defacto Left Turn; LOS = Level of Service, -- = Approach has no volume recorded during this peak hour, "+" implies a significant adverse impact, Err = v/c or delay exceeds the maximum limit reportable in the analysis software

Table 21-<u>11</u>: Unsignalized Level of Service Analysis – Weekday MD Peak Hour No-Action vs. With-Action vs. Mitigated Conditions

WILL	n-Action	V 3. IV	nugai	eu co	ııuı	uons											
			No-Act	ion Conditi	ons			With-Ac	tion Condit	ions		With	n-Action With	n Mitigation	n Condit	ions	
#	Intersection & Approach	Lane Group	v/c Ratio	Delay (sec)	LOS	Queue Length (ft)	Lane Group	v/c Ratio	Delay (sec)	LOS	Queue Length (ft)	Lane Group	v/c Ratio	Delay (sec)	LOS	Queue Length (ft)	
4	Hamilton Avenu	e and Stuy	vesant Place	e													
4	Southbound	TR	0.25	13.6	В	25	TR	0.27	13.8	В	27	TR	0.27	13.8	В	27	
	Wall Street and	Stuyvesant	Place														
6	Eastbound	R	0.31	13.4	В	34	R	0.32	13.6	В	34	R	0.32	13.6	В	34	
	Southbound	L	0.10	23.9	С	8	L	0.10	24.2	С	8	L	0.10	24.2	С	8	
16	Van Duzer Stree																
	Westbound	R	0.04	14.2	В	3	R	0.04	15.2	С	3	R	0.04	15.2	С	3	
	Bay Street and																
17	Eastbound	LTR	0.19	24.4	С	17	LTR	0.15	20.0	С	13	LTR	0.21	27.2	D	19	
	Westbound	LTR	0.04	10.8	В	3	LTR	0.04	10.3	В	3	LTR	0.05	11.7	В	4	<u> </u>
	Northbound	LTR	0.02	0.7	Α	2	LTR	0.02	0.6	Α	2	LTR	0.02	0.6	Α	2	
	Bay Street and																
18	Eastbound	LTR	8.60	Err	F	Err	LTR	5.65	Err	F	Err		Si	gnalized			
	Westbound	R	0.08	10.1	В	6	R	0.08	10.4	В	7			g			
	Bay Street and I																
21	Eastbound	LTR	3.03	Err	F	Err	LTR	2.25	1391.6	F	88		-				
	Westbound	LTR	Err	Err	F	Err	LTR	Err	Err	F	Err		Si	gnalized			
	Southbound	LT	0.02	2.8	Α	2	LT	0.03	4.9	Α	2						
	Bay Street and														-		ш
22	Eastbound	LR	4.41	Err	F	Err	LR	4.43	Err	F	Err	LR	9.26	Err	F	Err	
	Northbound	LT	0.15	25.8	D	12	LT	0.13	24.0	С	11	LT	0.32	166.6	F	25	+
	Bay Street and				-				0.17.0	-					-		ш
23	Eastbound	LR	0.35	213.2	F	27	LR	0.36	217.3	F	27	LR	0.93	774.8	F	44	
	Northbound	LT	0.00	0.0		0	LT	0.00	0.0		0	LT	0.00	0.0		0	
22	Jersey Street ar			44.0	-	0.4	- 15	0.00	445	-	00	- 10	0.00	44.5	-	00	<b>—</b>
33	Westbound	LR	0.22	11.9	В	21	LR	0.29	14.5	В	29	LR	0.29	14.5	В	29	<b>—</b>
	Southbound	LT Documents	0.10	3.7	Α	9	LT	0.12	3.9	Α	11	LT	0.12	3.9	Α	11	$\vdash$
34	Pike Street and	Brook Stre		4.0			1.7	0.00	4.0		2	1.7	0.00	4.0		_	$\vdash$
	Westbound		0.03	1.3	Α	2	LT	0.03	1.3	Α	2	LT	0.03	1.3	Α	2	Н
37	Pike Street and	LR		59.7	F	52	LR	1.93	727.5	F	164	LR	1.00	727.5	F	101	$\vdash$
<b>—</b>	Southbound Hudson Street a		0.47	59.7	<u> </u>	52	LK	1.93	/2/.5	l F	164	LK	1.93	/2/.5	F	164	Н
				10.1	В	2	LTR	0.02	9.9		2	LTR	0.02	0.0		2	$\vdash$
39	Eastbound	LTR LTR	0.02		В	0	LTR	0.02	10.4	A B	0	LTR	0.02	9.9 10.4	A B	0	$\vdash$
39	Westbound Northbound	LTR		10.5		1	LTR				1			1.1			Н
	Southbound	LTR	0.01	1.1 0.0	A	0	LTR	0.01 0.00	1.1 0.0	A	0	LTR LTR	0.01 0.00	0.0	A	0	$\vdash$
	Broad Street an			0.0		U	LIK	0.00	0.0		U	LIK	0.00	0.0		U	Н
		LTR	0.05	1.6	Α	4	LTR	0.05	1.5	Ι Λ	4	LTR	0.05	1.5	۸ ا	4	Н
40	Eastbound Westbound	LT	0.05	0.9	A	2	LT	0.05	0.9	A	2	LT	0.05	0.9	A	2	Н
70	Northbound	LTR	0.03	13.0	B	0	LTR	0.03	13.4	B	0	LTR	0.03	13.4	B	0	$\vdash$
1	Southbound	LIK	0.68	80.0	F	92	LIK	0.64	71.4	F	85	LTR	0.64	71.4	F	85	$\vdash$
Martan	Southbound	LK	0.00	00.0		92	LK	0.04	11.4		00	LIK	0.04	/ 1.4	Г	92	_

Notes: Le Left Turn, T= Through, R= Right Turn, DELE Defacto Left Turn; LOS = Level of Service, -- = Approach has no volume recorded during this peak hour, "+" implies a significant adverse impact, Err = v/c or delay exceeds the maximum limit reportable in the analysis software

Table 21-1<u>2</u>: Unsignalized Level of Service Analysis – Weekday PM Peak Hour No-Action vs. With-Action vs. Mitigated Conditions

VVIU	n-Action	1 V 3. IV	nugai	eu co	IIUI	uons												
			No-Act	ion Condition	ons			With-Ac	tion Condit	ions			With	h-Action Witl	h Mitigation	n Condi	ions	
#	Intersection & Approach	Lane Group	v/c Ratio	Delay (sec)	LOS	Queue Length (ft)	Lane Group	v/c Ratio	Delay (sec)	LOS	Queue Length (ft)		Lane Group	v/c Ratio	Delay (sec)	LOS	Queue Length (ft)	
4	Hamilton Avenu	e and Stuy	vesant Place	e														
-	Southbound	TR	0.18	11.8	В	16	TR	0.18	11.8	В	16		TR	0.18	11.8	В	16	
	Wall Street and																	
6	Eastbound	R	0.30	13.8	В	31	R	0.30	13.8	В	31		R	0.30	13.8	В	31	
	Southbound	L	0.14	23.3	С	12	L	0.14	23.3	С	12		L	0.14	23.3	С	12	
16	Van Duzer Stree																	
	Westbound	R	0.03	12.1	В	3	R	0.04	12.8	В	3		R	0.04	12.8	В	3	_
	Bay Street and			40.0		40	LTD	0.44	40.0				LTD	0.44	00.0		40	<u> </u>
17	Eastbound Westbound	LTR LTR	0.11	19.3 14.7	C B	10 1	LTR LTR	0.11 0.01	18.9 12.9	C B	9	Н	LTR LTR	0.14 0.01	23.0 15.1	C	12 1	⊢
	Northbound	LTR	0.01	0.2	A	1	LTR	0.01	0.3	A	1		LTR	0.01	0.3	A	1	<u> </u>
	Bay Street and			0.2	А		LIK	0.01	0.3	A		H	LIK	0.01	0.3	А		<del>                                     </del>
18	Eastbound	LTR	5.65	Err	F	Err	LTR	13.71	Err	F	Err							<u> </u>
	Westbound	R	0.08	9.7	Ä	7	R	0.08	9.8	Ä	7	-		S	ignalized			-
	Bay Street and I			5.7			- '\	0.00	5.0		· · ·	H						
	Eastbound	LTR	1.30	683.4	F	76	LTR	3.00	1965.6	F	92							
21	Westbound	LTR	1.17	2659.2	Ė	25	LTR	Err	Err	F	Err			s	ignalized			
	Southbound	LT	0.00	0.2	A	0	LT	0.01	3.7	A	1				•			
	Bay Street and \	William Stre	eet	•				•			•							
22	Eastbound	LR	3.01	Err	F	Err	LR	6.82	Err	F	Err	+	LR	14.42	Err	F	Err	+
i	Northbound	LT	0.14	13.8	В	12	LT	0.31	91.8	F	27	+	LT	0.64	298.8	F	48	+
	Bay Street and	Congress S	treet															
23	Eastbound	LR	0.40	155.2	F	34	LR	0.58	261.5	F	45		LR	0.90	494.7	F	57	
	Northbound	LT	0.03	2.1	Α	2	LT	0.06	11.9	В	5		LT	0.11	43.5	E	9	+
	Jersey Street ar	nd Brook St	reet															
33	Westbound	LR	0.19	11.8	В	17	LR	0.22	13.3	В	21		LR	0.22	13.3	В	21	
	Southbound	LT	0.08	3.0	Α	6	LT	0.09	3.0	Α	7		LT	0.09	3.0	Α	7	
34	Pike Street and																	
	Westbound	LT	0.03	1.7	Α	2	LT	0.03	1.7	Α	2		LT	0.03	1.7	Α	2	_
37	Pike Street and																	ш
	Southbound	LR	0.30	35.6	Е	30	LR	0.98	249.4	F	107		LR	0.98	249.4	F	107	$\vdash$
	Hudson Street a											Ш						$\vdash$
20	Eastbound	LTR	0.03	9.3	A	2	LTR	0.03	9.2	A	2	Ш	LTR	0.03	9.2	A	2	ш
39	Westbound	LTR	0.00	0.0	A	0	LTR	0.00	0.0	A	0		LTR	0.00	0.0	A	0	$\vdash$
	Northbound	LTR	0.01	1.7	A	1	LTR	0.01	1.7	A	1	Н	LTR	0.01	1.7	A	<u>1</u>	Н
	Southbound	LTR	0.01	4.1	Α	1	LTR	0.01	4.1	Α	1	Н	LTR	0.01	4.1	Α	1	$\vdash$
	Broad Street an	LTR		0.0		_	LTD	0.00	0.8	١ ٨	2	Н	LTD	0.00	0.0		2	$\vdash$
40	Eastbound Westbound	LIK	0.02	0.9	A	<u>2</u>	LTR LT	0.02	0.8	A	1	$\vdash$	LTR LT	0.02	0.8	A	1	$\vdash$
40	Northbound	LTR	0.00	0.2	A	0	LTR	0.01	0.2	A	0	$\vdash$	LTR	0.01	0.2	A	0	Н
I	Southbound	LIK	0.00	28.8	D D	15	LIK	0.00	32.4	D A	17	$\vdash$	LTR	0.00	32.4	D D	17	$\vdash$
Marray I	Southbound	LK	0.17	26.8	ט	15	LK	0.19	32.4	U	17		LIK	0.19	32.4	U	17	ل

Notes: Le Left Turn, T= Through, R= Right Turn, DELE Defacto Left Turn; LOS = Level of Service, -- = Approach has no volume recorded during this peak hour, "+" implies a significant adverse impact, Err = v/c or delay exceeds the maximum limit reportable in the analysis software

Table 21-1<u>3</u>: Unsignalized Level of Service Analysis – Saturday MD Peak Hour No-Action vs. With-Action vs. Mitigated Conditions

			No-Acti	ion Conditi	ons			With-Act	tion Condit	ions		v	ith-Action Wit	h Mitigatio	n Condit	ions
#	Intersection & Approach	Lane Group	v/c Ratio	Delay (sec)	LOS	Queue Length (ft)	Lane Group	v/c Ratio	Delay (sec)	LOS	Queue Length (ft)	Lane Group		Delay (sec)	LOS	Queue Length (ft
4	Hamilton Avenu	e and Stuy	vesant Place	)							'					
+	Southbound	TR	0.15	11.8	В	13	TR	0.15	11.9	В	13	TR	0.15	11.9	В	13
	Wall Street and	Stuyvesant	Place													
6	Eastbound	R	0.17	11.0	В	15	R	0.17	11.0	В	15	R	0.17	11.0	В	15
	Southbound	L	0.08	15.0	С	6	L	0.08	15.0	С	6	L	0.08	15.0	С	6
6	Van Duzer Stree	et and St Ju	lian Place													
0	Westbound	R	0.04	11.7	В	3	R	0.04	12.2	В	3	R	0.04	12.2	В	3
	Bay Street and	St Julian Pl	ace													
17	Eastbound	LTR	0.09	17.9	С	8	LTR	0.08	16.1	С	7	LTR	0.11	20.3	С	9
.,	Westbound	LTR	0.02	13.2	В	2	LTR	0.02	11.7	В	2	LTR	0.03	14.4	В	2
	Northbound	LTR	0.01	0.2	Α	1	LTR	0.01	0.2	Α	1	LTR	0.01	0.2	Α	1
	Bay Street and	Grant Stree	t													
18	Eastbound	LTR	4.08	Err	F	Err	LTR	5.09	Err	F	Err			ignalized		
	Westbound	R	0.09	9.9	Α	8	R	0.10	10.2	В	8		-	ignanzeu		
	Bay Street and	Baltic Stree	t													
21	Eastbound	LTR	1.39	675.4	F	86	LTR	2.18	1230.9	F	97					
	Westbound	LTR	5.02	Err	F	Err	LTR	Err	Err	F	Err		S	ignalized		
	Southbound	LT	0.00	0.0		0	LT	0.00	0.0	-	0					
	Bay Street and	William Stre	eet													
22	Eastbound	LR	1.81	568.0	F	219	LR	2.91	1110.4	F	281	LR	5.63	Err	F	Err
	Northbound	LT	0.07	6.5	Α	6	LT	0.09	11.6	В	7	LT	0.21	69.8	F	17
	Bay Street and															
23	Eastbound	LR	0.09	96.7	F	7	LR	0.12	140.5	F	10	LR	0.35	475.1	F	21
	Northbound	LT	0.01	1.2	Α	1	LT	0.02	2.3	Α	1	LT	0.04	11.9	В	3
	Jersey Street an															
33	Westbound	LR	0.15	10.6	В	13	LR	0.17	11.7	В	16	LR	0.17	11.7	В	16
	Southbound	LT	0.05	2.2	Α	4	LT	0.06	2.3	Α	4	LT	0.06	2.3	Α	4
34	Pike Street and	Brook Stre														
•	Westbound	LT	0.02	1.4	Α	1	LT	0.02	1.5	Α	1	LT	0.02	1.5	Α	1
7	Pike Street and															
	Southbound	LR	0.31	48.4	Е	30	LR	0.73	181.2	F	73	LR	0.73	181.2	F	73
	Hudson Street a															
	Eastbound	LTR	0.02	9.6	Α	2	LTR	0.02	9.5	Α	2	LTR	0.02	9.5	Α	2
39	Westbound	LTR	0.00	9.2	Α	0	LTR	0.00	9.2	A	0	LTR	0.00	9.2	Α	0
	Northbound	LTR	0.01	2.0	Α	1	LTR	0.01	2.0	A	1	LTR	0.01	2.0	Α	1
	Southbound	LTR	0.00	0.0		0	LTR	0.00	0.0		0	LTR	0.00	0.0		0
	Broad Street an															
	Eastbound	LTR	0.01	0.4	Α	1	LTR	0.01	0.3	Α	1	LTR	0.01	0.3	A	1
40	Westbound	LT	0.01	0.4	Α	1	LT	0.01	0.3	Α	1	LT	0.01	0.3	Α	1
	Northbound	LTR	0.01	19.1	С	1	LTR	0.02	20.5	С	1	LTR	0.02	20.5	С	1
	Southbound	LR	0.21	30.3	D	19	LR	0.22	31.5	D	20	LTR	0.22	31.5	О	20

# TRANSIT (BUS)

The Proposed Actions would result in a capacity shortfall on all bus routes serving the study area during the Weekday AM and PM peak hours, as shown in Table  $21-1\underline{4}$ . These significant adverse impacts could be fully mitigated by the addition of two to six additional standard buses to each direction of each route during both peak hours, as shown in Table  $21-1\underline{4}$ . The general policy of NYCT is to provide additional bus service where demand warrants, taking into account financial and operational constraints.

Table 21-14: With-Action With-Mitigation Conditions Local Bus Analysis

Route	Peak Direction	Maximum Load Point	Peak Hour Buses <sup>(1)</sup>	Peak Hour Passengers	Average Passengers Per Bus	Total Capacity	Available Capacity	Additional Buses for Mitigation	Total Mitigated Peak Hours Buses	Available Capacity with Mitigation
					Weekday AM					
S51/81	NB	Bay Street and Canal Street	7	644	92	378	-266	5	12	4
S51/81	SB	Bay Street and Victory Boulevard	4	317	79	216	-101	2	6	7
S74/84	NB	Bay Street and Victory Boulevard	6	503	84	324	-179	4	10	37
S74/84	SB	Richmond Road and Clove Road	4	321	80	216	-105	2	6	3
S76/86	NB	Bay Street and Victory Boulevard	7	694	99	378	-316	6	13	8
S76/86	SB	Richmond Road and Clove Road	6	406	68	324	-82	2	8	26
S78	NB	Bay Street and Victory Boulevard	6	554	92	324	-230	5	11	40
S78	SB	Hylan Boulevard and Clove Road	7	472	67	378	-94	2	9	14
					Weekday PM					
S51/81	NB	Bay Street and Victory Boulevard	4	473	118	216	-257	5	9	13
S51/81	SB	Bay Street and Victory Boulevard	7	536	77	378	-158	3	10	4
S74/84	NB	Targee Street and DeKalb Street	4	304	76	216	-88	3	7	74
S74/84	SB	Bay Street and Victory Boulevard	5	397	79	270	-127	3	8	35
S76/86	NB	Bay Street and Victory Boulevard	4	417	104	216	-201	4	8	15
S76/86	SB	Bay Street and Victory Boulevard	5	499	100	270	-229	5	10	41
S78	NB	Hylan Boulevard and Clove Road	4	370	92	216	-154	3	7	8
S78	SB	Bay Street and Victory Boulevard	5	391	78	270	-121	3	8	41
lotes:										
		ntly available data from NYCT/MTA.								
<ol><li>Availab</li></ol>	le canacity ba	sed on a maximum of 54 passengers pe	r bus (40-foot star	ndard huses)						

# **PEDESTRIAN**

As discussed in Chapter 14, "Transportation," the results of the analyses of pedestrian conditions show that demand from the Proposed Actions would significantly adversely impact a total of 11 sidewalks and <u>five</u> crosswalks in one or more peak hours under the With-Action condition, as shown in Tables 21-15 through 21-17.

Table 21-15: Summary of Significant Pedestrian Sidewalk Impacts

				Availa	ble Circ	ulation	Space								
	Total				(ft <sup>2</sup>	<sup>2</sup> /p)		Non-Pl	atoon C	onditio	ns LOS	Plato	on Cor	ditions	LOS
	Width	Obstruction	Effective	'	Neekda	у	Sat	٧	Veekda	у	Sat	٧	Veekda	ıy	Sat
Location	(ft.)	Width (ft.)	Width	AM	MD	PM	MD	AM	MD	PM	MD	AM	MD	PM	MD
Bay St and Victory Blvd (S leg, E sidewalk)	20	11.5	8.5	179.0	80.7	87.1	66.2	Α	Α	Α	Α	В	С	С	С
Bay St and Hannah St (N leg, E sidewalk)	20	11.5	8.5	151.0	56.6	56.1	62.8	Α	В	В	Α	В	С	С	С
Bay St and Hannah St (E leg, N sidewalk)	5	4.5	0.5	17.5	3.5	11.4	8.8	D +	F +	E +	E +	E +	F +	E +	F +
Bay St and Hannah St (S leg, E sidewalk)	7	3	4	112.0	56.7	49.7	58.7	Α	В	В	В	В	С	С	С
Bay St and Hannah St (E leg, S sidewalk)	3.5	3	0.5	4.6	4.6	6.2	11.3	F +	F +	F +	E +	F +	F +	F +	E +
Bay St and Swan St (S leg, W sidewalk)	14.5	11	3.5	83.9	41.9	49.1	50.0	Α	В	В	В	С	С	С	С
Bay St and Clinton St (N leg, E sidewalk)	13	8	5	107.0	64.9	64.5	93.4	Α	Α	Α	Α	В	С	С	В
Bay St and Clinton St (N leg, W sidewalk)	8.5	6.8	1.8	108.0	40.3	40.6	45.8	Α	В	В	В	В	С	С	С
Bay St and Baltic St (N leg, E sidewalk)	16	9.5	6.5	193.0	119.0	108.0	89.9	Α	Α	Α	Α	В	В	В	С
Bay St and Baltic St (N leg, W sidewalk)	4.5	3.5	1	75.9	27.5	28.7	30.5	Α	С	С	С	С	D +	D +	D +
Bay St and Wave St (N leg, E sidewalk)	5.1	3	2.1	42.8	30.1	24.5	19.0	В	С	С	D +	С	D +	D +	E +
Bay St and Wave St (S leg, E sidewalk)	7.3	3	4.3	63.4	56.3	44.6	39.7	Α	В	В	С	С	С	С	D +
Bay St and Wave St (S leg, W sidewalk)	4.2	3.5	0.7	23.9	12.9	14.9	13.9	D +	E +	E +	E +	D +	E +	E +	E +
Bay St and Wave St (N leg, W sidewalk)	5	3.5	1.5	45.1	17.0	16.7	18.9	В	D +	D +	D +	С	E +	E +	E +
Front St and Hannah St (S leg, E sidewalk)	8	3	5	750.0	1240.0	1472.0	461.0	Α	Α	Α	Α	Α	Α	Α	В
Front St and Hannah St (S leg, W sidewalk)	6	3	3	55.2	28.4	35.7	15.3	В	С	С	D +	С	D +	D +	E +
Front St and Wave St (N leg, E sidewalk)	17	14	3	54.0	53.5	34.1	33.0	В	В	С	С	С	С	D +	D +
Front St and Wave St (N leg, W sidewalk)	12	6	6	228.0	106.0	337.0	78.3	Α	Α	Α	Α	В	В	В	С
Pike St and Brook St (W leg, S sidewalk)	6	3	3	842.0	201.0	767.0	662.0	Α	Α	Α	Α	Α	В	Α	Α
Jersey St and Victory Blvd (N leg, E sidewalk)	10	6.3	3.8	315.0	132.0	180.0	159.0	Α	Α	Α	Α	В	В	В	В
Jersey St and Victory Blvd (E leg, N sidewalk)	8	3	5	181.0	48.0	80.0	71.0	Α	В	Α	Α	В	С	С	С
Jersey St and Victory Blvd (E leg, S sidewalk)	4	3	1	190.0	39.5	44.2	64.1	Α	С	В	Α	В	D +	С	С
Bay St and Minthorne St (E leg, S sidewalk)	10	4.5	5.5	126.0	66.3	52.6	121.0	Α	Α	В	Α	В	С	С	В
Minthorne St and Victory Blvd (S leg, E sidewalk)	5	3	2	2444.0	1629.0	4888.0	815.0	Α	Α	Α	Α	Α	Α	Α	Α
Minthorne St and Victory Blvd (E leg, S sidewalk)	8.5	3	5.5	747.0	640.0	840.0	747.0	Α	Α	Α	Α	Α	Α	Α	Α
Minthorne St and Victory Blvd (W leg, S sidewalk)	8.5	3	5.5	249.0	106.0	163.0	115.0	Α	Α	Α	Α	В	В	В	В
Front St and Baltic St (N leg, E sidewalk)	12	3	9	172.0	474.0	152.0	157.0	Α	Α	Α	Α	В	В	В	В
Front St and Baltic St (N leg, W sidewalk)	5.5	3	2.5	99.0	29.6	32.2	26.0	Α	С	С	С	В	D +	D +	D +
Note: "+" implies a significant adverse impact.															•

<sup>\*</sup>This table has been modified for the FEIS.

Table 21-16: Summary of Significant Pedestrian Crosswalk Impacts Signalized Intersections

			Availal	ole Circula	e (ft²/p)	Cros	swalk Ci	rculatio	n LOS	
	Length	Width		Weekday		SAT		Weekda	у	Sat
Location	(ft.)	(ft.)	AM	MD	PM	MD	AM	MD	PM	MD
Bay St and Victory Blvd (S leg)	60.0	21.5	75.1	33.8	40.1	64.2	Α	С	В	Α
Bay St and Hannah St (N leg)	92.0	11.0	80.7	18.8	14.8	31.3	Α	D +	E +	С
Bay St and Hannah St (E leg)	32.0	12.5	148	33.8	54.8	41	Α	С	В	В
Bay St and Clinton St (N leg)	60.0	11.5	121	73	74.1	87.1	Α	Α	Α	Α
Bay St and Clinton St (S leg)	59.5	13.0	231	49.2	79.4	111	Α	В	Α	Α
Bay St and Clinton St (W leg)	24.0	11.0	438	98.8	136	172	Α	Α	Α	Α
Bay St and Wave St (N leg)	35.5	10.0	134	35	20.4	34.5	Α	С	D +	С
Bay St and Wave St (E leg)	30.3	11.3	82.6	45.5	58	38.7	Α	В	В	С
Bay St and Wave St (S leg)	36.8	10.0	140	32.8	16.7	28.4	Α	С	D +	С
Bay St and Wave St (W leg)	21.3	10.6	175	64.8	92.8	69.3	Α	Α	Α	Α
Front St and Hannah St (W leg)	34.5	10.0	49.5	45.3	22.7	22.1	В	В	D +	D +
Jersey St and Victory Blvd (N leg)	36.0	10.0	289	77.3	167	137	Α	Α	Α	Α
Jersey St and Victory Blvd (E leg)	40.0	10.0	69.8	13.2	23.1	22.2	Α	E +	D +	D +

Note: "+" implies a significant adverse impact.

This table has been modified for the FEIS.

Table 21-17: Summary of Significant Pedestrian Crosswalk Impacts Unsignalized Intersections

			Ave	rage Pedes	strian Dela	y (s)	Cros	swalk Ci	rculation	LOS
				Weekday		Sat		Weekday	1	Sat
Location	Length (ft)	Width (ft)	АМ	MD	PM	MD	АМ	MD	PM	MD
Bay St and Grant St (W leg)	37.4	8.0	2.4	0.9	2.1	1.7	Α	Α	Α	Α
Bay St and Baltic St (W leg)	23.5	12.0	0.6	0.2	0.2	0.3	Α	Α	Α	Α
Bay St and Minthorne St (E leg)	29.5	10.0	5.0	3.6	2.4	2.3	Α	Α	Α	Α

EFFECTS OF TRAFFIC MITIGATION ON PEDESTRIAN CONDITIONS

Proposed traffic mitigation measures would potentially affect pedestrian conditions at a total of eight intersections during one or more peak hours, including the intersections at Bay Street with Grant Street and Bay Street with Baltic Street, where new traffic signals are proposed. At these intersections, it was assumed that as part of the new traffic signals, crosswalks across Bay Street would be added; the east crosswalk at the Bay Street and Baltic Street intersection was not included in the analysis as it is across an existing driveway.

In total, potential traffic mitigation measures would result in new significant adverse impacts at five crosswalks: the south crosswalk at the Bay Street and Victory Boulevard intersection, the north and east crosswalks at the Bay Street and Hannah Street intersection, and the north and south crosswalks at the Bay Street and Wave Street intersection. Table 21-18 shows conditions at these pedestrian elements with the proposed traffic mitigation measures.

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Table 21-1 $\underline{\underline{\bf a}}$ : Summary of Significant Pedestrian Crosswalk Impacts with Vehicle Mitigation

**Signalized Intersections** 

			Availa	ble Circula	tion Space	e (ft²/p)		Crossw	alk Ci	rculatio	n LOS	;	
				Weekday		Sat		Week	day			Sa	t
Location	Length (ft)	Width (ft)	AM	MD	PM	MD	АМ	М	)	PN	1	ME	)
Bay St and Victory Blvd (S leg)	60.0	21.5	82.3	20.8	50.3	73.1	Α	D	+	В		Α	
Bay St and Hannah St (N leg)	92.0	11.0	147	13.2	26.2	22.4	Α	Е	+	С		D	+
Bay St and Hannah St (E leg)	32.0	12.5	75.5	16.4	19.7	21.7	Α	D	+	D	+	D	+
Bay St and Grant St (N leg)	59.0	10.0	75.4	60.6	32.3	55.8	Α	Α		С		В	
Bay St and Grant St (S leg)	59.0	10.0	126	35.5	61.9	60.7	Α	С		Α		Α	
Bay St and Grant St (W leg)	21.0	7.0	254	51.7	108	92.8	Α	В		Α		Α	
Bay St and Clinton St (N leg)	60.0	11.5	78.7	39.7	30.5	47.2	Α	С		С		В	
Bay St and Clinton St (S leg)	59.5	13.0	148	25.1	29.0	56.9	Α	С		С		В	
Bay St and Clinton St (W leg)	24.0	11.0	464	111	168	188	Α	Α		Α		Α	
Bay St and Baltic St (N leg)	37.0	11.0	137	24.9	40.3	36.1	Α	С		В		С	
Bay St and Baltic St (S leg)	36.0	22.0	233	24.1	44.4	50.1	Α	С		В		В	
Bay St and Baltic St (W leg)	23.5	12.0	451	143.1	205.1	182.4	Α	Α		Α		Α	
Bay St and Wave St (N leg)	35.5	10.0	75.3	15.6	10.2	18.2	Α	D	+	Е	+	D	+
Bay St and Wave St (E leg)	30.3	11.3	99.0	63.1	66.6	51.6	Α	Α		Α		В	
Bay St and Wave St (S leg)	36.8	10.0	79.9	14.6	8.6	15.3	Α	Е	+	Е	+	D	+
Bay St and Wave St (W leg)	21.3	10.6	206	88.3	106	90.5	Α	Α		Α		Α	
Front St and Hannah St (W leg)	34.5	10.0	50.6	49.1	23.2	22.6	В	В		D	+	D	+
Jersey St and Victory Blvd (N leg)	36.0	10.0	261	77.3	167	137	Α	Α		Α		Α	
Jersey St and Victory Blvd (E leg)	40.0	10.0	78.4	13.2	23.1	22.2	Α	Е	+	D	+	D	+

Note: "+" implies a significant adverse impact.

A significant adverse pedestrian impact is considered mitigated if measures implemented return the anticipated conditions to an acceptable level, following the same impact criteria used in determining impacts. Standard mitigation for projected significant adverse pedestrian impacts can include providing additional signal green time or new signal phases; widening crosswalks; relocating or removing street furniture; providing curb extensions, neck-downs, or lane reductions to reduce pedestrian crossing distance; and sidewalk widening. Discussed below are recommended mitigation measures to address the Proposed Actions' potential significant adverse pedestrian impacts. The mitigation measures generally consist of crosswalk widening. If, prior to implementation, DOT determines that an identified mitigation measure is infeasible, an alternative and equivalent mitigation measure will be considered. However, if no other alternative mitigation measures can be identified, those impacts would be unmitigated.

#### **SIDEWALKS**

Of the 28 sidewalks analyzed, 11 are expected to be significantly adversely impacted during one or more peak hours, as shown in Table  $21-1\underline{9}$ . Due to constrained right-of-way, mitigation measures to address the potential significant adverse pedestrian impacts for the 11 sidewalks are not feasible. Therefore, these sidewalks could not be mitigated and the impacts are considered significant and unavoidable.

#### **CROSSWALKS**

With the implementation of vehicle mitigation measures, seven of the 20 analyzed crosswalks would be significantly adversely impacted by the Proposed Actions during one or more peak hours. Tables 21-20 and 21-21 shows the recommended mitigation measures to address these impacts and their effectiveness. As discussed below, the implementation of the proposed mitigation measures would fully mitigate seven crosswalk elements.

Measures to mitigate the potentially significant adverse crosswalk impacts are as follows:

- Bay Street and Victory Boulevard, south crosswalk: to fully mitigate this potential significant adverse pedestrian impact, the crosswalk would have to be widened by 3.2 feet.
- Bay Street and Hannah Street, north crosswalk: to fully mitigate this potential significant adverse pedestrian impact, the crosswalk would have to be widened by 8.6 feet.
- Bay Street and Hannah Street, east crosswalk: to fully mitigate this potential significant adverse pedestrian impact, the crosswalk would have to be widened by 5.2 feet.
- Bay Street and Wave Street, north crosswalk: to fully mitigate this potential significant adverse pedestrian impact, the crosswalk would have to be widened by 5.6 feet.
- Bay Street and Wave Street, south crosswalk: to fully mitigate this potential significant adverse pedestrian impact, the crosswalk would have to be widened by 10.3 feet.
- Front Street and Hannah Street, west crosswalk: to fully mitigate this potential significant adverse pedestrian impact, the crosswalk would have to be widened by 0.6 feet.
- *Jersey Street and Victory Boulevard, east crosswalk:* to fully mitigate this potential significant adverse pedestrian impact, the crosswalk would have to be widened by 7.1 foot.

Table 21-19: With-Action With-Mitigation Sidewalk Conditions

			ľП			ulation										
	Total				(ft <sup>2</sup>	²/p)		Non-Pl	atoon C	onditio	ns LOS	Plate	on Cor	ditions	LOS	
		Obstruction	Effective	1	Neekda	v	Sat	١	Neekda	V	Sat	٧	Veekda	ıy	Sat	Proposed
Location	(ft.)	Width (ft.)	Width	AM	MD	PM	MD	AM	MD	PM	MD	AM	MD	PM	MD	Mitigation
Bay St and Victory Blvd (S leg, E sidewalk)	20	11.5	8.5	179.0	80.7	87.1	66.2	Α	Α	Α	Α	В	С	С	С	Ĭ.
Bay St and Hannah St (N leg, E sidewalk)	20	11.5	8.5	151.0	56.6	56.1	62.8	Α	В	В	Α	В	С	С	С	-
Bay St and Hannah St (E leg, N sidewalk)	5	4.5	0.5	17.5	3.5	11.4	8.8	D +	F +	E +	E +	E +	F +	E +	F +	Unmitigatable
Bay St and Hannah St (S leg, E sidewalk)	7	3	4	112.0	56.7	49.7	58.7	Α	В	В	В	В	С	С	С	-
Bay St and Hannah St (E leg, S sidewalk)	3.5	3	0.5	4.6	4.6	6.2	11.3	F +	F +	F +	E +	F +	F +	F +	E +	Unmitigatable
Bay St and Swan St (S leg, W sidewalk)	14.5	11	3.5	83.9	41.9	49.1	50.0	Α	В	В	В	С	С	С	С	-
Bay St and Clinton St (N leg, E sidewalk)	13	8	5	107.0	64.9	64.5	93.4	Α	Α	Α	Α	В	С	С	В	-
Bay St and Clinton St (N leg, W sidewalk)	8.5	6.8	1.8	108.0	40.3	40.6	45.8	Α	В	В	В	В	С	С	С	-
Bay St and Baltic St (N leg, E sidewalk)	16	9.5	6.5	193.0	119.0	108.0	89.9	Α	Α	Α	Α	В	В	В	С	-
Bay St and Baltic St (N leg, W sidewalk)	4.5	3.5	1	75.9	27.5	28.7	30.5	Α	С	С	С	С	D +	D +	D +	Unmitigatable
Bay St and Wave St (N leg, E sidewalk)	5.1	3	2.1	42.8	30.1	24.5	19.0	В	С	С	D +	С	D +	D +	E +	Unmitigatable
Bay St and Wave St (S leg, E sidewalk)	7.3	3	4.3	63.4	56.3	44.6	39.7	Α	В	В	С	С	С	С	D +	Unmitigatable
Bay St and Wave St (S leg, W sidewalk)	4.2	3.5	0.7	23.9	12.9	14.9	13.9	D +	E +	E +	E +	D +	E +	E +	E +	Unmitigatable
Bay St and Wave St (N leg, W sidewalk)	5	3.5	1.5	45.1	17.0	16.7	18.9	В	D +	D +	D +	С	E +	E +	E +	Unmitigatable
Front St and Hannah St (S leg, E sidewalk)	8	3	5	750.0	1240.0	1472.0	461.0	Α	Α	Α	Α	Α	Α	Α	В	-
Front St and Hannah St (S leg, W sidewalk)	6	3	3	55.2	28.4	35.7	15.3	В	С	С	D +	С	D +	D +	E +	Unmitigatable
Front St and Wave St (N leg, E sidewalk)	17	14	3	54.0	53.5	34.1	33.0	В	В	С	С	С	С	D +	D +	Unmitigatable
Front St and Wave St (N leg, W sidewalk)	12	6	6	228.0	106.0	337.0	78.3	Α	Α	Α	Α	В	В	В	С	-
Pike St and Brook St (W leg, S sidewalk)	6	3	3	842.0	201.0	767.0	662.0	Α	Α	Α	Α	Α	В	Α	Α	-
Jersey St and Victory Blvd (N leg, E sidewalk)	10	6.3	3.8	315.0	132.0	180.0	159.0	Α	Α	Α	Α	В	В	В	В	-
Jersey St and Victory Blvd (E leg, N sidewalk)	8	3	5	181.0	48.0	80.0	71.0	Α	В	Α	Α	В	С	С	С	-
Jersey St and Victory Blvd (E leg, S sidewalk)	4	3	1	190.0	39.5	44.2	64.1	Α	С	В	Α	В	D +	С	С	Unmitigatable
Bay St and Minthorne St (E leg, S sidewalk)	10	4.5	5.5	126.0	66.3	52.6	121.0	Α	Α	В	Α	В	С	С	В	-
Minthorne St and Victory Blvd (S leg, E sidewalk)	5	3	2	2444.0	1629.0	4888.0	815.0	Α	Α	Α	Α	Α	Α	Α	Α	-
Minthorne St and Victory Blvd (E leg, S sidewalk)	8.5	3	5.5	747.0	640.0	840.0	747.0	Α	Α	Α	Α	Α	Α	Α	Α	-
Minthorne St and Victory Blvd (W leg, S sidewalk)	8.5	3	5.5	249.0	106.0	163.0	115.0	Α	Α	Α	Α	В	В	В	В	-
Front St and Baltic St (N leg, E sidewalk)	12	3	9	172.0	474.0	152.0	157.0	Α	Α	Α	Α	В	В	В	В	-
Front St and Baltic St (N leg, W sidewalk)	5.5	3	2.5	99.0	29.6	32.2	26.0	Α	С	С	С	В	D +	D +	D +	Unmitigatable
Note: "+" implies a significant adverse impact.			•													

This table has been modified for the FEIS.

Table 21-20: With-Action With-Mitigation Crosswalk Conditions Signalized Intersections

			Availal	ble Circula	tion Space	e (ft²/p)		Crosswalk Ci	rculation LOS	3	
				Weekday		Sat		Weekday		Sat	
Location	Length (ft)	Width (ft)	АМ	MD	PM	MD	АМ	MD	PM	MD	Proposed Mitigation
Bay St and Victory Blvd (S leg)	60.0	24.7	95.0	24.1	58.1	84.3	Α	С	В	Α	Increase crosswalk width by 3.2'
Bay St and Hannah St (N leg)	92.0	19.6	263	24.0	48.1	40.5	Α	С	В	В	Increase crosswalk width by 8.6'
Bay St and Hannah St (E leg)	32.0	17.7	108.9	24.0	28.9	31.6	Α	С	С	С	Increase crosswalk width by 5.2'
Bay St and Grant St (N leg)	59.0	10.0	75.4	60.6	32.3	55.8	Α	Α	С	В	-
Bay St and Grant St (S leg)	59.0	10.0	126	35.5	61.9	60.7	Α	С	Α	Α	-
Bay St and Grant St (W leg)	21.0	7.0	254	51.7	108	92.8	Α	В	Α	Α	-
Bay St and Clinton St (N leg)	60.0	11.5	78.7	39.7	30.5	47.2	Α	С	С	В	-
Bay St and Clinton St (S leg)	59.5	13.0	148	25.1	29.0	56.9	Α	С	С	В	-
Bay St and Clinton St (W leg)	24.0	11.0	464	111	168	188	Α	Α	Α	Α	-
Bay St and Baltic St (N leg)	37.0	11.0	137	24.9	40.3	36.1	Α	С	В	С	-
Bay St and Baltic St (S leg)	36.0	22.0	233	24.1	44.4	50.1	Α	С	В	В	-
Bay St and Baltic St (W leg)	23.5	12.0	451	143.1	205.1	182.4	Α	Α	Α	Α	-
Bay St and Wave St (N leg)	35.5	15.6	118.9	25.2	16.9	29.5	Α	С	D	С	Increase crosswalk width by 5.6'
Bay St and Wave St (E leg)	30.3	11.3	99.0	63.1	66.6	51.6	Α	Α	Α	В	-
Bay St and Wave St (S leg)	36.8	20.3	165.0	31.3	19.1	33.1	A	С	D	С	Increase crosswalk width by 10.3'
Bay St and Wave St (W leg)	21.3	10.6	206	88.3	106	90.5	Α	Α	Α	Α	-
Front St and Hannah St (W leg)	34.5	10.6	53.8	52.2	24.7	24.1	В	В	С	С	Increase crosswalk width by 0.6'
Jersey St and Victory Blvd (N leg)	36.0	10.0	261	77.3	167	137	Α	Α	Α	Α	-
Jersey St and Victory Blvd (E leg)	40.0	17.1	137.3	24.2	41.6	39.9	Α	С	В	С	Increase crosswalk width by 7.1'

Note: \*-\* implies that there is no proposed mitigation. Bay/Grant and Bay/Baltic are unsignalized in the No Action/With Action conditions and will be signalized in the Mitigation condition only.

Table 21-21: With-Action With-Mitigation Crosswalk Conditions Unsignalized Intersections

		Ave	rage Pedes	strian Dela	y (s)	Cros	swalk Ci	rculation	LOS
			Weekday		Sat		Weekday	1	Sat
Length (ft)	Width (ft)	АМ	MD	PM	MD	АМ	MD	РМ	MD
29.5	10.0	5.0	3.6	2.4	2.3	Α	Α	Α	Α
	(ft)	(ft) (ft)	Length (ft) (ft) AM	Length (ft) Width (ft) AM MD	Length (ft) Width (ft) AM MD PM	Length (ft) (ft) AM MD PM MD	Length (ft) Width (ft) AM MD PM MD AM	Length (ft) Width (ft) AM MD PM MD AM MD	Length (ft) Width (ft) AM MD PM MD AM MD PM

Note: \* - Intersection becomes signalized in Mitigation condition.

#### PROPOSED SCHEDULE FOR PEDESTRIAN MITIGATION MEASURES

Subject to DOT approval, the mitigation measures described above would be implemented to mitigate the significant adverse pedestrian impacts resulting from full build-out of the Proposed Actions in 2030. As the development of the Proposed Actions would be expected to occur over a 12-year period, it is possible that some of the significant adverse impacts to sidewalks, crosswalks and corner areas could occur prior to full build-out in 2030. <u>Details regarding the TMP</u>, which will confirm proposed mitigations measures, are discussed at the beginning of the Transportation section of this chapter.

Implementation of mitigation measures to address significant adverse pedestrian impacts should be coordinated with the completion of construction of adjacent projected development sites.

- Pedestrian mitigation measures at the Bay Street and Victory Boulevard intersection should be done in coordination with construction of Site 7.
- Pedestrian mitigation measures at the Bay Street and Hannah Street intersection should be done in coordination with construction of Sites 2 and 8.
- Pedestrian mitigation measures at the Bay Street and Wave Street intersection should be done in coordination with construction of Site 6.
- Pedestrian mitigation measures at the Front Street and Hannah Street intersection should be done in coordination with construction of Stapleton Waterfront Phase III Site.
- Pedestrian mitigation measures at the Jersey Street and Victory Boulevard intersection should be done in coordination with construction of Disposition Site 2.

### **PARKING**

As discussed in Chapter 14, "Transportation," the Proposed Actions is not expected to result in significant adverse on-street parking impacts during the Weekday AM, MD, PM, or overnight periods, or the Saturday MD period. However, the proposed traffic mitigations would incorporate a number of modifications to curbside parking regulations. Additional restrictions would be implemented at approximately four locations within ¼-mile of the <u>Project Area</u>, which would result in the displacement of approximately 14 on-street parking spaces. Accounting for these displaced spaces, a total of approximately 1,259, 472, 1,374, and 776 on-street parking spaces would remain available during the Weekday AM, MD, PM, and overnight periods, respectively, and 1,298 on-street parking spaces would remain available during the Saturday MD period, as shown in Table 21-22. However, at the subarea level, parking demand is expected to exceed available on-street parking for the following conditions:

- St. George/Ferry Terminal: a parking deficit of 133 parking spaces of the total 1,076 on-street spaces is expected during the Weekday MD period.
- Bay Street North: a parking deficit of 283 parking spaces of the total 1,319 on-street spaces is expected during the Weekday MD period.
- Bay Street South: a parking deficit of 101, 77, and 491 parking spaces of the total 1,090 onstreet spaces is expected during the Weekday AM, Weekday PM, and Weekday overnight periods, respectively, and a parking deficit of 62 parking spaces is expected during the Saturday MD period.

The expected on-street parking deficits in the Bay Street South subarea during the Weekday AM, Weekday PM, and Saturday MD periods would be less than half the available on-street parking spaces (101 of 333 available spaces, 77 of 435 available spaces, and 62 of 343 available spaces, respectively), and would therefore not be considered significant. The expected on-street parking deficits within the St. George/Ferry Terminal, Bay Street North, and Bay Street South (Weekday overnight only) would be greater than half the available on-street parking spaces. However, given the proximity to multiple bus routes on Bay Street/Richmond Terrace, the Staten Island Ferry, and the SIR, and the availability of parking spaces in adjacent subareas, the expected parking deficits are not considered significant. Furthermore, as shown in Table 20-22, the total parking availability within the ¼-mile radius of the overall Study Area would be sufficient to accommodate any shortfall within a specific subarea. The proposed traffic mitigation measures would therefore not result in new significant adverse impacts to on-street parking conditions within ¼-mile of the Project Area.

Table 21-22: With Action With Mitigation 1/4-Mile On-Street Parking Utilization Summary (Subareas and Total)

2030 With-Action With Mitigation	Weekday AM	Weekday MD	Weekday PM	Weekday Overnight	Saturday MD
St. George/Ferry Terminal Area With-Action On-Street Capacity	1076	1076	1076	1076	1076
St. George/Ferry Terminal Area Net Change in With-Action With Mitigation On-Street Parking Supply (1)	0	0	0	0	0
St. George/Ferry Terminal Area With-Action With Mitigation On-Street Capacity	1076	1076	1076	1076	1076
St. George/Ferry Terminal Area With-Action Total On-Street Demand	877	1209	814	794	870
St. George/Ferry Terminal Area Available Spaces	199	-133	262	282	206
St. George/Ferry Terminal Subarea: With-Action With Mitigation Utilization	82%	112%	76%	74%	81%
Bay Street North Area With-Action On-Street Capacity	1319	1319	1319	1319	1319
Bay Street North Area Net Change in With-Action With Mitigation On-Street Parking Supply <sup>(1)</sup>	-6	-6	-6	-6	-6
Bay Street North Area With-Action With Mitigation On-Street Capacity	1313	1313	1313	1313	1313
Bay Street North Area With-Action Total On-Street Demand	1030	1596	1047	1089	989
Bay Street North Area Available Spaces	283	-283	266	224	324
Bay Street North Subarea: With-Action With Mitigation Utilization	78%	122%	80%	83%	75%
Victory Boulevard/Jersey Street Area With-Action On-Street Capacity	1295	1295	1295	1295	1295
Victory Boulevard/Jersey Street Area Net Change in With-Action With Mitigation On-Street Parking Supply (1)	0	0	0	0	0
Victory Boulevard/Jersey Street Area With-Action With Mitigation On-Street Capacity	1295	1295	1295	1295	1295
Victory Boulevard/Jersey Street Area With-Action Total On-Street Demand	776	752	778	820	790
Victory Boulevard/Jersey Street Area Available Spaces	519	543	517	475	505
Victory Boulevard/Jersey Street Subarea: With-Action With Mitigation Utilization	60%	58%	60%	63%	61%
Canal Street Area With-Action On-Street Capacity	1363	1363	1363	1363	1363
Canal Street Area Net Change in With-Action With Mitigation On-Street Parking Supply (1)	-3	-3	-3	-3	-3
Canal Street Area With-Action With Mitigation On-Street Capacity	1360	1360	1360	1360	1360
Canal Street Area With-Action Total On-Street Demand	1001	1049	955	1074	1035
Canal Street Area Available Spaces	359	311	405	286	325
Canal Street Subarea: With-Action With Mitigation Utilization	74%	77%	70%	79%	76%
Bay Street South Area With-Action On-Street Capacity	1090	1090	1090	1090	1090
Bay Street South Area Net Change in With-Action With Mitigation On-Street Parking Supply <sup>(1)</sup>	-5	-5	-5	-5	-5
Bay Street South Area With-Action With Mitigation On-Street Capacity	1085	1085	1085	1085	1085
Bay Street South Area With-Action Total On-Street Demand	1186	1051	1162	1576	1147
Bay Street South Area Available Spaces	-101	34	-77	-491	-62
Bay Street South Subarea: With-Action With Mitigation Utilization	109%	97%	107%	145%	106%
Total With-Action Capacity	6143	6143	6143	6143	6143
Net Change in With-Action With Mitigation On-Street Parking Supply <sup>(1)</sup>	-14	-14	-14	-14	-14
Total With-Action With Mitigation On-Street Capacity	6129	6129	6129	6129	6129
Total With-Action On-Street Demand	4870	5657	4755	5353	4831
Total Available Spaces	1259	472	1374	776	1298
Total With-Action With Mitigation Utilization	79%	92%	78%	87%	79%
Note:					
1. Parking spaces lost due to mitigation measures					

#### **G.** CONSTRUCTION

### HISTORIC AND CULTURAL RESOURCES

As described in Chapter 7, "Historic and Cultural Resources," development under the Proposed Actions— specifically, on Projected Development Site 20 and Potential Development Site Q—could result in inadvertent construction-related damage to two NYCL- and/or S/NR-eligible historic resources, as they are located within 90 feet of one or more of the aforementioned projected and potential development sites. The two eligible resources – S/NR-eligible 292 Van Duzer Street and the S/NR-eligible and NYCL-eligible Stapleton Branch of the New York City Public Library – would not be redeveloped under the No-Action condition.

The New York City Building Code, under section C26-112.4, provides some measures of protection for all properties against accidental damage from adjacent construction by requiring that all buildings, lots, and service facilities adjacent to foundation and earthwork areas be protected and supported. For designated NYCL and S/NR- listed historic buildings located within 90 feet of a proposed construction site, additional protective measures under the DOB's TPPN #10/88 supplement the procedures of C26-112.4 by requiring a monitoring program to reduce the likelihood of construction damage and detect at an early stage the beginnings of damage so that construction procedures can be changed. For the two non-designated resources that are within 90 feet of Projected Development Site 20 and Potential Development Site Q, development under the Proposed Actions could potentially result in construction-related impacts to the resources, and the protective measures under TPPN #10/88 would only apply if the resources become designated.

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If these eligible resources are designated in the future prior to the initiation of construction, the protective measures of DOB's TPPN #10/88 would apply and indirect significant adverse impact from construction would be avoided. Should they remain undesignated, however, the additional protective measures of TPPN #10/88 would not apply, and the potential for significant adverse construction-related impacts would not be mitigated.

#### Noise

As described in Chapter 20, "Construction," the Proposed Actions would have the potential to result in significant adverse construction noise impacts throughout the Project Area and at sensitive receptors in the vicinity of the Project Area.

Based on the construction stage predicted to occur at each development site according to the conceptual construction schedule during each of the selected analysis periods, many receptors are expected to experience an exceedance of the *CEQR Technical Manual* noise impact threshold. One peak construction period per year over the analysis period of 2019 to 2030 was analyzed. Receptors where noise level increases are predicted to exceed the noise impact threshold criteria for two or more consecutive years or receptors where noise level increases are predicted to exceed the 15 dBA increment threshold for a shorter period (less than two years) were identified.

Because the analysis is based on anticipated construction phases, it does not capture the natural daily and hourly variability of construction noise at each receptor. The level of noise produced by construction fluctuates throughout the days and months of the construction phases, while the construction noise analysis is based on a conservative worst-case time periods only. The noise analysis results show that the predicted noise levels could exceed the *CEQR Technical Manual* impact criteria throughout the Project Area.

This analysis is based on a conceptual site plan and construction schedule. It is possible that the actual construction may be of less magnitude, or that construction on multiple Projected Development Sites might not overlap, in which case construction noise would be less intense than the analysis predicts.

Mitigation measures to address the identified construction noise impacts were explored between the DEIS and FEIS. It was found that there are no reasonable means to ensure measures be employed that would mitigate, partially or fully, the significant adverse construction noise impacts; therefore, the significant adverse construction noise impacts identified in Chapter 20, "Construction," would be unavoidable.